

**Integrated Ocean Drilling Program
Expedition 308 Preliminary Report**

Gulf of Mexico Hydrogeology

**Overpressure and fluid flow processes in the deepwater Gulf of
Mexico: slope stability, seeps, and shallow-water flow**

30 May–8 July 2005

Expedition 308 Scientists

PUBLISHER'S NOTES

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ABSTRACT

Integrated Ocean Drilling Program (IODP) Expedition 308 is the first part of a two-component program dedicated to the study of overpressure and fluid flow on the Gulf of Mexico continental slope. We are examining how sedimentation, overpressure, fluid flow, and deformation are coupled in passive margin settings. Expedition 308 tested a multidimensional flow model by examining how physical properties, pressure, temperature, and pore fluid composition vary within low-permeability mudstones that overlie a permeable and overpressured aquifer. We drilled, logged, and made in situ measurements in a reference location where little overpressure was deemed to be present: the Brazos-Trinity Basin. We contrasted these measurements with experiments performed in a region of very rapid Pleistocene sedimentation where overpressure is known to be present: the Ursa region of the northern Gulf of Mexico. Drilling documented severe overpressure in the Ursa region. Postcruise studies will illuminate controls on slope stability, seafloor seeps, and large-scale crustal fluid flow. Two key components of the experimental plan were to take substantial whole-core geotechnical samples for later shore-based analysis and to deploy the temperature and dual pressure probe (developed jointly between the Massachusetts Institute of Technology, Pennsylvania State University, and IODP at Texas A&M University) to measure in situ pressure.

Expedition 308 science met many of the objectives proposed in the original IODP Proposal 589-Full3 and provided the foundation to implement long-term in situ monitoring experiments in the aquifer and bounding mudstones in a future expedition designed to meet the full objectives of IODP Proposal 589-Full3. An important achievement of Expedition 308 is to have successfully recorded in situ formation pressure and temperature in an overpressured basin. This is the first time that we know of that such measurements have been obtained.

INTRODUCTION

Rapid sediment loading (>1 mm/y) drives overpressure (P^* ; pressure in excess of hydrostatic) in basins around the world (Fertl, 1976; Rubey and Hubbert, 1959). Sedimentation is so rapid that fluids cannot escape, the fluids bear some of the overlying sediment load, and pore pressures are greater than hydrostatic (Fig. F1).

Recent work has focused on how sedimentation and common stratigraphic architectures couple to produce two- and three-dimensional flow fields. For example, if a per-

meable sand is rapidly loaded by a low-permeability mud of varying thickness, fluids flow laterally to regions of low overburden before they are expelled into the overlying sediment (Figs. **F1**, **F2A**). This will create characteristic distributions of rock properties, fluid pressure, effective stress, temperature, and fluid chemistry in the aquifers and bounding mudstones (Fig. **F2B**). This simple process can cause slope instability near the seafloor (Fig. **F3A**) (Dugan and Flemings, 2000; Flemings et al., 2002); in the deeper subsurface, this process drives fluids through low-permeability strata to ultimately vent them at the seafloor (Fig. **F3B**) (Boehm and Moore, 2002; Davies et al., 2002; Seldon and Flemings, 2005).

Expedition 308 documents the spatial variation in pressure, vertical stress, and rock properties in a flow-focusing environment. We first established rock and fluid properties at a reference location (Brazos-Trinity Basin #4). We then drilled multiple holes along a transect in the overpressured Ursa system to characterize spatial variation in rock properties, temperature, pressure, and chemistry.

Geological Overview: The Gulf of Mexico

The Gulf of Mexico is a type location for a shallow drilling campaign aimed at understanding how sedimentation drives compaction and fluid flow (Fig. **F1**). Sedimentation, deformation, hydrodynamics, slope stability, and biological communities are interwoven in the Pleistocene strata of the Gulf of Mexico. Rapid sedimentation upon a mobile salt substrate is the driving force behind many of the active processes present (Worrall and Snelson, 1989). Bryant et al. (1990) described the physiographic and bathymetric characteristics of this continental slope (Fig. **F4**). In the region of offshore Texas and western Louisiana, individual slope minibasins are surrounded by elevated salt highs (Pratson and Ryan, 1994) producing a remarkable hummocky topography. This morphology is obscured in the eastern Gulf of Mexico, where sedimentation has been very rapid and more recent than the region of offshore Texas and Louisiana.

Pleistocene sediments were drilled in Brazos-Trinity Basin #4 and Ursa Basin (Fig. **F4**). The sedimentation rate in Brazos Trinity Basin #4 was envisioned to be relatively low, whereas the sedimentation rate in Ursa Basin was envisioned to reach rates of at least 1 cm/y. We anticipated hydrostatic pore fluid pressures in Brazos-Trinity Basin #4 and overpressured pore fluids in Ursa Basin.

Geological Setting

Brazos-Trinity Basin #4

Brazos-Trinity Basin #4 is 200 km due south of Galveston, Texas (USA) in ~1400 m water depth (Figs. F4, F5). The basin is one of a chain of five basins that are connected by interbasinal highs. It is a classic area for analysis of turbidite depositional environments because it is used as a modern analog to describe the formation of deepwater turbidite deposits (Badalini et al., 2000; Winker, 1996; Winker and Booth, 2000).

The primary data set used to evaluate the well locations is a high-resolution two-dimensional (2-D) seismic survey shot by Shell Exploration and Production Company to image the turbidite stratigraphy (Fig. F5). The line spacing is ~300 m. Three of the drilled locations are shown on dip seismic Line 3020 (Fig. F6). A strike line through Site U1320 is also illustrated (Fig. F7). Site U1320 (Figs. F5, F6, F7) is located where the turbidite deposits are thickest, whereas Site U1319 (Figs. F5, F6) is along the southern flank of the basin where turbidite deposits are more condensed.

Ursa Basin

Ursa Basin (~150 km due south of New Orleans, Louisiana [USA]) lies in ~1000 m of water (Figs. F4, F8). The region is of economic interest because of its prolific oilfields that lie at depths >4000 meters below seafloor (mbsf). Mahaffie (1994) described the geological character of the Mars oilfield. The Ursa field is in Mississippi Canyon Blocks 855, 897, and 899 and is 11.9 km east of the Mars tension leg platform.

We are interested in the sediments from 0 to 1000 mbsf. Four extraordinary three-dimensional (3-D) seismic data sets are available within Ursa Basin (Fig. F9). Shell and industry partners shot the Ursa exploration survey for exploration purposes. The high-resolution surveys were shot by Shell for the purpose of shallow hazards analysis.

Winker and Booth (2000) described deposition of Pleistocene to Holocene sediments. The Mississippi Canyon Blue Unit is a late Pleistocene, sand-dominated, “ponded fan” that was deposited in a broad topographic low that extended in an east-west direction for as much as 200 km and a north-south direction for as much as 100 km. The Blue Unit is overlain by a leveed-channel assemblage that was mud dominated and had dramatic along-strike variation in thickness. Pulham (1993) described a similar facies assemblage for this region.

Shell made downhole pressure measurements with a pore-pressure penetrometer (piezoprobe) at the Ursa platform (Eaton, 1999; Ostermeier et al., 2000; Ostermeier et al., 2001; Pelletier et al., 1999) (Fig. F10). They also acquired whole-core samples and performed consolidation experiments to evaluate preconsolidation stress and estimate overpressure. Piezoprobe measurements (circles) and maximum past effective stresses interpreted from consolidation experiments (triangles) indicate that (1) overpressure begins near the seafloor and (2) the pore pressure is ~50% of the way between the hydrostatic (P_h) and the lithostatic (σ_v) (Fig. F10). Pressures (both hydrostatic and lithostatic) are calculated from below seafloor and not from sea level.

Seismic Line A–A' (Fig. F11) illustrates the proposed boreholes. The sedimentary section is composed of a 300 m thick overburden that is predominantly mudstone. Beneath the overburden lies the first significant sand: the Blue Unit. The Blue Unit has a relatively flat base. Its upper boundary has relief, which most likely reflects post-depositional erosion. The Blue Unit is composed of interbedded sand and mudstone (Figs. F10, F11). A leveed-channel facies overlies the Blue Unit; it has a sand-cored channel that is flanked by mud-prone levee deposits. A mudstone package that thickens to the west overlies this sand assemblage. This mudstone package has numerous detachment surfaces that record slumping. The overlying mudstone is the eastern margin of a larger levee-channel system formed to the west.

SCIENTIFIC OBJECTIVES

The six original specific scientific objectives of Expedition 308 and their rationale were as follows.

- 1. Document how pressure, stress, and geology couple to control fluid migration on passive margins.*

We hypothesized that flow-focusing is present in Ursa Basin (Fig. F3). This should result in a characteristic spatial distribution of fluid pressure and rock properties (e.g., consolidation, permeability, and shear strength) in the mudstone overlying the Blue Unit. Our objective was to measure fluid pressure and rock properties through downhole tools, core, and logs to establish the vertical and lateral variation in pressure and rock properties above the Blue Unit. These data would test and refine the flow-focusing model.

- 2. Establish reference properties at Brazos-Trinity Basin #4.*

We wished to establish reference logging and core properties where overpressure is hypothesized to be zero and thus to measure properties at a range of effective stresses. These data would serve as a baseline against which the properties measured in Ursa Basin could be compared, allowing us to establish the deviation in sediment and fluid properties caused by fluid overpressure and low effective stress.

3. Illuminate the controls on slope stability.

Massive paleolandslides are present in Ursa Basin. We wished to determine pore pressure, rock properties, and overburden stress to predict the potential for slope failure in the present and to estimate the conditions that drove previous slope failures.

4. Understand timing of sedimentation and slumping.

Sedimentation rate drives the generation of overpressure. However, the age of strata in Ursa Basin is poorly understood. We wished to establish an age model to predict the sedimentation rate and the timing of paleolandslides.

5. Establish geotechnical and petrophysical properties of shallow sediments.

We wished to understand the state and evolution of geotechnical and petrophysical properties of mudstone at effective stresses encountered between the seafloor and 500 mbsf. A complete logging suite, in situ measurements of permeability and pressure, and core samples will allow us to understand compaction and flow processes near the seafloor.

6. Provide an extraordinary data set to observe ponded and channelized turbidite systems.

Brazos-Trinity Basin #4 and Ursa Basin are foci of study for turbidite depositional systems. Logging and core data will provide a unique opportunity to study turbidity currents and related mass deposits.

OPERATIONAL STRATEGY

The overall strategy for Expedition 308 was to complete continuous coring, wireline logging, in situ measurements, and logging-while-drilling (LWD) operations at each primary site. As time allowed, we also visited alternate locations. To minimize the time that expensive LWD tools and personnel were kept on board the ship, the strat-

egy was to first core and perform downhole measurements in Brazos-Trinity Basin #4 and then to perform continual LWD measurements first in Brazos-Trinity Basin #4 and then in Ursa Basin. Thereafter, the LWD tools would be offloaded and final coring and downhole measurements would be performed in Ursa Basin.

We planned to use LWD because we expected to encounter thick unconsolidated sands in Brazos-Trinity Basin #4 and because we might encounter unconsolidated sands in Ursa Basin. Unconsolidated sands can result in unstable boreholes where it is not possible to deploy wireline tools. LWD would ensure that a good logging suite was obtained.

In addition to LWD, we also planned to use measurement while drilling (MWD). In MWD, logging data are communicated in real time from near the drill bit to the ship so that the borehole conditions can be continuously monitored. In Ursa Basin, we expected to encounter overpressured mudstones and it was possible we would encounter overpressured and unconsolidated sands. If we encountered unconsolidated and overpressured sands, there was a risk that “shallow-water flow” would occur. Shallow-water flow results when overpressured unconsolidated sands flow into a borehole that has a lower pressure than the formation pressure. With MWD, we would be able to monitor both the downhole annular pressure and the formation lithology. When shallow-water flow occurs, an elevated pressure is recorded as sand flows into the borehole. Through continuous monitoring we would be able to decide whether it was necessary to increase the mud weight to offset the flow into the borehole or terminate the drilling and kill the well.

Finally, to minimize shallow-water flow, we planned to use heavy mud during drilling and coring of portions of proposed Sites URS-1B and URS-2C. We also planned to deploy heavy mud during long-term in situ measurements with penetration probes (Davis-Villinger Temperature-Pressure Probe [DVTTP] or temperature/dual pressure [T2P] probe).

It was planned to use two downhole tools to measure pressure and temperature: the T2P, which was designed by the Massachusetts Institute of Technology (MIT), Pennsylvania State University, and Integrated Ocean Drilling Program (IODP) U.S. Implementing Organization Science Services, Texas A&M University (TAMU) and the DVTTP. The T2P is designed to measure pore pressure more rapidly than the DVTTP. It has a narrow tip with a temperature and pressure sensor; a second pressure measurement is collected slightly up-probe from the sensors at the tip (Fig. F12). The design

allows for rapid measurement of pressure in low-permeability sediments. In addition to temperature measurements made with the T2P and DVTPP, temperature measurements were made during coring with the advanced piston corer (APC) using the advanced piston corer temperature (APCT) tool. Multiple 10–20 cm long whole-round cores were planned to assist interpretation of the T2P and DVTPP data, directly measure formation pressures, and infer the in situ stress state through laboratory analysis.

SITE RESULTS

Site U1319

Site U1319 is located on the southern flank of Brazos-Trinity Basin #4 (Figs. F5, F6). The primary objective at this site was to establish a reference section to determine the rock and fluid properties in a normally pressured basin. Secondary objectives included establishing an age model for Brazos-Trinity Basin #4 and studying turbidite deposits. To achieve these objectives, Hole U1319A was continuously cored from the seafloor to a terminal depth of 157.5 mbsf. A MWD/LWD-dedicated hole (Hole U1319B) was then drilled to a terminal depth of 180 mbsf.

Site U1319 is located at the edge of the minibasin. As a result, the cored succession of hemipelagic deposits and turbidites (Fig. F13) is condensed relative to that at the basin center. Nevertheless, a detailed record of turbidite deposition was present, which could be correlated to the basin center. Six lithostratigraphic units were recognized: Unit I (Holocene drape), Unit II (turbidites and debris flows), Unit III (hemipelagic sediments), Unit IV (distal turbidites), Unit V (hemipelagic sediments), and Unit VI (very distal turbidites mixed with hemipelagic sediments). Unit V was deposited prior to the formation of the Brazos-Trinity minibasin, and all overlying sediments were deposited within it. Ash layer Y8, a regional stratigraphic marker resulting from the Los Chocoyos (Guatemala) eruption and dated at 84 ka (Drexler et al., 1980; Mallarino et al., in press), was recovered in Unit III. Hemipelagic Units I and V are interpreted to have been deposited during eustatic highstands at the present and at 125 ka, respectively.

Rare to abundant assemblages of well-preserved microfossils, spanning the late Pleistocene–Holocene period (marine oxygen isotope Stages [MIS] 1–6), were recovered. Tropical to subtropical species dominate the interglacial assemblages, whereas cool-temperate species are more common in assemblages from glacial intervals. The absence of reworked Cretaceous–Neogene nannofossils in the lower part of Hole

U1319A (Units III and V) point to quiet open-marine environments. Moderately abundant benthic foraminifers in the upper ~30 m of the hole indicate a low-oxygen, high-nutrient environment.

Bulk density, measured both on the multisensor track (MST) and on discrete samples, increases with depth from ~1.3 to 2.0 g/cm³, reflecting normal compaction. Core resistivity, derived from the MST, increases with depth to ~60 mbsf and thereafter remains constant. Porosities decrease from initial values near 80% to ~50% near the bottom of the hole (Fig. F13). Peak shear strength (Fig. F13) shows a general increase with depth as a result of increasing vertical effective stress and sediment consolidation. The trend is relatively smooth from the seafloor to ~80 mbsf; beneath 80 mbsf there is a sharp increase in undrained shear strength. The maximum peak strength recorded was 89 kPa. Ratios between the peak and undrained shear strengths show that the clays encountered at Site U1319 have a low sensitivity.

Interstitial water chemistry shows large variations in alkalinity from 2.95 to 19.45 mM, with a downhole concave profile and a rapid increase to its maxima at 15 mbsf. pH shows a similar concave depth profile, but with a maximum at ~30 mbsf. Sulfate concentrations in interstitial water show rapid downhole depletion with a sulfate/methane interface at 15 mbsf. The ionic concentrations of dissolved Mn show a similar depletion trend as the sulfate concentration, whereas dissolved Ba, B, and Si show a concave downward profile similar to the alkalinity and pH. The sharp pore water chemistry changes at shallow subseafloor depths suggest rapid anaerobic degradation of organic matter through sequential redox reactions within the uppermost 15 m.

Average total organic carbon (TOC) content is relatively low for Gulf of Mexico sediments (0.75 wt%), but these values are consistent with the relatively low microbial biomass encountered (maximum cell density observed = 1×10^6 cells/mL). Inorganic carbon concentration is highly variable throughout the hole, ranging from 0.87 to 4.08 wt% (10.44 to 48.96 wt% CaCO₃). The average C/N ratio in the sediment was 3.77, suggesting either that algal material is the predominant source of organic matter or that the presence of inorganic nitrogen (such as ammonia) artificially lowers C/N ratios. The C/N maximum of 5.92 is coincident with the bottom of the sulfate reduction zone. The lack of any ethane (C₂) in headspace samples suggests that the relatively large quantities (as much as 11,310 ppmv) of methane (Fig. F13) detected is of biogenic, not thermogenic, origin.

Two deployments of the T2P were completed in Hole U1319A. The first deployment was at 1388 meters below sea level (41.6 m above seafloor) and provided a successful pressure test that demonstrated the tool could successfully pass through the lockable float valve (LFV) of the bottom-hole assembly (BHA). Measured pressure (13.76 MPa) was slightly below hydrostatic (13.94 MPa), and the recorded water temperature was 4.9°C. A second T2P deployment at 80.5 mbsf recorded 1 m of penetration into the sediment. After 30 min, the tip pressure was at 15.49 MPa and the shaft pressure at 15.95 MPa; hydrostatic pressure was 15.19 MPa, and formation temperature was 7.3°C. Because of the nonvertical penetration of the T2P into the sediment, the tip of the tool was bent.

MWD/LWD operations were completed in Hole U1319B to 180 mbsf with data coverage by all MWD/LWD tools over the interval cored in Hole U1319A (0–157.5 mbsf). From the seafloor to 180 mbsf, the following trends were observed: gamma radiation increased from 45 to 75 gAPI, deep button resistivity increased from 0.6 to 1.8 Ωm (Figs. F13), porosity decreased from 75% to 50%, and bulk density increased from 1.4 to 2.0 g/cm³. These data suggest a normal compaction trend in the clay-rich section of Site U1319 (Fig. F13). Deviations from this trend occur at 25 mbsf, where the gamma ray has a step decrease (top of Unit III, foraminifer-rich clay), from 30.5 to 31.5 mbsf where gamma radiation increased (onset of fine lamina of sand, Unit IV), and from 78 to 93 mbsf, where bulk density decreased (consistent with physical properties observed in the cores).

Drilling objectives at Site U1319 were fully accomplished. The almost continuous coring, lithostratigraphic, biostratigraphic, and logging records make Site U1319 an important reference location for the study of sediment compaction. The low thermal gradient (~20°C/km) was also striking. Finally, the ability to detect individual lithostratigraphic units within the uppermost 30 mbsf allowed us to date and describe these turbidite deposits.

Site U1320

Site U1320 is located near the center of Brazos-Trinity Basin #4 (Fig. F5). The main drilling objective at this site was to establish a reference section to determine the rock and fluid properties in a normally pressured basin. Secondary objectives included improving the age model for Brazos-Trinity Basin #4 and studying turbidite deposits. Hole U1320A was continuously cored and wireline logged to a terminal depth of

299.6 mbsf. A MWD/LWD-dedicated second hole (Hole U1320B) was then drilled to a terminal depth of 320 mbsf.

The lower part of the sedimentary succession (Fig. F14) is termed lithostratigraphic Unit V in Hole U1320A. This sedimentary sequence is dominated by clay with rare silt lamina often containing fragments of foraminifers. Most of the succession is intensely bioturbated. We interpret lithostratigraphic Unit V to represent hemipelagic sedimentation with a high influx of siliciclastic material derived from either river plumes and/or very low density turbidity currents. Above lithostratigraphic Unit V, Unit IV is dominated by clay and represents the initial pulse of turbidite influx into the Brazos-Trinity Basin #4. Lithostratigraphic Unit III consists of a foraminifer-bearing light greenish gray clay that contains a volcanic ash layer (Y8), the product of the Los Chocoyos (Guatemala) eruption dated at 84 ka (Drexler et al., 1980; Mallarino et al., in press). Lithostratigraphic Unit II represents the main phase of basin filling and is defined by a 135 m thick succession of both sandy and muddy turbidites and muddy slump/debris flow deposits. Lithostratigraphic Unit I consists of a thin veneer of Holocene hemipelagic sediments. The overall basin fill succession shows a general upward increase in proportion of sand and thickness of turbidite packages (Fig. F14).

Site U1320 yielded rare to abundant assemblages of calcareous microfossils spanning the late Pleistocene–Holocene in MIS 1–6. Tropical to subtropical species dominate the interglacial assemblages, whereas cool-temperate species are more common in assemblages from glacial intervals. Intervals deposited during MIS 5 show no reworked nanofossils, indicating a quiet open-marine environment during sea level highstands. Frequent small thin-shelled benthic species of *Bolivina* and *Bulimina* are found in the lower part of Hole U1320A, suggesting that low-oxygen, nutrient-rich bottom conditions prevailed during MIS 6 in Brazos-Trinity Basin #4.

Results of physical property analysis at Site U1320 suggest that compaction-driven fluid expulsion was a main factor influencing the physical characteristics (Fig. F14) of the sediments. Lithostratigraphic Unit II is characterized by considerable scatter in porosity (36%–71%) (Fig. F14). This is interpreted to result from variations in lithofacies, in particular the presence or absence of sandy intervals. Lithostratigraphic Unit V is characterized by a gradual decline in porosity with depth, reaching ~50% by ~299 mbsf. This porosity decrease drives increases in thermal conductivity, magnetic susceptibility, and resistivity. Bulk density increases with depth from 1.4 g/cm³ at the seafloor to 2.0 g/cm³ at 273 mbsf. Grain density variations are small (between 2.6 and 2.8 g/cm³). Thermal conductivity increases with depth from 1.1 to 1.3 W/m·K.

Chemical pore water data in Hole U1320A suggest rapid anaerobic degradation of organic matter through sequential oxidation fronts within shallow depths, whereas chemical changes in deeper sections of the hole point to diagenetic processes and/or deep-seated fluid flow. Rapid change in interstitial water profiles occurs at shallow depths within the upper part of lithostratigraphic Unit II (uppermost 40 mbsf). The decrease in SO_4 , from approximately ambient seawater concentrations of 24.4 mM to a minimum of 0.5 mM at 21.5 mbsf, coincides with a concomitant increase in alkalinity from 4.77 to a maximum of 15.99 mM at 20 mbsf. Mn concentrations also decrease downhole to a minimum of 1.37 mM at 34.5 mbsf. Salinity and Ca, Mg, K, Li, and Sr decrease with depth to 40 mbsf. In lithostratigraphic Unit V, a significant increase in Ca and Sr corresponding with a decrease in Li concentration takes place. Ba has its maximum concentration between 120 and 180 mbsf (lithostratigraphic Units III and IV).

The average TOC content (0.53 wt%) is consistent with the concentrations observed in Hole U1319A and is estimated to be either primarily derived from algal material (average C/N = 4.21) or to contain a substantial amount of inorganic (bound) nitrogen that lowered the C/N ratio. Trends in total inorganic carbon, TOC, N, C/N, and H data clearly correlate with seismic reflector surfaces R10 and R20. The highest concentration of methane (57,714.2 ppm) is observed at 122 mbsf (Fig. F14). Methane to ethane ratios (C_1/C_2) are very high, suggesting a biogenic origin for the methane. The calculated sulfate/methane interface (SMI) depth is 22 mbsf. The inverse correlation between sulfate and methane gradients suggests local methanogenesis; however, the low microbial biomass (1×10^6 cells/mL) cannot support the in situ production of large amounts of methane.

Two deployments of the T2P were completed in Hole U1320A. The first deployment was at 126.3 mbsf (below Core 308-U1320A-15X) and the second deployment was at 213.0 mbsf (below Core 308-U1320A-24X). Both deployments used the tapered needle probe. The first deployment was completed with the drill bit ~1 m from the bottom of the hole and used the drill string to push the T2P into the formation. The deployment resulted in a slight bend to the needle probe, and the pressure transducer did not record data. The second deployment was also completed with the drill bit 1 m above the bottom of the hole, but instead of using the pressure of the drill string, the tool string weight was used to insert the probe into the formation. All transducers performed well, and the T2P was retrieved without damage. Both deployments recorded pressures that were slightly below hydrostatic. The temperature gradient between the two deployments was 20°C/km.

From the seafloor to 177 mbsf, resistivity, gamma ray (Fig. F14), and porosity logs from downhole logging operations delineate a series of interbedded sand and mud facies that correspond to lithostratigraphic Unit II. Porosity decreases with depth from 87% to ~45% at a total depth of 297 mbsf, indicating compaction and potential fluid expulsion throughout the entire drilled interval. LWD resistivity images of the borehole show apparent breakouts at the bottom of the hole with an east-west orientation.

All primary and secondary drilling objectives were accomplished at Site U1320. Drilling results, together with those from Site U1319, provided key information on the space-time evolution of sedimentary and geochemical systems in Brazos-Trinity Basin #4 and on the range of variation for physical properties for this basin.

Site U1321

Site U1321 is located on the southern portion of Brazos-Trinity Basin #4 within a section of basin turbidites underlain by a thicker section of hemipelagic mud (Figs. F5, F6). Hole U1321A was drilled as a dedicated MWD/LWD hole to better correlate lithostratigraphic units and individual sand layers across the south-southwest margin of Brazos-Trinity Basin #4 and to document the lateral change in petrophysical properties (Fig. F15) of the fan units above Reflector R40 (Fig. F6, F15). The LWD data indicate a shallow series of interbedded sand and mud facies that correspond to lithostratigraphic Unit II in Hole U1320B. Porosity from logging data (Fig. F15) decreases with depth from 80% to 45% at ~34 mbsf, indicating rapid compaction and potential fluid expulsion in shallow sections. Most of the units identified in the logs seem to be thinning with respect to the units identified in Hole U1320B. Resistivity images of the borehole show apparent breakouts at the bottom of the hole with an east-west orientation, similar to what was observed at Site U1320. These breakouts indicate a north-south maximum horizontal stress direction. The resistivity images are also characterized by a series of thin alternating resistive and conductive laminations that may represent variations in silt content. Steep features at the bottom of the hole have been identified as potential slump deposits or faulted blocks.

MWD/LWD operations at Site U1321 permits bed by bed correlation between Sites U1319 and U1320 (see discussion in **“Synthesis of Brazos-Trinity Basin #4 Geology”**), which is critical for the study of sandy turbidites.

Site U1322

Site U1322 is the easternmost site drilled in Ursa Basin during Expedition 308 (Fig. F8). Of the three sites in Ursa Basin, Site U1322 has the thinnest sediment cover above the permeable Blue Unit (Fig. F9). The principal objectives of drilling Site U1322 were to document rock physical properties at the location of minimal overburden in Ursa Basin, measure in situ formation temperature and pressure, document geochemical composition of the pore water, and establish a preliminary age model leading to an estimate of sediment accumulation rates at this location. The ultimate goal of drilling in Ursa Basin was to explore fluid flow and fluid pressures in an overpressured basin.

Hole U1322A was the first dedicated MWD/LWD hole in Ursa Basin. It was decided to utilize MWD/LWD before coring because acquisition of real time pressure and lithology data were needed to know whether shallow water flow was occurring during drilling. The approach established for IODP that MWD/LWD as a viable tool to monitor pressure and lithology in a drill hole. Drilling in Hole U1322A advanced at an average rate of penetration (ROP) of 30 m/h to a depth of 200 mbsf. Below this, to prevent any communication with the Blue Unit, drilling continued at a reduced ROP of 20 m/h to the target depth of 238 mbsf. The MWD/LWD operation in Hole U1322A reached 238 mbsf without encountering any major sand units. Overall, hole quality remained good (average diameter = 26.9 cm) for almost the entire borehole. Hole U1322A is characterized by relatively monotonous logging data, mostly indicating clay, mud, and occasionally silt (Fig. F16). Resistivity and gamma ray measurements show the highest variability and can be correlated to several units defined by visual observation of the cores (see below) and to seismic Reflectors S10 and S30. In particular, logging data support the division of the lithostratigraphic column (Fig. F16) encountered in Hole U1322B into two lithostratigraphic units (Units I and II) and the further division of lithostratigraphic Unit I into Subunits Ia–Id. The constructed synthetic seismogram for Hole U1322A demonstrates that the correlation between logging data and high-resolution seismic matches only the uppermost 100 mbsf. Nevertheless, the overall quality of the time-depth model allows an approximate correlation of seismic reflections with observations in core and logging data. The GVR electrical images obtained in this hole reflect the occurrence of undisturbed sediments but also of contorted and faulted sediments. The most striking features are parallel east-west orientated contours of analog resistivity that may represent breakouts indicating the direction of the minimal horizontal stress exposed by the drilling process.

Based on visual description of the cores in Hole U1322B, the 234.5 m sediment succession (Fig. F16) was divided into two lithostratigraphic units (Units I and II). The total depth of this succession ties closely to seismic Reflection S60-1322, and the boundary between lithostratigraphic Units I and II (125.8 mbsf) occurs just above the prominent seismic Reflector S30. Lithostratigraphic Unit I is dominated by clay locally interbedded with silt and is further divided into four subunits (Subunits Ia–Id) based on the occurrence of intervals of deformed sediment. Lithostratigraphic Unit II is characterized by alternating intervals of meter-scale deformed and coherently laminated clay and mud. The deformed intervals are composed of brownish and greenish gray mud yielding intervals of dipping beds, small-scale faults, recumbent folds, and mud clasts. Nine deformed intervals with thicknesses varying from 2 to 5 m were recognized based on the occurrence of undeformed mud layers at their base.

Preliminary biostratigraphic data from nannofossils and planktonic foraminifers indicate that the sediment sequence recovered at Site U1322 was deposited over the last 60 k.y., more specifically during MIS 1–4. Sedimentation rates of ~1 to 2 m/k.y. were estimated for the intervals above 30 mbsf and between 125 and 185 mbsf. Between 30 and 125 mbsf and below 185 mbsf, sedimentation rates increased to 12 m/k.y. or possibly higher in the intervals of mass flow deposits. Distinctive cyclic patterns were observed in the distribution of nannoplankton and foraminifers, indicating periodic influx of sediments from the Mississippi River associated with turbidity currents in Ursa Basin. Persistent low-oxygenated “stress” environments due to rapid sediment loading encouraged the proliferation of infaunal benthic foraminifers. A deltaic benthic foraminifer assemblage from the interval between 185 and 234 mbsf is similar to those existing today along the shelf edge of the Mississippi delta, suggesting a period of strong gravity flow due to levee overflows or slope failures at ~60 ka.

Variations in physical properties correlate well with lithostratigraphic units and seismic reflectors at Site U1322. The porosity profile (Fig. F16) shows a relatively rapid decrease from the seafloor to 30 mbsf and then a more gentle decrease down to the bottom of the borehole. In slumped intervals, the porosity is lower than in non-slumped intervals: the maximum porosity decrease in the slumps is 5 porosity units. The undrained shear strength shows a more linear increase with depth (Fig. F16). A shift of 50 kPa at 125 mbsf is observed at the base of lithostratigraphic Subunit Id, a 30 m thick slump deposit. Smaller shifts are also observed at the base of each slump deposit. Slumps typically have higher undrained shear strengths than non-slumped deposits.

Chemical composition of the interstitial waters at Site U1322 shows large variations in the top 100 mbsf, in particular around the boundary between seismic Reflectors S10 and S20. Alkalinity, pH, concentrations of Ca, Sr, Li and B ions, and ammonium show concave depth profiles with maxima centered at the depth around Reflector S10. Above Reflector S10, salinity and sulfate concentrations are constantly high, and they show a rapid decrease between Reflectors S10 and S20 associated with the decrease of several other elements such as Ca, Mg, B, Li, and Sr. At Site U1322, the SMI is very deep at 74 mbsf, which corresponds to a rapid increase in methane concentration. Above the SMI, only minor amounts of methane (several ppmv) were detected. The highest concentration of methane (29,536–51,001 ppmv) was observed between 75 and 129 mbsf (Fig. F16). Only trace amounts of ethane (<3.4 ppmv) and ethylene (<2.6 ppmv) were detected in a few headspace samples. No higher hydrocarbons were detected at Site U1322. The high C_1/C_2 ratios suggest a biogenic origin of the methane, which could come from in situ microbial activities or hydrogeologically driven migration. Considering the low abundance of subsurface microbes, in situ methanogenesis should also be low. Hence, the anomalously high concentrations in the middle part of lithostratigraphic Unit I are inferred to be associated with fluid flow from beneath the above-mentioned strata.

A maximum cell density of 4.0×10^5 cells/mL was observed at 2.9 mbsf in Hole U1322B. Microbial abundance decreased with depth below the cell enumeration confidence limit of 1.0×10^4 cells/mL at 74.5 mbsf. The extremely low cellular biomass at Site U1322 is consistent with microbial abundance levels at Site U1324. An important observation is that microbial biomass in Ursa Basin is an order of magnitude lower than cell densities observed at Sites U1319 and U1320 in Brazos-Trinity Basin #4. This phenomenon is as yet unexplained.

In Hole U1322C, there was one high-quality DVTTP deployment at 236 mbsf and one high-quality T2P deployment at 150 mbsf. These provided us with a reasonable record of in situ temperature and pressure for Site U1322. Most of the other deployments recorded subhydrostatic pressures immediately after the drill string was raised. Based on these results (or lack thereof), we decided to spend the remaining 36 h of operation time drilling an additional geotechnical hole at this site. This decision was also motivated by the fact that our revised authorized depth of penetration at Site U1323 (174 mbsf) meant that the interval of major scientific interest could not be penetrated. The purpose of the new Hole U1322D was to deploy the pressure and temperature probes and spot core after each deployment. The cores obtained were to be sampled for geotechnical analysis and then processed through the onboard laboratories.

All of the objectives set for Site U1322 are considered fulfilled. The principal result was that we acquired a good data set of formation pressures and temperatures for this site that can now be compared to Site U1324. T2P and DVTPP measurements at Site U1322 provided critical data for understanding overpressure and associated flow in Ursa Basin. Dissipation curves at Site U1322 (seven measurements) document overpressure at 50 mbsf and continuing to the bottom. The temperature gradient at Site U1322 is 26.4°C/km (13 measurements from 42 to 238 mbsf).

Site U1323

Site U1323 is located in Ursa Basin between Sites U1322 and U1324 (Figs. F8, F11). Site U1323 has a sediment cover above the permeable Blue Unit intermediate in thickness between those of Site U1322 and U1324. The objectives of drilling Site U1323 were to document rock physical properties at this location, measure in situ formation temperature and pressure, document geochemical composition of the pore water, and establish a preliminary age model leading to an estimate of sediment accumulation rates at this location. Site U1323 was logged using MWD/LWD and was not cored. This was because an overpressured sand was encountered during MWD/LWD at a relatively shallow depth. Ultimately, we chose to spend the remaining time making downhole measurements at Site U1322 rather than return to Site U1322 for coring.

MWD/LWD at Site U1323 proceeded at an average ROP of 30 m/h, but borehole diameters were typically >24 cm to a depth of 204 mbsf, where an overpressured sand was encountered. The silty sand layer, ~3 m thick, was detected at 204 mbsf and simultaneously a jump in pressure of 150 psi (~1 MPa) over the background drilling pressure in the APWD log was observed. A residual backpressure of 150 psi was also observed by the driller when he shut down the mud pumps. At 242 mbsf, a rapid drop in gamma radiation, suggestive of a second sand interval, was observed. At this point it was decided that to maximize the amount of science and conserve mud we should move to Site U1324 and plug and abandon Hole U1323A. Site U1323 was the *JOIDES Resolution's* first experience with riserless drilling using weighted mud. It was a valuable learning exercise and everyone came away with confidence in the ability to handle downhole pressures in a routine fashion. We confirmed that we can carefully monitor shallow flows, take appropriate action to control the flow, drill ahead under appropriate conditions, and provide accurate real-time downhole information.

Lithostratigraphic interpretation of LWD and seismic data are still preliminary as a malfunctioning battery required onshore processing of the resistivity image data be-

fore a comprehensive interpretation could be performed. Logging and seismic data (Fig. F17) confirm that the upper 197 m interval is predominantly mud and clay rich, including two mass transport deposits. Preliminary interpretation of the resistivity image data that were sent back to the ship at the end of the expedition shows several highly deformed intervals confirming the original logging-seismic interpretation of the presence of several mass transport deposits. These mass transport deposits also displayed trademark characteristics of higher bulk density and resistivity compared with surrounding undeformed sediment and will provide great data for postcruise analysis of such deposits.

Despite not coring Site U1323, the high-quality logging data prove valuable for analysis of the stratigraphic history of Ursa Basin. Drilling objectives for Site U1323 were thus achieved in three different ways: (1) overpressure was evidenced during MWD/LWD operations, (2) the novel IODP approach to “riserless-controlled drilling” proved efficient in controlling the flow, and (3) data obtained at Site U1323 provide information on the lateral continuity and the stratal architecture of Ursa Basin.

Site U1324

Site U1324 is the westernmost site drilled in Ursa Basin during Expedition 308 (Fig. F8). Of the three sites in Ursa Basin, Site U1324 has the thickest sediment package above the permeable Blue Unit. The principal objectives of drilling Site U1324 were to document rock physical properties at the location of maximum overburden thickness in Ursa Basin, measure in situ formation temperature and pressure, document geochemical composition of the pore water, and establish a preliminary age model leading to an estimate of sediment accumulation rates at this location.

The stratigraphy of Hole U1324A (Fig. F18) was first divided into two main units based on logging responses. These units were further divided into several subunits based on comparisons with nearby core data from Hole U1324B and variations in the logging responses. The main regional seismic reflectors (S10–S50) can be identified in the logging data as significant variations in velocity, gamma radiation, and/or resistivity (Fig. F18). The LWD resistivity images show a large degree of deformation, especially in logging Unit II. These images show significant folds and variable dips ranging from shallow to relatively steep ($>60^\circ$). This suggests a significant amount of deformation most likely caused by mass transport events. These events seem to indicate a high degree of slope instability due to the presence of turbidites that have been

dislocated, and in some instances, also folded. Tilted beds, folds, and faults are dominated by a general east-west strike.

The 612 m thick sedimentary succession overlying the Blue Unit at Site U1324 records the evolution of the eastern levee of the Southwest Pass Canyon channel-levee system (Fig. F18). Visual observation of the cores supported the division of the lithologies into two lithostratigraphic units. Lithostratigraphic Unit I is composed of clay and mud and contains two mass transport deposits. Lithostratigraphic Unit II is composed of interbedded silt, sand, and mud and contains at least three mass flow deposits. Prior to Expedition 398, seismic correlation suggested that acoustically semitransparent intervals in lithostratigraphic Unit I represent regional mass flow deposits composed of faulted and contorted masses of mud and clay. However, close examination of the cores reveals that the mass flow deposits contain levee clay and mud that are only mildly deformed and tilted and thus are interpreted to have not been transported very far from their original position.

Variations in physical properties correlate well with lithostratigraphic units. The interbedded silt, sand, and mud and mass flow deposits in lithostratigraphic Unit II are characterized by highly variable bulk density, porosity (Fig. F18), and peak shear strength. Physical properties show much less scatter in the uniform hemipelagic mud and clay in lithostratigraphic Unit I. MAD bulk density is consistent with those measured by MST and LWD in lithostratigraphic Unit I. A porosity increase at 40 mbsf correlates with seismic Reflector S10. A decrease in resistivity and low thermal conductivity were also observed at that depth. A sharp porosity increase at ~160 mbsf is related to the silt layer above seismic Reflector S30 (Fig. F18), which may be significantly overpressured. This explanation is supported by the observed decrease in *P*-wave velocity, thermal conductivity, and undrained shear strength at this depth.

Preliminary biostratigraphic data from nannofossils and planktonic foraminifer assemblages as well as magnetostratigraphy indicate that the sediment sequence recovered at Site U1324 was deposited over the last 60 k.y., more specifically during MIS 1–4. Sedimentation rates varied between 5 and >10 m/k.y. for lithostratigraphic Unit I in the interval above 365 mbsf of Hole U1324B, with possible sedimentation rate peaks of 12 m/k.y. or more in the intervals of mass flow. Between 365 and 608 mbsf, in lithostratigraphic Unit II, sedimentation rates appear to have been higher, perhaps in excess of 25 m/k.y. However, the low microfossil abundance and the relatively young age of the sediments render precise dating of this interval difficult. Distinctive cyclic patterns were observed in the distribution of nannoplankton and foraminifers,

indicating periodic influx of sediments from the Mississippi River associated with turbidity currents in Ursa Basin. The infauna-dominated benthic foraminifer assemblages also suggest a prevalence of low-oxygenated “stress” environments due to rapid sediment loading in the basin during the last glacial period.

Variation in interstitial water chemistry at Site U1324 is largest at shallow depths (<100 mbsf). Below this depth, only very limited changes are observed. Pronounced pore water chemical changes are particularly important from the seafloor to the S10 seismic reflector (~35 mbsf). Li, B, and Sr reach their maxima within this depth range, and Mn reaches its minimum at ~35–40 mbsf. H_4SiO_4 and Fe reach their maxima between ~20 and 25 mbsf. Between 40 and 160 mbsf, salinity, Li, B, and Sr decrease; Ba, Fe, and NH_4 increase; and Cl, Mn, and H_4SiO_4 are constant. The extremely high ammonium contents (up to 6820 μM) in pore water are consistent with more reducing conditions at this site compared with the sites drilled in Brazos-Trinity Basin #4. The general downhole increase in ammonium likely reflects enhanced organic degradation at greater depths. The vertical profile, especially the surficial maximum and minimum in dissolved Fe and Mn, are consistent with the hierarchy of redox reactions often observed in deep-marine sediments. The high Fe contents at shallow depths might reflect enhanced Fe reduction and/or greater availability of detrital Fe oxides/oxyhydroxides, or simply Fe-rich clays. The pore water chemistry is probably dominated by dissolution processes rather than by organic matter degradation, which enhances alkalinity, Ca, Mg, Sr, B, and Li concentrations at ~35 mbsf. The causes for the very acidic (pH < 7.0) nature of the pore water found above 200 mbsf at Site U1324 are unclear and needs further investigation.

Methane concentration (Fig. F18) increases dramatically in the middle section of lithostratigraphic Unit I (160 mbsf) but remains low in the rest of the hole. The predominant hydrocarbon found in Hole U1324B was methane, and the C_1/C_2 ratios were high, suggesting a biogenic origin for the methane. Therefore, we interpret the methane found at Site U1324 as resulting from in situ microbial activities or alternatively as having migrated from lateral locations. The microbial cell count at Site U1324 was low, with a maximum cell density of 2.0×10^5 cells/mL at 2.8 mbsf. This is an extremely low and unexpected value considering the location and high sedimentation rate of this site. At this time, the predominance of clay-rich sediment at Site U1324 preventing fluid migration is the only reason thought to explain the low abundance of microbial communities.

In situ measurements made with the T2P and DVTPP documented fluid overpressure and a low thermal gradient at Site U1324. Successful fluid pressure measurements at 117, 300, 405, and 608 mbsf yielded values for λ^* between 0.2 and 0.6 (λ^* = ratio of overpressure to hydrostatic vertical stress). Eighteen temperature measurements constrain a geothermal gradient of about 19°C/km.

All of the objectives set for Site U1324 are considered fulfilled. The principal result is that we acquired a good data set of formation pressures and temperatures for this site. Once compared to a similar data set at Site U1322, this will allow testing of the model of overpressure on which the strategy of Expedition 308 was based. However, the fact that pore water pressures in Holes U1324B and U1324C lie between the lithostatic and hydrostatic pressure gradient is already a demonstration that Ursa Basin is overpressured. Moreover, results from lithostratigraphy and biostratigraphy have constrained unusually high sedimentation rates and the timing of mass flow deposition at this location. The data and observations made at Site U1324 are critical for logging-seismic integration, and for the understanding of geological processes leading to overpressure in Ursa Basin.

DISCUSSION AND CONCLUSIONS

Challenges of Drilling in Overpressured Basins

Expedition 308 was the first expedition in IODP/ODP/DSDP history during which large volumes of weighted mud were used as part of the experimental design to achieve the scientific goals of the expedition (Fig. F19). Prior to the expedition, it was determined that there was a significant probability of encountering shallow-water flow in the subsurface. Shallow-water flow occurs when overpressured and unconsolidated sands flow into the borehole, which is at a lower pressure. Ultimately, these sands can be expelled at the seafloor.

To counter this behavior, weighted muds were used during drilling. The weighted mud is pumped down to the seafloor and ultimately expelled at the seafloor (Fig. F20). The effect of the weighted mud is to create a higher pressure within the annulus, which will offset the overpressure within the formation. During Expedition 308, a weighted mud composed of barite, sepiolite, and seawater was used at Sites U1323 and U1324, two of the sites where shallow-water flow was considered a significant risk. In these locations, 10.5 ppg mud was generally used. Shallow-water flow was, in fact, encountered in Hole U1323A (see “[Operations](#)”) at ~200 mbsf while drilling

with seawater (Fig. F21). An abrupt increase in pressure associated with a thin sand (indicated in the gamma ray log) was identified. After raising the mud weight in the borehole, we drilled forward some distance before ultimately killing the flow with a 13.5 ppg mud, whereupon we cemented the hole with 14 ppg mud. Table T1 illustrates the approximate volumes, durations, and depth ranges that mud was used.

In addition to the need to drill the borehole safely, weighted mud was also used to stabilize the hole for long-term deployments of penetrometers (DVTPP and T2P). In this case, the weighted mud was extremely useful for keeping the hole open. Because the formation is relatively plastic, over time it has a tendency to close on the drill string. Thus, there is a danger when one is not rotating or circulating fluid that the hole will close on the drill string. In Ursa Basin, this began to happen when seawater was in the hole at depths below 50 mbsf. However, when a 10.5 ppg weighted mud was used, this problem was greatly reduced. This allowed us to make prolonged penetrometer measurements. In these cases, the borehole stability was striking. We ran some DVTPP deployments for >1.5 h and experienced no problems with borehole closure. These deployments were far longer than previous deployments of downhole tools in IODP/ODP history. Typically it took 40–70 bbl of weighted mud to be spotted in the hole during a penetration deployment.

Challenges of Measuring Pressure

A critical goal of Expedition 308 was to measure pressure within mudstones using a penetrometer. Two tools were used for this task: the DVTPP and the T2P (Fig. F22). The DVTPP was deployed previously during ODP Legs 190, 201, and 204 (Moore et al., 2001; D'Hondt, Jørgensen, Miller, et al., 2003; Tréhu, Bohrmann, Rack, Torres, et al., 2003). The T2P is a new tool under development as a cooperative effort between MIT, Pennsylvania State University, and IODP-TAMU. The DVTPP and the T2P are similar devices. The primary difference between the two tools is that the T2P has a 6 mm diameter tip, whereas the DVTPP has a ~23 mm diameter tip that rapidly widens backwards from the tip. The T2P was designed both to dissipate more rapidly and to dissipate with a characteristic pressure profile. Both properties allow the T2P to be deployed for shorter periods than the DVTPP in order to interpret in situ pressures.

These penetration tools induce a pressure pulse as they are inserted into the sediment. The initial pressure response and its decay are defined by the insertion rate of the probe, the modulus of the sediment, and the bulk permeability of the sediment. The

pressure dissipation that results after penetration is used to infer in situ pressure and rock properties (Fig. F23A).

Pressure measurements during Expedition 308 were extremely challenging. There were significant successes that allowed us to define the pressure gradient in Ursa Basin. There were a total of 25 T2P deployments and 20 DVTPP deployments (Fig. F24). Of these only 56% of the T2P and 45% of the DVTPP deployments were either fair or good and there were many poor or unsuccessful deployments (Fig. F23). Key problems were threefold. First, in early cases, there was a leak in one of the DVTPP tools and there may have been a leak in one of the T2P tools (e.g., Fig. F23C). The leak resulted in abrupt pressure drops below hydrostatic pressure during the dissipation phase. Second, the T2P was prone to bending due to the very narrow diameter tip. Third, both tools had difficulty remaining coupled to the sediments during deployment in the shallow sections (Figs. F23B, F25). During many of the deployments, after the drill string was raised and subsequent to penetration, there was an abrupt drop in pore pressure. In these cases, there was often a frictional heating pulse associated with the drill string being raised. In addition, the accelerometer in the DVTPP suggests movement of the tool when the drill string was raised. These results are interpreted to record the partial dislodgment of the tool due to friction in the collected delivery system (e.g., Fig. F25). Review of DVTPP records from Legs 201 and 204 suggest that both leakages and tool dislodgement during elevation of the drill string have been a persistent problem with the DVTPP (D'Hondt, Jørgensen, Miller, et al., 2003; Tréhu, Bohrmann, Rack, Torres, et al., 2003).

Synthesis of Brazos-Trinity Basin #4 Geology

Summary of Principal Results

Brazos-Trinity Basin #4 contains a 175 m thick succession of sand-rich turbidite fans, mass transport deposits, and hemipelagic deposits laid down within the last ~122 k.y. Prefan deposits dating back to MIS 6 form a conformable succession of laminated and bioturbated clays deposited from distal turbidity currents and/or river plumes. The initial turbidite deposits in the basin are mud rich, with the exception of the very first turbidity currents to enter the basin. This initial pulse, possibly derived from failure of older shelf edge deposits, accumulated an ~8 m thick sand-rich interval. A basin-wide pause in turbidity current influx spans 30–40 k.y. between late MIS 5 and MIS 4/3. During MIS 3–2, a 130 m thick succession of sand-rich fans accumulated in Brazos-Trinity Basin #4, containing 2–25 m thick packets of very fine to lower medium sand

beds. A 2–3 m microfossil-rich clay marks the end of turbidity current influx into the basin during the Holocene.

Background on the Brazos-Trinity Region

Brazos-Trinity Basin #4 is the terminal basin of a series of bowl-shaped minibasins on the upper–middle continental slope that are linked to late Pleistocene shelf edge deltas by a network of submarine channels offshore Texas (Fig. F4). The fluvial, shelf, and slope portions of the Brazos-Trinity drainage system represent a natural laboratory to investigate the mechanics of sediment transfer across a continental margin from source to sink. Originally studied with sparse seismic records and piston cores (Gardiner, 1986; Satterfield, 1988; Satterfield and Behrens, 1990), the basin has been the subject of numerous detailed studies by the industry and academia (Winker, 1996; Beaubouef and Friedman, 2000; Pirmez et al., 2000; Badalini et al., 2000; Beaubouef et al., 2003; Mallarino et al., in press). Industry studies have focused particularly on the stratigraphic architecture of the intraslope basins because of their similarity with deepwater reservoirs formed on continental margins with a mobile (salt or shale) substrate. The shallow burial depths of such near-seafloor analogs allow for exceptional vertical and spatial resolution through the use of very high frequency (>150 Hz), short-offset seismic profiles. Studies to date have focused on the mapping of sequences using both 2-D grids and 3-D seismic data, resulting in the development of stratigraphic models derived from the interpretation of seismic geometry, acoustic facies, and seismic attributes (Winker, 1996; Badalini et al., 2000; Beaubouef et al., 2003).

Lithologic calibration of these basin-fill models has been limited to short piston cores (e.g., Satterfield and Behrens, 1990). More recently, Mallarino et al. (in press) report on a series of long piston cores in Brazos-Trinity Basin #4, but the recovery was limited to the upper ~5 to ~25 m in the sandy basin fill, although successful cores up to 42 m long were obtained in the basin margins. The basin margin cores enabled Mallarino et al. (in press) to develop a high-resolution chronostratigraphy for the upper part of the basin fill, dating to ~90 ka.

Expedition 308 successfully acquired cores and a full suite of downhole logs that, for the first time, sample the entire infill of Brazos-Trinity Basin #4 and underlying conformable succession along a transect from the basin center to the basin margin (Fig. F6). This unique data set provides a detailed characterization of the sediment gravity

flow deposits and hemipelagic successions within the basin fill and allows for the age dating of the various fan sequences.

Seismic Stratigraphy

The Brazos-Trinity Basin #4 transect was drilled on a dip-oriented seismic line from the basin entry point to the east and across the thickest portion of the basin fill (Fig. F26). The short-offset multichannel seismic line has a frequency content in the range of 100–500 Hz with peak frequency at ~300 Hz (Winker, 1996). Reflector R40 separates two distinct units: a conformable succession of subparallel reflections below and an onlapping succession representing the infill of Brazos-Trinity Basin #4 above. The underlying succession appears to thicken gradually toward the northern basin margin. The basin fill succession displays an alternation of acoustically transparent intervals with packages displaying high-amplitude continuous to semicontinuous reflections. Previous workers interpreted these seismic facies as the result of the alternation between muddy mass transport complexes (transparent intervals) and sandy turbidite fans (bedded intervals) (Winker, 1996; Beaubouef and Friedmann, 2000; Badalini et al., 2000).

Well logs from Sites U1319, U1320, and U1321 are posted on the dip seismic line in Figure F26. The integration between logging-core and high-resolution seismic makes it possible to confidently correlate stratigraphic units up to a few meters thick and to estimate the lateral extent of individual mud and sand packets away from the boreholes (Fig. F27). The match between lithostratigraphic boundaries and most key reflectors in the basin using the preliminary shipboard results is quite good (Fig. F26, F27).

Seismic Reflector R40 represents an angular unconformity at the base of the basin infill and can be traced continuously across the entire area. Seismic Reflector R30 marks an angular unconformity within the basin fill. A thin interval of parallel reflections forms a laterally continuous marker locally disrupted by an acoustically transparent/chaotic unit. Seismic Reflectors R10 and R20 are continuous reflections that separate acoustically transparent/chaotic intervals from intervals of high acoustic amplitude intervals with reflections ranging from laterally continuous to discontinuous. Winker (1996) showed that sediments between Reflectors R40 and R10 are sourced from the western feeder channel and sediments above R10 were sourced from the eastern feeder channel.

Stratigraphic Evolution

A preliminary age model was developed on board by integrating microfossil biostratigraphy together with correlation of magnetic susceptibility and NRM intensity data with global curves (Fig. F28). The chronostratigraphy developed by Mallarino et al. (in press) provided additional constraints for the age model developed onboard. Tephra event Y8 (Drexler et al., 1980, Mallarino et al., in press) occurs in the drilled section, providing an absolute correlation and age marker. The entire drilled succession appears to be younger than 150 ka since the last occurrence (LO) datum of *Helicosphaera inversa* was not observed. The base of the basin infill occurs near the W/X planktonic foraminifer zone boundary, at ~122 ka, and coincides with a ~2 m thick condensed hemipelagic interval. A pause in turbidity current influx also occurs within the basin fill and spans a ~40 k.y. period from ~90 to ~50 ka. The LO of *Globorotalia flexuosa* at ~68 ka is observed at both Sites U1319 and U1320, but based on seismic correlation and the occurrence of *G. flexuosa* within the turbidite infill section at Site U1320, it is possibly the result of reworking by turbidity currents.

Integration of the lithostratigraphy, biostratigraphy, logging characteristics, and seismic stratigraphic correlations are summarized in a structural cross section (Fig. F29). Examples of core photographs of the lithofacies encountered in each of the Brazos-Trinity Basin #4 sequences are illustrated in Figure F30.

The following summarizes the basin stratigraphic architecture and evolution, from oldest to youngest:

Prefan Sequence

All three sites penetrated a succession of laterally extensive subparallel reflectors below seismic Reflector R40 at the base of the basin infill. This succession is composed of terrigenous laminated clay with color banding between grayish green and reddish brown with varying degrees of bioturbation (Fig. F30E). These clays have a low TOC (average = 0.5 wt%) but are rich in CaCO₃ (average = 23 wt%), most of which is associated with fine-grained detrital carbonate and dolomite. The unit is devoid of sand and contains very rare silt lamina.

The 125 m thick prefan deposits cored at Sites U1319 and U1320 are interpreted to be younger than 150 ka and were deposited at an average rate of >4 m/k.y. This succession is interpreted to represent deposition from distal turbidity currents overspilling from basins adjacent to Brazos-Trinity Basin #4 (laterally and/or updip), possibly with

a significant contribution from sedimentation from surface plumes of coastal rivers. It is unclear at this stage whether these slope deposits contain a record of spillover from updip basins or whether they represent distal turbidity currents from adjacent basins at a time when shelf edge deltas of the Brazos-Trinity drainage system were located to the east and/or west of Basin #1.

Hemipelagic Drape—Base of Infill

Capping the prefan deposits there is a ~2 m thick intensely bioturbated microfossil-bearing clay recovered at Site U1319 (Fig. [F30D](#)). At Site U1320, the same interval occurs within a zone of poor core recovery. This condensed sedimentation interval marks a dramatic reduction of terrigenous sediment flux to the basin and occurs at the base of the onlap fill of Brazos-Trinity Basin #4. We interpret this condensed interval to represent the sea level highstand during MIS 5e. Seismic correlation of the regional seismic Reflector R40 between the two sites indicates that this condensed interval represents the base of Brazos-Trinity Basin #4 infill.

Lower Fan—Seismic Reflectors R40–R30

The lower fan unit in Brazos-Trinity Basin #4 thins very gradually onto the basin margin, from 30 m at Site U1320 to ~10 m at Sites U1321 and U1319. The sequence is dominated by laminated and bioturbated muds with thin beds of silt and sand (Fig. [F30C](#)). Sand content decreases from ~23% at Site U1320 to only a few percent at Site U1319. Most of the sand occurs in a ~8 m thick interval of poor recovery at the base of the lower fan at Site U1320, as interpreted from the well logs. This basal sand displays a significant lateral variation in thickness along the 20 m separating Holes U1320A and U1320B and probably represents the infill of an erosional scour or channel. Excluding this basal sand, the lower fan has a sand content of only 8%.

The mud-rich lower fan was deposited between ~120 and ~90 ka. The first pulse of sandy turbidity currents appears to have occurred within MIS 5e or at the rapid sea level fall event marking the MIS 5e–5d transition. At that time, sea level was still higher than today and the coastline was far landward of the modern shelf edge. The source of this initial pulse of turbidites is inferred to result from remobilization of shelf edge sediments deposited from previous sea level lowstands or from submarine failures in the updip basins.

Hemipelagic Drapes—Base of Middle Fan

The lower fan is capped by an ~8 m thick interval of foraminifer- and nannofossil-bearing clay displaying intense bioturbation, similar to the hemipelagic drape at the base of the lower fan (Fig. F30B). Near the base of this hemipelagic drape, a 2 cm thick layer of volcanic glass shards is observed at both Sites U1319 and U1320. This ash layer provides an independent correlation and age marker confirmed by the *Emiliana huxleyi* acme in close proximity to the ash. This ash layer is interpreted as tephra event Y8, representing the outfall from the Los Chocoyos (Guatemala) eruption at 84 ka (Drexler et al., 1980; Mallarino et al., in press). Seismic Reflector R30 occurs at the top of this interval and can be laterally traced over most of the basin.

The duration of this basin-wide pause in sediment flux to Brazos-Trinity Basin #4 cannot be determined precisely without additional shore-based analyses of the material recovered, particularly magnetic and isotope stratigraphies. Mallarino et al. (in press) indicate that the pause in turbidite sedimentation may have lasted into early MIS 3, but earlier MIS 4 turbidites may not have reached the basin margin core site that Mallarino et al. (in press) studied. The paucity of terrigenous input into the basin during this interval, despite significant oscillations in sea level, is interpreted to indicate that either fluvio-deltaic input was directed away from the head of the system near Basin #1 or that turbidity currents were completely trapped in updip Basins #1 and #2.

Middle Fan—Seismic Reflectors R30–R10

The middle fan comprises a succession of sediment gravity flow deposits including massive and normally graded fine to lower medium sand beds up to several meters thick interbedded with thinly laminated muds and silts.

The middle fan thins from ~110 m at Site U1320 to ~50 m at Site U1321 and to ~12 m at Site U1319, illustrating the strong effect of basin margin topography on sand distribution. The lower part of the middle fan is represented by a very thin interval at Sites U1321 and U1319, whereas the upper part of the fan succession reaches higher onto the basin margin. At the base of the middle fan, an acoustically transparent interval corresponds to a slump/debris flow deposit containing contorted beds and mud clasts. This slump unit originates from the basin margin to the east (Winker, 1996).

Average sand content of the middle fan unit is ~40% at Site U1320, ~80% at Site U1321, and only minor amounts of sand were recorded at the basin margin Site U1319. Sand distribution within the middle fan, however, is quite variable both ver-

tically and spatially. At Site U1320, sand beds are organized in 2–10 m thick packets with an overall increase in sand content upward, particularly above seismic Reflector R20. The sand packets are capped by muds and intervals of laminated mud with thin bedded silts and sands. Some of these muddy intervals can be correlated across the transect, whereas others are either eroded away or pinch out between boreholes (Fig. F29).

The upper portion of the middle fan, above seismic Reflector R20, is the sandiest interval of the entire basin fill with amalgamated sand beds forming a 25 m thick unit at Site U1321 (Fig. F29). This interval is also remarkably transparent on seismic data reflection profiles (Fig. F26). At Site U1320, a sharp contact between a thick-bedded sand packet above a laminated, partly contorted interval of mud with thin beds of silt and sand correlates with a subtle seismic reflection. At Site U1321, this acoustically transparent interval is composed of ~100% sand. Subtle reflections on the seismic lines suggest that the basal mud unit at Site U1320 is most likely eroded by channels and scours and is completely absent at Site U1321 (Figs. F26, F27).

Previous basin models derived from seismic facies analyses interpreted this transparent unit as muddy mass transport deposits (e.g., Winker, 1996; Badalini et al., 2000; Beaubouef and Friedmann, 2000; Beaubouef et al., 2003). Detailed logging-seismic-physical property analyses on shore are needed to unravel the low impedance contrasts within these shallowly buried muds and sands.

Capping the middle fan is a ~10 m thick organic-rich homogeneous dark green to black clay with a sharp base and top. This unit thins onto the basin margin but appears to extend across the entire basin fill (Figs. F26, F27). It is interpreted to represent a debris flow deposit.

Upper Fan—Seismic Reflector R10 to Seafloor

The upper fan comprises a sand-rich unit forming a tapered wedge across the basin. At Site U1320 it is ~25 m thick and contains thick and medium beds of fine and very fine sand. The upper fan thins to ~18 m at Site U1321 and has similar logging characteristics but a slightly lower sand content than at Site U1320. The correlative unit at Site U1319 is only ~3 m thick and is mostly mud with some thin beds of silt and sand. Sand beds in the upper fan are organized in bed packets ranging in thickness between 2 and 8 m capped by intervals of mud with thin beds. Correlation to seismic profiles (Fig. F27) shows that the sand packets represent mounded seismic bodies with internally discontinuous reflections representing fan lobes extending laterally for sev-

eral kilometers. Beaubouef et al. (2003) show spectacular high-resolution 3-D images from these channelized fan lobes. The upper fan is capped by a microfossil-rich clay, indicating that turbidity current deposition ceased in the basin during the last sea level rise.

The upper and middle fans were deposited between ~47–60 and ~10 ka and represent the main pulse of turbidity current influx into Brazos-Trinity Basin #4. This implies an average accumulation rate between 2.5 and 3.5 m/k.y. for the 130 m thick succession at Site U1320, compared with an average accumulation rate of ~0.2 m/k.y. at the basin margin Site U1319. Terrigenous influx was reduced dramatically throughout Brazos-Trinity Basin #4 during the Holocene as indicated by the presence of a microfossil-rich clay in the upper 2–3 m of the sediment column at both Brazos-Trinity Basin #4 sites.

Conclusions on the Evolution of Brazos-Trinity Basin #4

Sedimentation in Brazos-Trinity Basin #4 is the result of a complex interaction between fluvio-deltaic dynamics, sea level changes, and interactions between turbidity currents and submarine topography. During the low sea level period corresponding to MIS 6, the basin received significant input of terrigenous sediments, but a complete absence of sand and silt indicates that either turbidity currents were filling basins updip or that deltaic systems were positioned in areas adjacent to the Brazos-Trinity slope at the time.

During the stepwise sea level fall between MIS 5e and 2, the basin received as much as 175 m of sediment gravity flow deposits comprising turbidites, slumps, and debris flows. A pause in turbidite deposition occurred from MIS 5a to ~MIS 4. This period comprised both a relative rise and a relative fall in sea level. Therefore the lack of turbidite influx into Brazos-Trinity Basin #4 must be the result of factors other than sea level changes, including lateral shifts in the sediment source on the shelf or trapping of sediments in Basins #1 or #2 updip preventing the spillover of turbidity currents into Brazos-Trinity Basin #4.

Seismic facies-based interpretations of the basin fill architecture by previous authors are often contradictory, and our results provide the needed calibration to validate these interpretations. Seismic intervals that show abrupt onlap onto the basin margins generally correspond to sand-rich turbidites (e.g., middle fan above Reflector R30), whereas those seismic units that have a gradual thinning pattern onto the basin margin tend to have lower sand content (e.g., lower fan between Reflector R40 and

R30). The acoustically transparent units observed in the basin fill are composed of very high sand content, ranging from 50% to ~100%, contradicting previous interpretations (e.g., Badalini et al., 2000; Beaubouef and Friedman, 2000; Beaubouef et al., 2003).

Mud-rich turbidite intervals appear to extend laterally for significant distances across the basin and rise as much as ~50 m above the basin floor. This could result from turbidity current run-up onto the basin margins or represent a measure of the thickness of turbidity currents entering the basin. However, some of the relief, perhaps as much as 20 m, appears to result from subsidence at the basin center since the onset of basin filling.

Overall, the sand content in the basin fill increases upward with the lowest sand content observed in the lowermost fan (~23%), but there is significant spatial variability in the profiles. The highest sand content is encountered in the southernmost edge of the basin at Site U1321, in the upper part of the middle fan. The sand content of the upper fan is high (~60%–70%), but not as high as the upper part of the middle fan (77% to ~100%). Although the general increase in sand content could be interpreted as the result of progressive sea level fall and advance of the Brazos-Trinity fluvial systems toward the shelf edge (e.g., Mallarino et al., in press), it is clear that lateral shifts in deltaic depocenters and trapping of sands in the updip basins also have an important influence in sand influx into Brazos-Trinity Basin #4.

Synthesis of Ursa Basin Geology

Drilling at Sites U1322, U1323, and U1324 investigated a sedimentary wedge flanking a buried submarine channel of the modern Mississippi Fan, the Southwest Pass Canyon channel-levee system (Fig. F31). Of the two cored sites, Site U1324 penetrated the thickest part of the east levee. Site U1322, 12 km east, penetrated the thinner portion of the levee. The core descriptions and age results of these two sites, along with the lithostratigraphic column interpreted from the LWD data at Site U1323, provide the basis to evaluate the diverse sedimentary history of this system.

Age Constraints

Nannofossils and planktonic foraminifers indicate that the sediment sequence recovered at Sites U1322 and U1324 was mainly deposited over the last 60 k.y. A good correlation can be made between the two sites using faunal assemblage zones and species datums (Fig. F32).

Sediment sections corresponding to lithostratigraphic Subunits Ib (lower part) to Id at both sites (30–130 mbsf at Site U1322 and 30–170 mbsf at Site U1324), between seismic Reflectors S10 and S30, are dated by planktonic foraminifers belonging to MIS 2 (10–25 ka). The age control points are rare from the lower part of Holes U1322B and U1324B. However, fairly reliable planktonic foraminifer data indicate an MIS 3 age for sediments recovered from 130 to 190 mbsf at Site U1322 and from 170 to 329 mbsf at Site U1324. Farther downhole, biostratigraphic constraints are inadequate to correlate between the two sites. The nonoccurrence of some datums older than 65 ka provides negative evidence that the sediment from the lowermost part of Sites U1322 and U1324 is younger than 65 ka. The rarity of microfossils in the lower part of the drilled section provides little specific information regarding species datums but does suggest that the sediment interval was deposited during sea level lowstands belonging to MIS 4 (~60–65 ka). Results from previous studies, including Winker and Booth (2000), indicate that the last occurrence datum of *G. flexuosa* (68 ka) lies at the base of the Blue Unit, which is ~200 m deeper than the bottom of either Hole U1322B or Hole U1324B. Therefore, we believe that the sediment sequence recovered at both sites in Ursa Basin was deposited in the last 60 k.y., during MIS 1–4.

Correlation and Sedimentary History

The upper 160 m of Site U1324 and the upper 135 m of Site U1322 are remarkably similar. They consist of mud, clay, and two mass transport deposits (Fig. F31). The base of these intervals ties closely with the regional seismic Reflector S30 and is dated at 24 ka. Sedimentation rates during the accumulation of these correlative intervals at both Sites U1324 and U1322 were similar, ranging from 10 to 12 m/k.y., and declining to lower rates in the uppermost Holocene (Fig. F32).

The base of the cored sections of Sites U1324 and U1322 tie closely with seismic Reflector S60 (Fig. F33), which we believe to be ~60 ka based on shipboard biostratigraphic and magnetostratigraphic analyses (Fig. F32). S60 is a reflector within the Ursa Canyon east and west levee and therefore should have been deposited approximately synchronously.

Although the upper portions of Sites U1322 and U1324 are similar, sections below show lithologic contrasts. Between seismic Reflectors S60 and S40-1324 at Site U1324, lithostratigraphic Unit II contains interbedded sand, silt, and mud, representing relatively unconfined flow turbidites deposited by a developing channel system. Above seismic Reflector S60 at Site U1322, lithostratigraphic Unit II contains a series of

stacked clay- and mud-rich mass transport deposits with a marked paucity of sand and silt. Apparently, the Ursa Canyon channel-levee system acted as a barrier that confined sand and silt at Site U1324 and effectively shielded Site U1322 from deposition. The Ursa Canyon system would have had considerable topographic relief on the seafloor which would have confined sands, silt, and mud to the west during the accumulation of lithostratigraphic Unit II at Site U1324. Many seismic reflectors within the upper part of lithostratigraphic Unit II climb to the east up and over the top of the Ursa Canyon channel-levee system; therefore, we interpret there was very little accumulation at Site U1322 before sediment breached the height of the Ursa Canyon system.

Mass Transport Deposits and Westward Retrogressive Failure

During Expedition 308, we examined numerous cores containing mass transport deposits. Inclined bedding planes, folds, and faults commonly characterize mass transport deposits (Fig. F34). Mass transport deposits are recognized seismically by their discontinuous to chaotic reflections of transparent to variable amplitude (Fig. F34). Logging curves typically show positive anomalies in density and resistivity at the top of, and within, mass transport deposits (Fig. F34). The resistivity-at-the-bit logging images reveal striking folds and faults associated with mass transport deposits and suggest north to south sediment transport.

The seismic cross section and the contrasting lithostratigraphic columns at Sites U1322 and U1324 suggest mass transport deposition was more active earlier to the east and progressively migrated upsection and to the west. The more rapid accumulation of sediments in the basal portion of Site U1324 relative to Site U1322 may have created a thickness imbalance that could have expelled pore fluid to the east, initiating failure. The overpressured sands that created operational problems while drilling Site U1323 may represent a fingerprint of this process of lateral expulsion of fluids.

Physical Properties in Brazos-Trinity #4 Basin and Ursa Basin

Analysis of bulk density and porosity profiles suggests overpressure in the lower lithostratigraphic units near the depocenter of Brazos-Trinity Basin #4 (Site U1320) and throughout Ursa Basin (Sites U1322, U1323 and U1324). The magnitude of the overpressure is here defined as

$$\lambda^* = (P - P_h) / (\sigma_v - P_h), \quad (1)$$

where

P = pore pressure,
 P_h = hydrostatic pressure, and
 σ_v = total vertical stress.

Brazos-Trinity Basin #4

Lithostratigraphic Unit V at Site U1320 and lithostratigraphic Unit VI at Site U1319 (both below Reflector R40) are equivalent stratigraphic sections that have been subject to different burial histories. Above Reflector R40 at Site U1320, there is 178 m of overburden represented by the ponded infill of the Brazos-Trinity Basin #4. In contrast, at Site U1319, located on the basin's flank, there is only a few meters of overburden. Immediately below Reflector R40, porosities are ~65% at Site U1319 and ~50% at Site U1320. At the bottom of the holes at both sites porosities are ~40%, although the overburden is higher at Site U1320 than at Site U1319 (Fig. F35).

Porosity (ϕ) relates to void ratio (e) by the formula

$$e = \phi / (100 - \phi). \quad (2)$$

The pore pressure at Site U1320 is estimated from the differences in void ratio with respect to the hydrostatic effective stress (Fig. F36) using the formula

$$P = \sigma_v - 10^{(e_0 - e)/C_c}, \quad (3)$$

where

P = pore pressure predicted from the void ratio,
 σ_v = total vertical stress,
 e = measured void ratio,
 e_0 = reference void ratio (3.49), and
 C_c = compression index (0.89).

Reference void ratio and compression index constants are derived from the curve fit of the data from Site U1319 in Figure F36. This approach is derived from standard geotechnical practice (e.g., Lamb and Whitman, 1969). We predict the difference in pore pressures between Sites U1319 and U1320 based on the assumption that both locations have similar stress-strain properties, that sediments at Site U1319 are normally

pressured, and that sediments at both locations are normally consolidated (i.e., their in situ effective stress is their maximum past effective stress).

The overpressure at Site U1320 that is estimated from the differences in void ratio with Site U1319 is approximately $\lambda^* = 0.7$ (Fig. F36). This contrasts with the last value measured by the T2P, which recorded an overpressure $\lambda^* = 0.2$. Further consolidation tests in the laboratory and refined analysis of the T2P and DVTPP pore pressures will refute, refine, or confirm these estimates.

Ursa Basin

In Ursa Basin, lithostratigraphic Subunits Ia–Id are the same lithostratigraphic units at Sites U1322, U1323, and U1324. Lithostratigraphic Subunits Ib and Id are slump deposits, whereas lithostratigraphic Subunits Ia and Ic are not disturbed. The lithostratigraphic units below Reflector S30 are not equivalent at each site, and thus comparison is difficult. The thickness of the strata between the seafloor and Reflector S30 is 124 m at Site U1322, 197 m at Site U1323, and 165 m at Site U1324. Lithostratigraphic Subunits Ia–Id have a similar overburden at all three sites and have comparable lithology and depositional history, although the accumulation rate is higher at Site U1322 than at Site U1324.

Sites U1322, U1323, and U1324 have similar porosity and bulk density in lithostratigraphic Unit I and therefore similar consolidation states (Fig. F37). The porosity profiles from the three sites show similar trends with a relatively rapid decrease in porosity from 80% at seafloor to 55% in lithostratigraphic Subunit Ia (above seismic Reflector S10). Then, a gentler gradient is observed down to the bottom of the hole, with the lowest porosities at ~45%.

It is assumed that lithostratigraphic Subunit Ic at Site U1324 is hydrostatically pressured. The amount of overpressure at Sites U1322 and U1324 can be estimated through equation 3. The reference void ratio ($e_0 = 3.32$) and compression index ($C_c = 0.81$) are obtained from the void ratio versus vertical effective stress plot of lithostratigraphic Subunit Ic at Site U1324 (Fig. F38). The estimated overpressure is $\lambda^* = 0.4$ – 0.5 of the vertical effective stress below Reflector S30 at Site U1322 and is $\lambda^* = 0.6$ – 0.7 at Site U1324 (Fig. F38). The predicted pore pressures fit along the last recorded in situ pore pressure measurements from the T2P and DVTPP measurements. Further consolidation tests in the laboratory and refined analysis of the T2P and DVTPP pore pressures will refute, refine, or confirm those estimates.

At Site U1322, bulk densities are greater in slumps than in material that is not a part of a slump deposit (Fig. F37). The bases of slump deposits typically show lower porosities than the non-slumped intervals immediately below. These variations in porosities are accompanied by differences in undrained shear strength (e.g., Fig. F16), with slumps typically showing higher values than non-slumped deposits. The higher consolidation is inferred to result from the reformation of the originally loose sediments into a more dense structure by dewatering during the landslide process. It is also observed that porosity and undrained shear strength at the top of the slumps does not vary significantly with respect to the in situ sediments above. This might imply that dewatering and consolidation preferentially takes place at the base of the slump where shearing is most likely.

Subunits Id and Ib correspond to the same slump intervals at Sites U1322 and U1324. The general trend in porosity and undrained shear strength was similar at both sites. However, the porosity and undrained shear strength profiles at Site U1324 (Fig. F18) show more subdued variations (or no variation at all) between slumped and non-slumped units than those at Site U1322 (Fig. F16). We speculate that at Site U1324, upslope on the Mississippi Canyon levee, the total shear deformation may have been less than at Site U1322, in the center of the basin. The higher shearing at Site U1322 might then translate into a higher degree of consolidation.

Within the non-slumped units, some layers appear to have high porosity and water content. An example is the interval that correlates with Reflector S30 (~160 mbsf at Site U1324) at the base of lithostratigraphic Subunit Id, a 35 m thick slump deposit (Fig. F37). These layers might have significant overpressure and then have acted as weak layers along which landslides initiated.

Brazos-Trinity Basin #4 versus Ursa Basin

The porosities in Brazos-Trinity Basin #4 and Ursa Basin show similar trends with depth (Fig. F39). The porosities in Ursa Basin are slightly lower in the uppermost 100 m of the sediment column and then decrease more gradually with depth than those in Brazos-Trinity Basin #4. It is not clear if the differences in the porosity trends are due to the differences in lithology at the two different locations, the difference in vertical effective stress, or a combination of these factors.

The results that can be obtained now are quantitative, but relative estimates are based on several assumptions. The processing of the pore pressure measurements (see “Downhole Logging”) from the T2P and DVTTP, as well as the consolidation tests in

the laboratory, will provide a better perspective of the overpressures at both basins and their hydrogeological regimes.

Geochemical Indicators of Fluid Flow

The geochemistry of sediment pore water is indicative of the composition of the sea-water trapped during sedimentation and is influenced by post depositional diagenetic transformation and mixing with new water masses. As such, it is a potentially useful means of tracing fluid flow in Brazos-Trinity Basin #4 and Ursa Basin. The 93 interstitial water samples collected from Brazos-Trinity Basin #4 (51 at Site U1319 and 42 at site U1320) and the 124 samples from Ursa Basin (49 from Site U1322 and 75 from Site U1324) were analyzed shipboard for alkalinity, pH, salinity, chlorinity, sulfate, phosphate, ammonium, silica, Na, K, Mg, K, B, Li, Sr, Ba, Fe, and Mn concentrations (Figs. [F40](#), [F41](#)).

Based on the fact that the maximal variation of the different tracers (Figs. [F40](#), [F41](#)) is limited to the sediments of the first 30 mbsf in Brazos-Trinity Basin #4 and the first 100 mbsf in Ursa Basin, we infer that organic degradation and microbially mediated reactions were restricted to these intervals. The pattern of anaerobic degradation of organic matter and the pore water redox conditions in both basins are characteristic of deep marine sediment diagenesis (e.g., Schulz, 2000). The sulfate-methane interface (SMI) occurs at shallower depths in Brazos-Trinity Basin #4 Sites U1319 (SMI = 15 mbsf) and U1320 (SMI = 22 mbsf) than in Ursa Basin Sites U1322 (SMI = 74 mbsf) and U1324 (SMI = 94 mbsf). We infer that this difference is mainly driven by the higher sedimentation rates at Ursa Basin compared to Brazos-Trinity Basin #4. Pore water SO_4 and Mn concentrations within the sulfate reduction zone show a strong antithetical relationship at all sites. Ammonium concentration at the Ursa Basin sites increases with depth, suggesting that more reducing conditions may have existed at these locations relative to sites in Brazos-Trinity Basin #4.

Alkalinity has a maxima at ~35 and 25 mbsf at Sites U1319 and U1320, respectively, in Brazos-Trinity Basin #4 and at ~26 and 47 mbsf at Site U1322 and U1324, respectively, in Ursa Basin. This maxima in alkalinity correlates with pore water increases in Ca, Sr, B, and Li concentrations (Figs. [F40](#), [F41](#)). We interpret this relationship as indicating diagenetic carbonate dissolution at shallow depths.

The initial pore water chemistry results obtained during Expedition 308 seem to indicate the presence of hydrogeologic flows in the overpressured sediments of Ursa Ba-

sin and Brazos-Trinity Basin #4. The strongest evidence supporting the presence of fluid flow is that seismic reflectors are often associated with pronounced changes in pore water chemistry, both in Brazos-Trinity Basin #4 and Ursa Basin (Figs. F40, F41). This suggests that seismic surfaces occur along permeable stratigraphic horizons that acted as conduits focusing lateral fluid migration. At Site U1320 in Brazos-Trinity Basin #4, the changes in pore water chemistry are mainly related to seismic Reflectors R10 and R30, whereas at Site U1319, which is a more condensed sedimentary section located at the steep margin of the basin, these changes are restricted mostly around Reflector R30 (Fig. F40). Below Reflector R30, some of the element concentrations also show similar spikes associated with seismic reflectors such as the Cl minimum between Reflectors R50 and R60. This minimum may indicate lateral migration of slightly fresher fluid at this particular strata (Fig. F40). At Site U1324 in Ursa Basin, changes in pore water chemistry equivalent to those described above in Brazos-Trinity Basin #4 are centered around Reflector S10 and below Reflector S30 (Fig. F41). At Site U1322, the chemical changes around Reflector S10 are similar to those observed at Site U1324, but the changes below Reflector S30 are less pronounced (Fig. F41).

Further evidence of fluid flow is provided by downhole variations in chloride concentration within Ursa Basin. Site U1322 exhibits a near linear decrease in chlorinity from the seafloor to terminal depth ($y = 3.7e^3 - 6.5x$; $R^2 = 0.68$) (Fig. F41). Initial concentrations are identical to seawater concentration of 559 mM, increase rapidly to 578 mM at 15 mbsf and then decrease to 542 mM at the base of the hole. This gradual pore water freshening may indicate mixing between overlying seawater and fluids from the Blue Unit. Alternatively, dewatering of clay-rich lithologies during diagenesis may also produce freshening of pore waters. However, we suggest this latter possibility is less likely as we did not observe a similar decrease in chlorinity with depths at Site U1324, which must have experienced more intense burial diagenesis as it was buried deeper (maximum drilling depth was 600 mbsf versus 238 mbsf at Site U1322).

In summary, chemical pore water profiles in Brazos-Trinity Basin #4 and Ursa Basin record a combination of processes, which includes anaerobic degradation of organic matter, carbonate dissolution and precipitation, and lateral fluid migration. We propose that most of the chemical changes in pore waters discussed above are driven by lateral fluid flow. Though postcruise work will provide higher resolution data and better constraints, we interpret the data as showing two fluid flow pathways: 1) above Reflector S30, a shallow fluid flow system possibly related to recharge of seawater or other shallow circulated fluids in the basin, and 2) a deep-seated fluid flow that took place below Reflector S30 and that could be linked to an overpressured unit such as

the Blue Unit in Ursa Basin. We stress, however, that this interpretation is preliminary, and postcruise work will serve as a test for this working hypothesis.

Preliminary Interpretation of Overpressure and Hydrodynamics in Ursa Basin

Overview

In the mudrocks above the Blue Unit in Ursa basin, porosity declines rapidly in the uppermost 100 m and subsequently declines only slightly. Pressure predictions based on porosity suggest overpressures with a normalized overpressure ratio (λ^*) >0.6 . Direct pressure measurements also record overpressures with $\lambda^* > 0.5$. At equivalent depths, pressures (as recorded by both consolidation and direct measurements) are slightly greater to the east at Site U1322 where the overburden is thin than to the west at Site U1324 where the overburden is thick. The temperature gradient is significantly greater at Site U1322 ($26^\circ\text{C}/\text{km}$) than to the west at Site U1324 ($18.4^\circ\text{C}/\text{km}$). Sedimentation rates at Site U1324 were almost 3 times greater than at Site U1322. A conceptual model that links these observations is that there is upward flow everywhere within the overburden above the Blue Unit; the flow rate is constant, reflecting a constant overpressure gradient, at each site. However, significant lateral flow within the Blue Unit must also be present to account for the similar overpressure gradient at the two locations (despite the threefold difference in sedimentation rate) and the elevated heat flow emanating from the Site U1322 location.

Permeability Architecture

Sediments deposited in the last ~ 70 k.y. in Ursa Basin can be divided into three successive depositional units: the Blue Unit, the Ursa and Southwest Pass Canyons channel-levee systems, and distal fan and hemipelagic deposition (Fig. **F10**).

The Blue Unit forms a regional permeable unit that is composed of interbedded thick sands (some >50 m thick) and mudstone. Its base is the base of the deepest sand, which ties to a weak negative amplitude within the shallow sedimentary section (Fig. **F9**, **F10**). Its top ties to a strong positive seismic amplitude that marks an increase in impedance with depth at the top of sands within the Blue Unit. In places, the thick Blue Unit sands are truncated by the Ursa channel (Fig. **F10**).

The Ursa Canyon channel-levee system has high-amplitude chaotic seismic reflections that most likely are permeable sands. However, the bounding deformation zone

is dominated by mudstone and contains rotated slump blocks within the Blue Unit where the channel has incised into the Blue unit.

Low permeability mudstones cap the channel-levee systems and are thicker to the west (Site U1324) than to the east (Site U1322). Multiple slope failures are present in this section with more to the east in the vicinity of Site U1322 (Fig. F33).

Sedimentation Rate: Driving Force for Fluid Flow

Sedimentation drives overpressure. Sedimentation rates in Ursa Basin are extremely rapid and have significant lateral variation (Fig. F32). On average, the sedimentation rate across the entire interval is ~2.6 times greater at Site U1324 than at Site U1322 (10 versus 3.8 mm/y). Late Pleistocene sedimentation rates varied ~2.8-fold (9.6 versus 3.5 mm/y). The detailed age model at both sites will be strengthened with further shore-based work. However, this work suggests that at the base of Site U1324 sedimentation rate exceeded 25 m/k.y. and at Site U1322 it exceeded 16 m/k.y.

Pressure Predicted from Consolidation State above the Blue Unit

A striking feature of the three sites (U1322, U1323, and U1324) is that the porosity at equivalent depths is similar (Fig. F42). For ~50 m there is a rapid decline in porosity from ~80% to ~60%. Thereafter porosity declines at a lower rate with depth to the bottom of the hole. We predict pressure from porosity (see “**Physical properties in Brazos-Trinity Basin #4 and Ursa Basin**”) and find elevated pressures beneath 125 mbsf at Site U1322 and beneath 150 mbsf at Site U1324 (Fig. F43). The overall pressure ratio (λ^* , the fraction of the hydrostatic stress [equation 1]) is ~0.5–0.6 at each location.

In Situ Pressure and Temperature

Pressure

We made multiple penetrometer measurements with the T2P and the DVTTP (Fig. F44). We have not processed these data and we have only posted the final pressures recorded at the end of the deployment. There is considerable scatter in these data (see “**Challenges of Measuring Pressure**”). None the less, several clear trends are present. At both locations, multiple measurements of in situ pressure record significant overpressures. Second, pressures between 100 and 250 mbsf are somewhat higher at Site U1322 than they are at Site U1324 (Fig. F44). This is intriguing because the porosity at these two sites is very similar at equivalent depths; thus, this difference is not pre-

dicted from the porosity-based pressure prediction. Deep at Site U1324, pore pressures rise to a λ^* value between 0.5 and 0.6.

Temperature

A striking observation is that the temperature gradient at Site U1324 is 18.4°C/km, whereas it is 26.2°C/km at Site U1322 (Fig. F45). These data were acquired by APCT, T2P, and DVTTP measurements. The APCT measurements were corrected to estimate the actual temperature from the measured temperature; the DVTTP data and the T2P data have not been corrected. Thermal conductivities at the base of Site U1324 are ~1.2 W/m·K, whereas they are ~1.15 W/m·K at Site U1322. If the heat flow is vertical and conductive, this implies a heat flow of ~22 mW/m² at the base of Site U1324 versus ~30 mW/m² at the base of Site U1322.

There are several possible explanations for the ~1.4-fold increase in heat flux at the base of Site U1322 relative to that at Site U1324. First, sedimentation is inversely correlated to heat flow (Wang and Davis, 1992). Thus, the increased thermal gradient at Site U1322 relative to Site U1324 may result from the fact that at Site U1322 the system is closer to thermal equilibrium, whereas at Site U1324 sedimentation was so rapid that it has outpaced the heat flow. A second possibility is that local variations in the proximity to salt bodies have significantly affected the local geothermal gradient. A final possible interpretation is that the heat flow entering the mudstone above the Blue Unit is greater at Site U1322 than at Site U1324 because there is lateral transfer of heat as described below.

Conceptual Hydrodynamic Model

Figure F46 illustrates our initial conceptual model for flow within Ursa Basin. After deposition of the Blue Unit, it was incised by the Ursa channel-levee system and then rapidly buried by mud. Sedimentation rates were extraordinarily rapid and the sedimentation rate at Site U1324 was almost three times that at Site U1322. One-dimensional flow modeling would suggest that the overpressure and upward flow rate should be greater at Site U1324 than at U1322 because the sedimentation rate is so much higher at Site U1324. However, the presence of similar overpressure gradients within rocks of similar lithology (and presumably similar hydraulic conductivity) implies that the upward flux of water is approximately equal at each location. To equalize these pressure gradients, given the very different sedimentation rates, we infer some flow must occur laterally within the Blue Unit (Fig. F46). The temperature gradient at Site U1322 is significantly greater than at Site U1324, which implies a con-

ductive heat flux that is 1.4 times greater at Site U1322 than at Site U1324 (Figs. F45, F46A, F46B). The elevated temperature gradient at Site U1322 may reflect lateral transfer of heat by advection within the Blue Unit (Fig. F46).

The overpressure encountered at the base of Site U1324 is significantly larger than at Site U1322 (3.1 versus 1.3 MPa) (Fig. F46). Early models suggested that the entire Blue Unit might be in hydrologic communication and that there would be a single overpressure encountered in both locations. More detailed analysis illustrates that the Blue Unit is composed of multiple sand bodies that have significant lateral extent (Fig. F46). These sands are truncated by the Ursa channel deformation zone, which has deformed the underlying Blue Unit. In the western location (Site U1324), the top of the Blue Unit has been eroded and only the deeper beds are present.

Based on pressure data analyzed here and more detailed regional seismic mapping, we interpret that only the basal sand within the Blue Unit has communicated laterally from Site U1324 to Site U1322. In this basal sand, flow is driven laterally toward Site U1322, underneath the Ursa channel-levee system. Within the Blue Unit at Site U1322, vertical flow will occur between the sand beds; however, there will be a large vertical pressure gradient within the shales between the sand beds. The impedance of these shale layers reduces the pressure from ~3.1 MPa at the base of the Blue Unit to ~1.3 MPa at the top of the Blue Unit (Fig. F46). These observations illustrate the critical importance of being able to sample the pressure field within the Blue Unit in order to fully understand this hydrodynamic system. This is the fundamental goal of the second component of the Gulf of Mexico Hydrogeology proposal.

OVERVIEW OF EXPEDITION ACHIEVEMENTS AND PRELIMINARY SCIENTIFIC ASSESSMENT

Original Objectives

We address the expedition achievements in light of the six original scientific objectives of Expedition 308 (see Introduction).

- 1. Document how pressure, stress, and geology couple to control fluid migration on passive margins.*

Our goal was to establish the vertical and lateral variation in pressure and rock properties above the Blue Unit to test the flow-focusing model and image the flow system within the mudstone capping the Blue Unit.

A fundamental achievement of the expedition is that we established the overpressure profile as a function of depth at two key locations in Ursa basin: Site U1322 and U1324 (Fig. F44). These measurements were difficult and we had a high failure rate (see **“Challenges of Measuring Pressure”**); however, ultimately we acquired enough data to constrain the overpressure field above the Blue Unit. To our knowledge, this is the first time in DSDP/ODP/IODP history that the spatial variation of the pressure field has been documented at this resolution. Previous deployments of the DVTTP generally yielded only single measurements in boreholes. We also acquired an extraordinary temperature data set that documented striking differences in temperature gradient between Sites U1322 and U1324 (Fig. F44). We also took an extensive amount of whole core for geotechnical analysis. Geotechnical experiments on these cores will further constrain the in situ pressure through analysis of the preconsolidation stresses. Modeling of the DVTTP and T2P pressure dissipation profiles will also further constrain the pressure field.

Our initial observations suggest both lateral and vertical flow are present within the Blue Unit. A fundamental result is that the pressure gradient at the two sites (U1322 and U1324) are similar despite the large difference in sedimentation rate at these locations. We infer that the hydrodynamic flow field within the Blue Unit is more complicated than originally envisioned (Fig. F46) (see **“Preliminary Interpretation of Overpressure and Hydrodynamics in Ursa Basin”**). Ultimately, to understand the flow field within and around the Blue Unit, it will be necessary to sample the pressures within the Blue Unit sands.

We acquired whole core at Sites U1322 and U1324, LWD/MWD logs at Site U1322, U1323, and U1324, and wireline logs at Site U1324. These data will be used to accurately constrain the variation in rock properties across Ursa Basin. All objectives were met at Sites U1322 and U1324. Because we encountered shallow-water flow at Site U1323, we were unable to core at this location. LWD/MWD, wireline logging, and coring proceeded with extraordinary efficiency despite the fact we were drilling in zones of significant overpressure.

2. Establish reference properties at Brazos-Trinity Basin #4.

We wanted to establish reference logging and core properties where overpressure is not present at a range of effective stresses in the Brazos-Trinity Basin. Coring and logging were successful at the Brazos-Trinity Basin #4 locations. However, only a limited number of pressures were measured due to early struggles with the DVTPP and T2P (see “**Challenges of Measuring Pressure**”). An intriguing result is that the mudstones beneath Brazos-Trinity Basin #4 (Site U1319) may be overpressured (Fig. **F36**). If Site U1319 is overpressured, then Sites U1319 and U1320 will provide important examples of a normally pressured location (Site U1319) and overpressured location (Site U1320) in the same location.

3. Illuminate the controls on slope stability.

We wanted to determine pore pressure, rock properties, and overburden stress to predict the potential for slope failure and estimate the conditions that drove previous slope failures. We gained a beautiful suite of data (whole core for geotechnical analysis, in situ pressures, and logs) across the failure surfaces. A striking result is the high degree of consolidation that is present within the slumped units (Fig. **F37**). A major component of the shore-based science will study the geometry, physical properties, timing, and pressures associated with these slumps.

4. Understand timing of sedimentation and slumping.

We wanted to establish the age of sediments in Brazos Trinity Basin #4 and Ursa Basin. Our preliminary results (Figs. **F28**, **F32**) suggest that the Brazos Trinity Basin #4 sediments span MIS VI to present, whereas the Ursa mudstones are <70 ka. At Brazos Trinity Basin #4, slumping, turbidite deposition, and sea level change were tightly linked. Dramatically high sedimentation rates were documented in Ursa Basin. Shore-based research will further constrain the chronostratigraphy of these systems.

5. Establish geotechnical and petrophysical properties of shallow sediments.

We wanted to break new ground in understanding geotechnical and petrophysical properties of shallow sediments (0–1000 mbsf). To support and complement core observations and laboratory measurements, we derived a complete logging suite, in situ measurements of pressure, and whole-core geotechnical samples. We will use these data to understand the compaction process near the seafloor and the evolution of overpressure during sedimentation. The ultimate scientific impact of acquiring these data will unfold in the years ahead. However, the Expedition 308 data set represents

a linked data set that has the potential to provide unparalleled insight into mudstone permeability and rheology.

6. Provide an extraordinary data set to observe ponded and channelized turbidite systems.

Expedition 308 sampled the ponded turbidite system at Brazos Trinity Basin #4 and the channelized systems present in Ursa Basin. These data are of great interest to both academic and industry researchers and will be deeply studied in postcruise research.

Additional Achievements

Expedition 308 was the first time where downhole pressure and lithology were monitored in real time (MWD) and it was the first time that weighted mud has been used as a tool to drill through overpressured regimes (see **“Challenges of Drilling in Overpressured Basins”**). Real time monitoring allowed us to observe shallow-water flow and to respond to this incident by raising the mud weight in order to hold back flow into the borehole. At both Sites U1323 and U1324 we showed that weighted mud and real-time monitoring can be used to safely drill and complete operations. Future expeditions in a variety of settings might benefit from the planned use of weighted mud to stabilize the borehole.

We expect research on the cores and data generated during Expedition 308 to break new ground, especially in the field of geotechnical and hydrogeological analysis of continental slope sediment successions, be it at passive or active continental margins. Despite initial setbacks, we have shown that programs of in situ measurement of pore pressure in fine-grained sediments can be done with overall success. We have demonstrated that drilling into overpressured formations with riserless technology can be managed using heavy mud, fluid flow into the borehole can be controlled, and operations can be safely concluded without risk to the seafloor environment.

OPERATIONS

Port Call Activities

Expedition 308 began with first line ashore at 1555 h on 30 May 2005.

The IODP technical and Transocean crew changes occurred on schedule on 31 May and 1 June, respectively. In addition to the normal port call routine of loading and unloading freight, offloading cores, a U.S. Coast Guard inspection, Transocean company compliance audit, vessel tours, and the bunkering of fuel (~1300 MT), there were a few nonstandard items related to the special needs of Expedition 308. In anticipation of extremely heavy mud usage during the upcoming expedition, >1000 short tons of bulk material was loaded during the first four days of the port call. Additionally, two service personnel joined the vessel to address specific high-profile aspects of the Gulf of Mexico enterprise; MWD Specialist Hwa Fong “Kelvin” Hoong from Schlumberger and Mud Engineer George Stokes from Milchem International.

The last line was released from the dock at 1455 h on 4 June, and the vessel departed for the first site of Expedition 308 (Table T2).

Brazos-Trinity Basin #4

Hole U1319A

The *JOIDES Resolution* arrived at Site U1319 on 6 June and a beacon was deployed at 1350 h. The T2P was first deployed above the seafloor, close to the mudline, to test that it could be deployed through the BHA and that the pressures measured were reasonable. The test was a success. A vibration-isolated television (VIT) survey was conducted prior to spudding. Electrical control problems associated with the mud pumps delayed operations for 45 min, and Hole U1319A was spudded at 0130 h on 7 June. The seafloor depth was estimated to be at 1440.0 meters below rig floor (mbrf) based on core recovery. Piston coring with nonmagnetic hardware advanced to a depth of 114.6 mbsf (Core 13H). Coring was then continued with the extended core barrel (XCB) system to a total depth of 157.5 mbsf. The total average recovery for this hole was 98.6%. The T2P was deployed in Hole U1319A for the first time at a depth of 80.5 mbsf for 30 min, but the tip of the probe was bent because of formation stiffness. The bit was pulled clear of the hole at 2120 h on 7 June and raised to 240 m above the seafloor. The vessel was then offset 2.3 nmi in dynamic positioning (DP) mode to Site U1320 at an average speed of 0.9 kt.

Hole U1320A

A beacon was dropped at Site U1320A at 0040 h on 8 June. The VIT was launched and the drill string lowered to 1469.6 mbrf. The vessel was offset 5 m north after spotting a man-made object on the seafloor (probably a garbage bag). Hole U1320A was spud-

ded at 0420 h on 8 June. The seafloor depth was established at 1480.4 mbrf based on recovery. Piston coring advanced to 69.4 mbsf where a sandy layer prevented further penetration. Coring continued with the XCB system to 299.6 mbsf (Core 33X). The T2P was deployed at 126.3 (Core 15X) and 231 mbsf (Core 24X), and temperature and pressure were successfully recorded. The first DVTTP temperature measurement was made at 203.4 mbsf (Core 23X) followed by a second measurement at 299.6 mbsf. APC recovery was 101.9%, whereas XCB recovery averaged 78.3%. Recovery for the total cored interval was 83.7%. A supply boat (*Emily G*) arrived at 0415 h on 10 June to discharge the MWD drilling hardware and departed at 0520 h. Downhole logging of Hole U1320A was undertaken with three tool strings: the triple combo, FMS-sonic, and Well Seismic Tool (WST). All tools reached the bottom of the hole, and good logs were obtained. The VIT was deployed and the hole was observed as the drill string was pulled clear of the seafloor at 1930 h on 10 June. The logging mud quickly obstructed the view, and the camera was promptly recovered.

Hole U1320B

Hole U1320B was spudded with a MWD drilling assembly at 0915 h on 11 June. The seafloor was established at a depth of 1485.0 mbrf. After washing in the bit to 14.9 mbsf, the VIT was retrieved. MWD drilling was initiated and continued at an average rate of penetration of 25.4 m/h to 320.0 mbsf, which was reached at 0325 h on 12 June. The bit was pulled out of the hole and cleared the seafloor at 0520 h on 12 June. The drill string was positioned 250 m above the seafloor and the vessel was offset 2.3 nmi back to Site U1319 at an average speed of 0.9 kt in DP mode.

Hole U1319B

The position of Hole U1319B was 20 m north of Hole U1319A. Hole U1319B was spudded at 1105 h on 12 June as the driller observed the bit contacting the seafloor at a depth of 1447.0 mbrf. MWD drilling advanced to 180 mbsf at an average ROP of 30 m/h by 2100 h on 12 June.

Hole U1321A

The *JOIDES Resolution* arrived at the location of Site U1321 by 0000 h and a beacon was deployed at 0005 h on 13 June. The driller tagged the seafloor at 1468.0 mbrf (precision depth recorder [PDR] = 1467.4 mbrf) and observed the spudding via the subsea camera at 0205 h. MWD drilling proceeded without incident to the depth objective of 140.0 mbsf by 0900 h at a controlled ROP of 30.0 m/h. The bit was recovered, and

the MWD drilling package was disassembled, laid down, and secured for the sea voyage to the next site. The vessel departed for Site U1322 at 1500 h on 14 June.

Transit to Ursa Basin

The 293 nmi transit from Site U1321 to Site U1322 was made at an average speed of 11.0 kt. A beacon was deployed at Site U1321 at 1815 h on 14 June.

Hole U1322A

Hole U1322A was spudded at 0130 h on 15 June when the driller tagged the seafloor at 1330.0 mbrf (PDR = 1336.4 mbrf). The bit was jettied to 3.8 mbsf, and the VIT was recovered. The hole was then drilled from 3.8 to 200.0 mbsf at an average ROP of 30 m/h. To ensure that we did not exceed our target depth, the interval from 200 to 238.0 mbsf was drilled at an ROP of 20 m/h. There was no indication of pressurized sands throughout the drilled interval. Resistivity and gamma ray data indicated that the main lithology was mud. After the hole was displaced with 70 bbl of 8.9 ppg sepiolite mud, the drill string was pulled out of the hole, clearing the seafloor at 1525 h on 15 June. When the bit was placed at 1040 mbrf (~222 m above seafloor), the DP operator began to offset the vessel to Site U1323. The vessel departed Site U1322 at 1600 h, leaving behind the beacon because of the planned return to this site subsequent to coring operations at Site U1324.

Hole U1323A

A beacon was deployed at Site U1323 at 1854 h on 15 June. Hole U1323A was spudded at 2025 h as the driller tagged the seafloor at 1271.0 mbrf (PDR = 1278.4 mbrf). The VIT was recovered, and MWD drilling advanced to 206 mbsf. A sand layer, ~1.5 m thick (as interpreted from natural gamma ray resistance data from the MWD bit), was detected at 204 mbsf. Simultaneously, a jump in pressure of 150 psi over the background drilling pressure in the pressure-while-drilling (PWD) log was observed. A residual backpressure of 150 psi was also observed by the driller when he shut down the mud pumps. We pumped 50 bbl of 10.5 ppg mud into the hole and noted that the backpressure went to zero. When this mud was displaced with seawater, the pressure returned. The pipe was filled with 110 bbl of 10.5 ppg mud, and a wiper trip was made to 51.1 mbsf and back to 204.6 mbsf. The overpressure remained, and it was decided to continue to drill ahead at a very low ROP gradually increasing to 30 m/h and with “pumping and dumping” 10.5 ppg mud. At 242 mbsf, a rapid drop in gamma ray resistivity, suggestive of a second sand interval, was observed in the data. At this point,

it was decided that to maximize the amount of science and to conserve mud, we should move to the location of Site U1324 and plug and abandon Hole U1323A. We displaced the hole with 73 bbl of 13.5 ppg mud. The VIT was deployed, and the top of the hole was observed to confirm that there was no flow. A free-fall funnel (FFF) was deployed and inspected again with the VIT. We reentered Hole U1323A at 0300 h on 17 June, and the hole was displaced with 31.8 bbl of 14.0 ppg cement that applied a cement plug from 140 to 40 mbsf. The drill string was then recovered, clearing the seafloor at 0550 h and the rotary table at 1010 h on 17 June.

This was the *JOIDES Resolution's* first experience with riserless drilling with a weighted mud. It was a valuable learning exercise and everyone came away with confidence in the ability to handle downhole pressures in a routine fashion. Provided with accurate real-time downhole information, we confirmed that we can carefully monitor shallow flows, take appropriate action to control the flow, and drill ahead under appropriate conditions. We also demonstrated that we can plug and abandon the hole in this environment without leaving any fluid flow.

Hole U1324A

A beacon was deployed at Site U1324 at 1040 h on 17 June. Hole U1324A was spudded at 1610 h on 17 June when the driller tagged the seafloor at 1066.0 mbrf (PDR = 1078.0 mbrf). After the bit was washed ahead to 5.0 mbsf, MWD drilling advanced without incident to 333.4 mbsf at an ROP of 30 m/h, where a wiper trip was made back to 60.8 mbsf. MWD drilling resumed to 477.7 mbsf, where another wiper trip was made back to 330.4 mbsf. Because of the potential for interbedded levee sands below 481 mbsf, heavy mud was continuously pumped from this depth to the total depth of 612 mbsf (20 m above the top of the Blue Unit). At ~2045 h on 18 June, MWD drilling advanced slowly at an ROP of 20 m/h and gradually increased to 30 m/h while “pumping and dumping” 10.0 ppg mud. The drilling advanced to the depth objective of 612 mbsf by 0410 h the next morning. The hole was plugged with cement and heavy mud and abandoned. A FFF was made up and deployed at 0808 h on 19 June with the bit at ~80 mbsf. The VIT was deployed, and a visual inspection confirmed that there was no flow emanating from the top of the FFF and that the funnel was upright. The bit was pulled free of the seafloor at 0853 h.

Reentry in Hole U1324A was made at 1828 hr on 19 June and the bit placed at the logging depth of 54.2 mbsf. A tool string consisting of the Hostile Environment Gamma Ray Sonde, DSI, and General Purpose Inclinometer Tool was deployed first.

The end of pipe was set at 54.2 mbsf and was later moved to 49 mbsf to ease passage of the logging string. A downhole log was recorded from seafloor at 550 m/s, and we encountered two obstructions at 59 and 509.6 mbsf. The shallow obstruction was passed after a few attempts, but the deeper obstruction remained impassable. After attempting to clear the obstruction for ~15 min and getting some overpull, we decided to log uphole from this point. We measured gamma radiation and *P*- and *S*-wave velocity at 15 Hz sampling rate in the first pass at 275 m/h up to 84.0 mbsf. The tool string was lowered for a second pass to 509.6 mbsf, where the same obstruction was encountered. We began the second pass from this depth recording gamma radiation, *P*- and *S*-wave velocity, low-frequency lower dipole, and Stoneley modes at 15 Hz sampling rate. The second deployment consisted of the WST. The marine mammal watch began 1 h prior to the WST deployment, and the operation started with putting the generator-injector (GI) gun in the water for the beginning of the soft shooting. The LFV obstructed lowering the WST into the open hole, and we had to pump seawater to ease the tool into the borehole. After this, a bad electrical line prevented power transfer to the main trigger box of the shooting setup. The line was changed, and the computer had to be powered down before the configuration worked. During this time, a corroded plug connecting the electrical leads to the GI gun was also found. This problem was also corrected but delayed the beginning of the experiment by ~1.5 h. Based on LWD caliper recordings, 16 stations were targeted at ~25 m intervals. The Schlumberger equipment was rigged down by 1330 h on 20 June. The hole was then displaced with 44.0 bbl of 11.0 ppg neat cement, forming a 145 m plug. The hole was successfully abandoned at 1745 h when the bit cleared the FFF.

Hole U1324B

The BHA for Hole U1324B was identical to the BHA used to core the Brazos-Trinity Basin #4 sites. After the VIT performed a survey of the seafloor, the driller tagged the bottom at 1066.8 mbrf. Hole U1324B was spudded with the APC at 0250 h. The recovery of the first core established the seafloor depth at 1067.5 mbrf. Piston coring advanced without incident to a depth of 117.8 mbsf, where the corer did not achieve a complete stroke but did recover 9.91 m (104%). Coring continued with the APC to 357.9 mbsf by advancing by recovery. At this depth, one XCB core was obtained prior to each deployment of the DVTTP and T2P. Piston coring continued to a total depth of 394.5 mbsf by advancing by recovery. A total of 48 piston cores were used in penetrating to this depth (average recovery = 101.3%). Nonmagnetic core barrels were used for all piston cores. The cores were oriented starting with Core 4H. The APCT was deployed in 14 cores, and a special Fugro cutting shoe was deployed in Cores 4H, 7H,

and odd-numbered piston cores up to and including 49H. Coring resumed with the XCB and deepened the hole to 608.2 mbsf. The XCB-cored portion of the hole was 223.8 m with an average recovery of 80.8%. The total cored interval of 608.2 m was obtained with 93.7% average recovery. In compliance with the operational protocol, heavy mud (10.5 ppg) was continuously pumped starting at 481 mbsf and sustained until the bottom of the hole. The DVTTP was deployed 10 times in this hole (229.1, 362.4, 387.9, 464.3, 493.1, 522.0, 541.2, 560.4, 589.2, and 608.3 mbsf). There were also 10 deployments (~30 min each) of the T2P (51.3, 89.3, 117.8, 136.3, 368.0, 394.5, and 593.2 mbsf). In accordance with the operating protocol, the hole was plugged with 44 bbl of 11.0 ppg neat cement forming a plug of ~145 m. The cement was followed by 40 bbl of 10.5 ppg mud and then chased with 50 bbl of seawater. The hole was observed by the VIT camera with the bit at ~80 mbsf, and no flow was detected. The bit was pulled free of the hole at 0025 h on 26 June. As the vessel was moved off location, a subsea release dart was pumped down to swab the inside of the pipe.

Hole U1324C

The vessel was dynamically repositioned 20 m west of Hole U1324A. After a VIT survey of the seafloor of the new hole failed to indicate any obstructions, Hole U1324C was spudded when the driller tagged the seafloor at 1066.5 mbrf. The hole was then drilled ahead to 50.0 mbsf, where the T2P was deployed with good results. Following the retrieval of the probe, a single APC core was obtained for physical property analysis. The hole was then drilled in increments of 50 m, alternating between T2P and DVTTP deployments and taking APC cores for geotechnical analysis. Operations in Hole U1324C continued with the deepening of the hole to 250.0 mbsf, where a DVTTP measurement was taken followed by a single piston core. The hole was then drilled from 250.0 to 300.0 mbsf, where the fifth T2P deployment was made, followed by a single piston core. The hole was then drilled to 405.0 and 505.0 mbsf, followed each time by a single piston core. The last piston cored advanced to a final depth of 511.8 mbsf. When the driller advanced beyond 481.0 mbsf, heavy mud (10.5 ppg) was continuously pumped in accordance with the operating protocol for this site. A total of eight piston cores were obtained, with the last seven advanced by recovery. The cored interval was 55.1 m with an average recovery of 100.9%. Before the drill string was withdrawn from Hole U1324C, the hole was observed by VIT camera and no flow was evident. Because penetration in the hole was terminated above the sand layers, it was not necessary to plug this hole with cement. The bit was pulled free of the seafloor at 0135 h on 28 June and positioned 204 m above the seafloor. The beacon was recovered before departing location at 0240 h.

Hole U1322B

The vessel was offset 6.2 nmi to Site U1322 at 0915 h on 28 June. After observing the seafloor with the VIT camera, Hole U1322B was spudded with the APC at 1145 h. Piston coring advanced the hole to a depth of 61.0 mbsf when operations were interrupted because of the failure of a control transformer in the variable field supply of the core winch. This required 3.75 h to troubleshoot and repair. Piston coring resumed at 2345 h on 28 June and continued to 0730 h on 30 June, when the total depth of 234.5 mbsf was attained. The average recovery for the hole was 101.0%. The T2P was deployed three times in this hole. The first measurement in the hole was made at 42.0 mbsf following Core 5H. The second attempt was made at 134.3 mbsf subsequent to Core 15H. On this occasion, the hole was displaced with 10.5 ppg mud. The last deployment was at a depth of 157.8 mbsf. This deployment was made after recovering Core 18H and with the hole displaced with 55 bbl of 10.5 ppg mud. The DVTPP was deployed once at a depth of 166.7 mbsf following Core 19H. On this occasion, the hole was displaced with 55 bbl of 10.5 ppg mud. The bit was pulled free of the hole at 1010 h on 30 June.

Hole U1322C

Hole U1322C was dedicated to temperature and pressure measurements. Following a DP offset of 20 m west of Hole U1322A, the VIT was deployed. The visual examination of the seafloor confirmed a clear area under the bit. Hole U1322C was spudded with the APC at 1125 h on 30 June. Hole U1322C was then drilled in six intervals to a final depth of 231.5 mbsf. The T2P was deployed at 50, 75, 150, and 200 mbsf. After the first measurement attempt, the hole was stabilized by displacing it with 10.5 ppg mud. The DVTPP was deployed at 100, 220, and 238 mbsf. The hole was also displaced with heavy mud prior to each deployment, and no circulation or rotation was applied. The hole was displaced with an additional 75 bbl of 10.5 ppg mud prior to abandonment. The bit cleared the seafloor at 1824 h on 1 July and was observed with the VIT. No flow was emanating from this hole. While operating in Hole U1322C, the *Emily G* made the third and final visit to the *JOIDES Resolution*. The *Emily G* was on location and standing by at 0400 h on 30 June. The work boat offloaded catering supplies and loaded freight originally destined for Panama. We also loaded 35.5 short tons (710 sacks) of Florigel (attupulgite) from the *Emily G*. The work boat departed for Port Fourchon, Louisiana at 0930 h transporting Mud Engineer George Stokes and two other personnel (IODP Marine Laboratory Specialist Karen Johnston and Transocean DP Operator John Powell) to shore.

Hole U1322D

The vessel was offset 20 m north of Hole U1322A, where Hole U1322D was spudded with the APC at 1925 h on 1 July. This followed a seafloor survey with the VIT. The hole was drilled and cored in five incremental steps to a total depth of 175.0 mbsf. Three piston cores were obtained from the seafloor to 9.5 mbsf, 70.0–79.5 mbsf, and 100.0–107.8 mbsf. The average recovery of the cored interval of 26.8 m was 101.5%. The T2P was deployed four times at 40.0, 70.0, 100, and 134 mbsf. The DVTTP was deployed at 175.0 mbsf. With the exception of the first T2P run, the holes were displaced with heavy mud prior to deployment, and all downhole measurements were attempted with no circulation or rotation. All operations concluded by 1600 h on 2 July to allow sufficient time to recover the drill string, beacons, and disassemble and store the BHA components. The VIT was deployed prior to withdrawal of the drill string from the hole, and a short inspection of the top of Hole U1322D confirmed the absence of any flow.

Transit to Panama

After the drilling equipment was secured, the vessel began the voyage to Panama at 0030 h on 3 July.

Expedition 308 officially ended with the first line ashore at 1420 h on 8 July 2005.

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Table T1. Heavy mud used while coring and drilling.

Hole	Total mud (bbl)	Weight (ppg)	Depth range (mbsf)	Duration (h)
U1324A (LWD)	4400	10.0	477–612	~4.5
U1324B (coring)	3880	10.5	481–608	~36.0

Note: LWD = logging while drilling.

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Table T2. Expedition 308 operations summary.

Hole	Latitude	Longitude	Depth (mbrf)	Cores (<i>N</i>)	Cored (m)	Recovery		Drilled (m)	Total penetration (m)	Total depth (mbrf)	Time on hole	
						m	%				h	days
U1319A	27°15.9751'N	94°24.1908'W	1440.0	18	157.5	155.29	98.6	0.0	157.5	1597.5	32.25	1.3
U1319B	27°15.9857'N	94°24.1908'W	1441.0	0	0.0	0.00	0.0	180.0	180.0	1621.0	14.17	0.6
Site U1319 totals:				18	157.5	155.29	98.6	180.0	337.5	NA	46.42	1.9
U1320A	27°18.0809'N	94°23.2527'W	1480.4	33	299.6	250.89	83.7	0.0	299.6	1780.0	70.08	2.9
U1320B	27°18.0900'N	94°23.2514'W	1479.0	0	0.0	0.00	0.0	320.0	320.0	1799.0	31.75	1.3
Site U1320 totals:				33	299.6	250.89	83.7	320.0	619.6	NA	101.83	4.2
U1321A	27°16.5398'N	94°23.9370'W	1462.0	0	0.0	0.00	0.0	140.0	140.0	1602.0	10.95	0.5
Site U1321 totals:				0	0.0	0.00	0.0	140.0	140.0	NA	10.95	0.5
U1322A	28°5.9628'N	89°1.5120'W	1330.0	0	0.0	0.00	0.0	238.0	238.0	1568.0	21.75	0.9
U1322B	28°5.9642'N	89°1.4995'W	1330.5	29	234.5	236.79	101.0	0.0	234.5	1565.0	49.00	2.0
U1322C	28°5.9640'N	89°1.5228'W	1330.0	1	4.5	4.53	100.7	231.5	236.0	1566.0	32.23	1.3
U1322D	28°5.9753'N	89°1.5104'W	1330.0	3	26.8	27.21	101.5	148.2	175.0	1505.0	30.10	1.3
Site U1322 totals:				33	265.8	268.53	101.0	617.7	883.5	NA	133.08	5.5
U1323A	28°5.4725'N	89°4.3509'W	1271.0	0	0.0	0.00	0.0	247.0	247.0	1518.0	35.50	1.5
Site U1323 totals:				0	0.0	0.00	0.0	247.0	247.0	NA	35.50	1.5
U1324A	28°4.7856'N	89°8.3574'W	1066.0	0	0.0	0.00	0.0	612.0	612.0	1678.0	83.58	3.5
U1324B	28°4.7845'N	89°8.3442'W	1067.5	74	608.2	569.92	93.7	0.0	608.2	1675.7	122.17	5.1
U1324C	28°4.7832'N	89°8.3683'W	1066.5	8	55.1	55.70	100.9	0.0	511.8	1578.3	50.25	2.1
Site U1324 totals:				82	663.3	625.62	94.3	612.0	1732.0	NA	256.00	10.7
Expedition 308 totals:				166	1386.2	1300.33	93.8	2116.7	3959.6	NA	583.78	24.3

Notes: *N* = number. NA = not applicable.

Figure F1. **A.** Overpressure results when sedimentation occurs more rapidly than fluids can be expelled by compaction. **B.** Overpressure (P^*) is pressure that is greater than the hydrostatic pressure. Vertical effective stress (VES) is the difference between the lithostatic stress and the pore pressure. **C.** Overpressure causes low effective stresses, which are recorded by an “undercompacted” porosity profile. A suite of models describes how overpressure is generated during rapid deposition (Bethke, 1986; Bredehoeft and Hanshaw, 1968; Gibson, 1958; Koppula and Morgenstern, 1982; Osborne and Swarbrick, 1997; Swarbrick and Osborne, 1996).

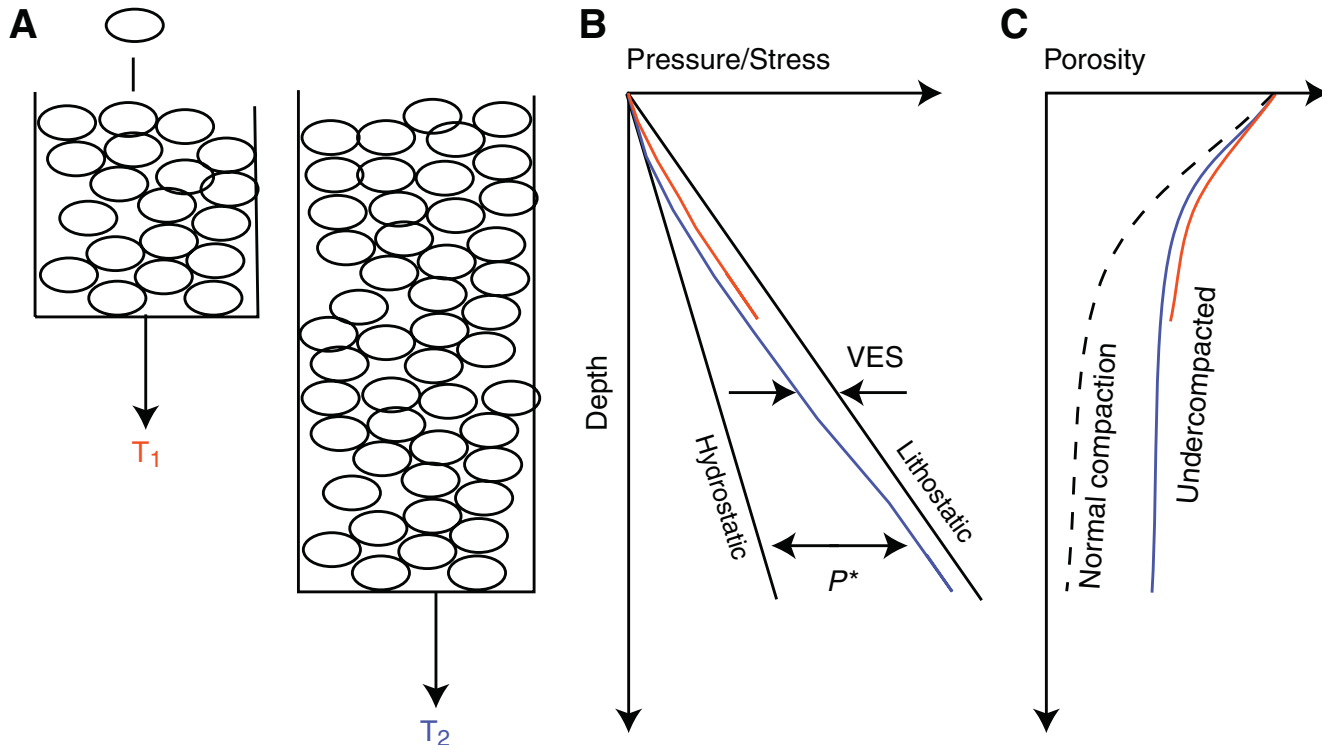


Figure F2. Flow-focusing model. **A.** Low permeability sediments are rapidly deposited on a high permeability aquifer (outlined in white). The sedimentation rate decreases from left to right, resulting in the final wedge-shaped geometry. Rapid sedimentation generates overpressures (P^* ; color contours) that are greatest on the left (red). Flow is driven laterally (left to right) along the aquifer and expelled at the toe of the slope where the aquifer ends (white arrows). The vertical effective stress (black contours) is lowest on the right. **B.** Predicted overpressure profiles where overburden is thick (Site U1324) and thin (Site U1322). (1) Overpressure at Site U1324 is greater than at Site U1322 for equivalent depths. (2) The vertical effective stress (σ_v') is much lower at Site U1322 than at Site U1324. (3) Porosities are much lower at Site U1322 than at Site U1324 for equivalent depths. (4) Pore pressures (P) equal the overburden stress (σ_v) at Site U1322. (5) Infinite slope analyses (FS; relates the failure-driving stress to the available shear strength for shallow failures) predict unstable conditions (FS < 1) for Site U1322. (6) Simulated vertical fluid velocity is higher at Site U1322 than at Site U1324. At Site U1324, we predict upward flow for most of the section but downward flow (velocity < 0) just above the aquifer. Model parameters: low permeability mudstone $k_v < 5 \times 10^{-8} \text{ m}^2$ and $k_h < 5 \times 10^{-16} \text{ m}^2$; aquifer permeability $k_h = k_v 5 \times 10^{-14} \text{ m}^2$; maximum sedimentation rate = 3.5 mm/y; minimum sedimentation rate = 0.8 mm/y.

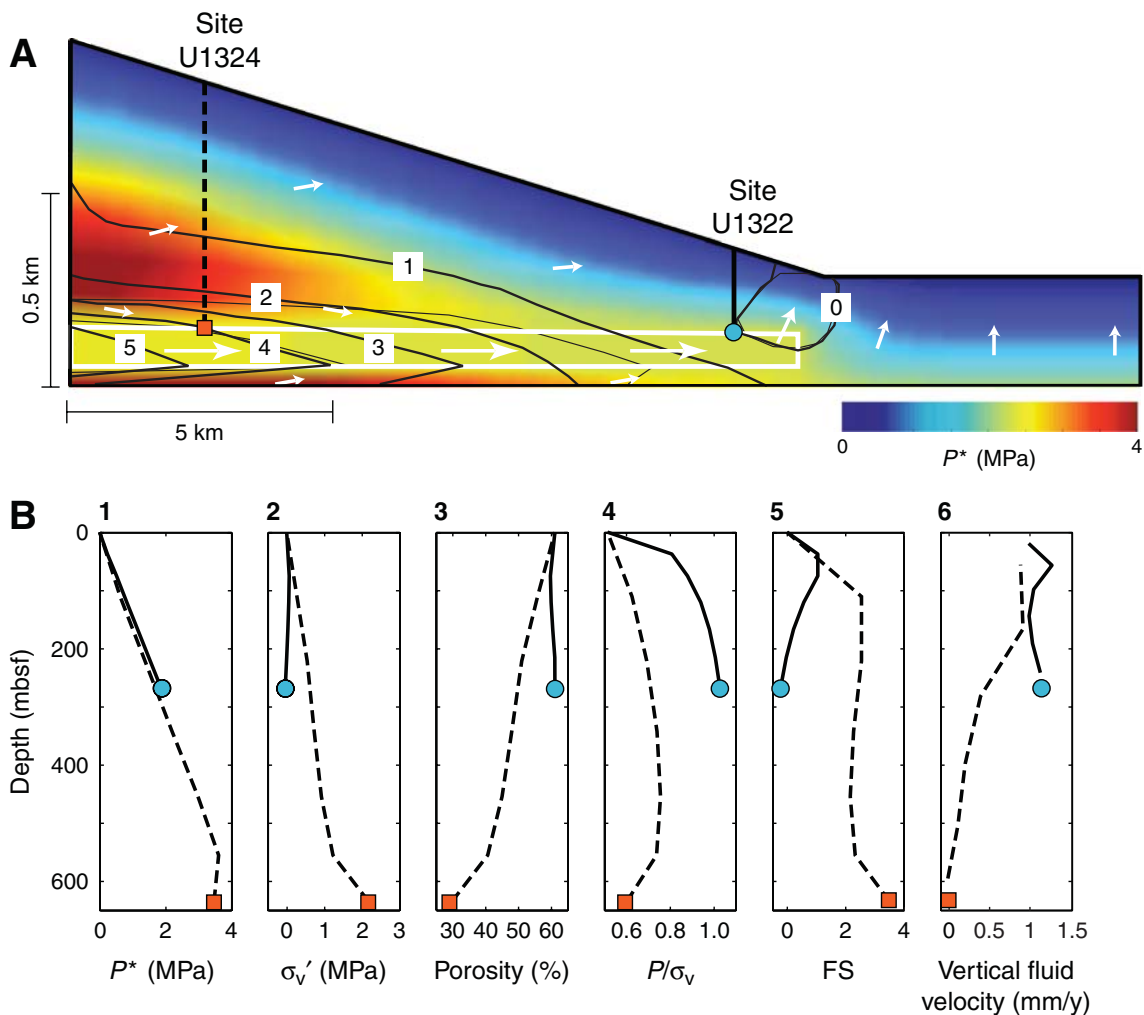


Figure F3. Flow-focusing drives (A) slope instability and (B) the migration of fluids. σ_v = overburden stress, σ_{hmin} = minimum horizontal stress.

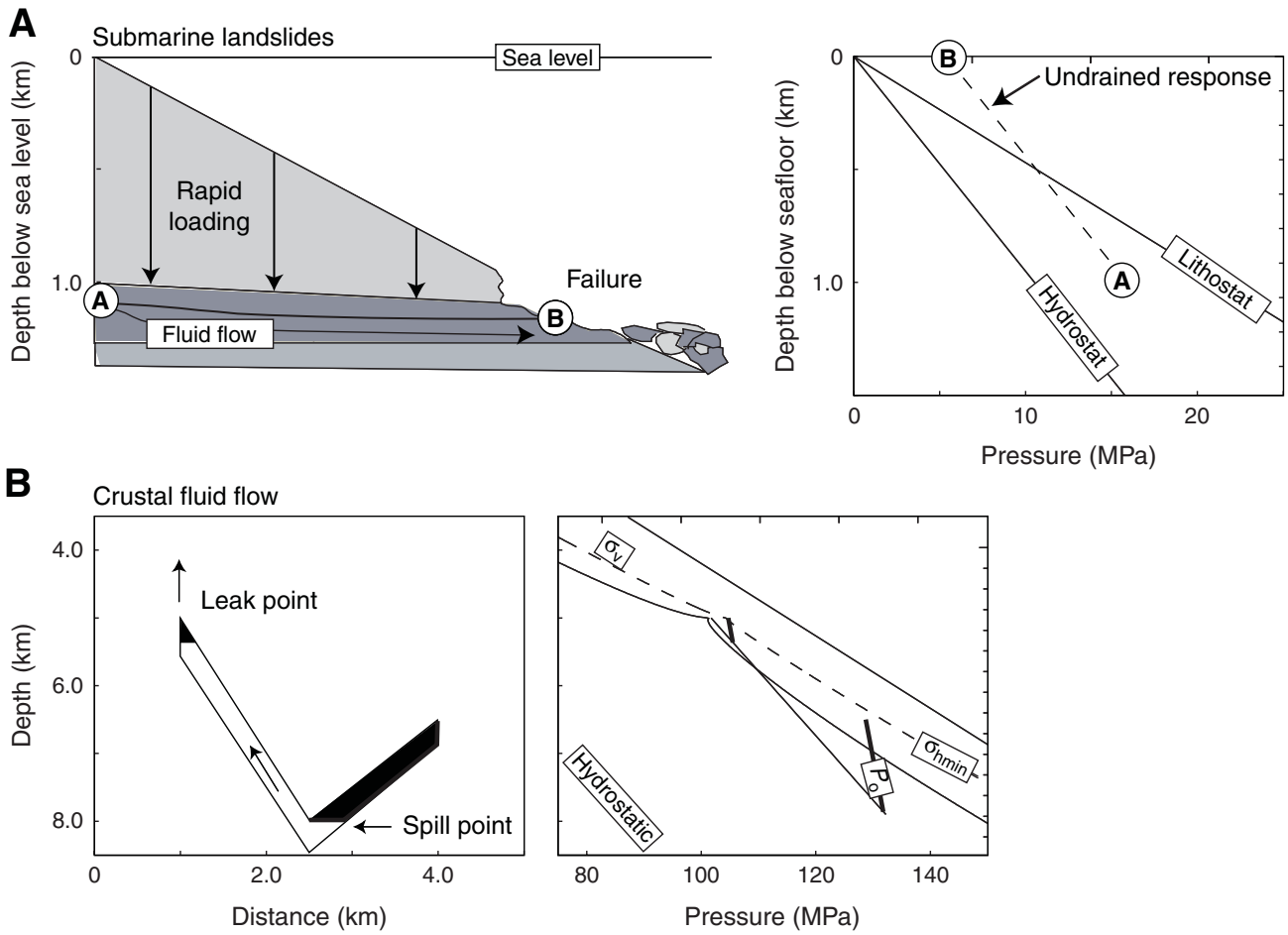


Figure F4. Bathymetric image of the continental slope of the Gulf of Mexico. Proposed drilling was in the Brazos-Trinity region and the Ursa region.

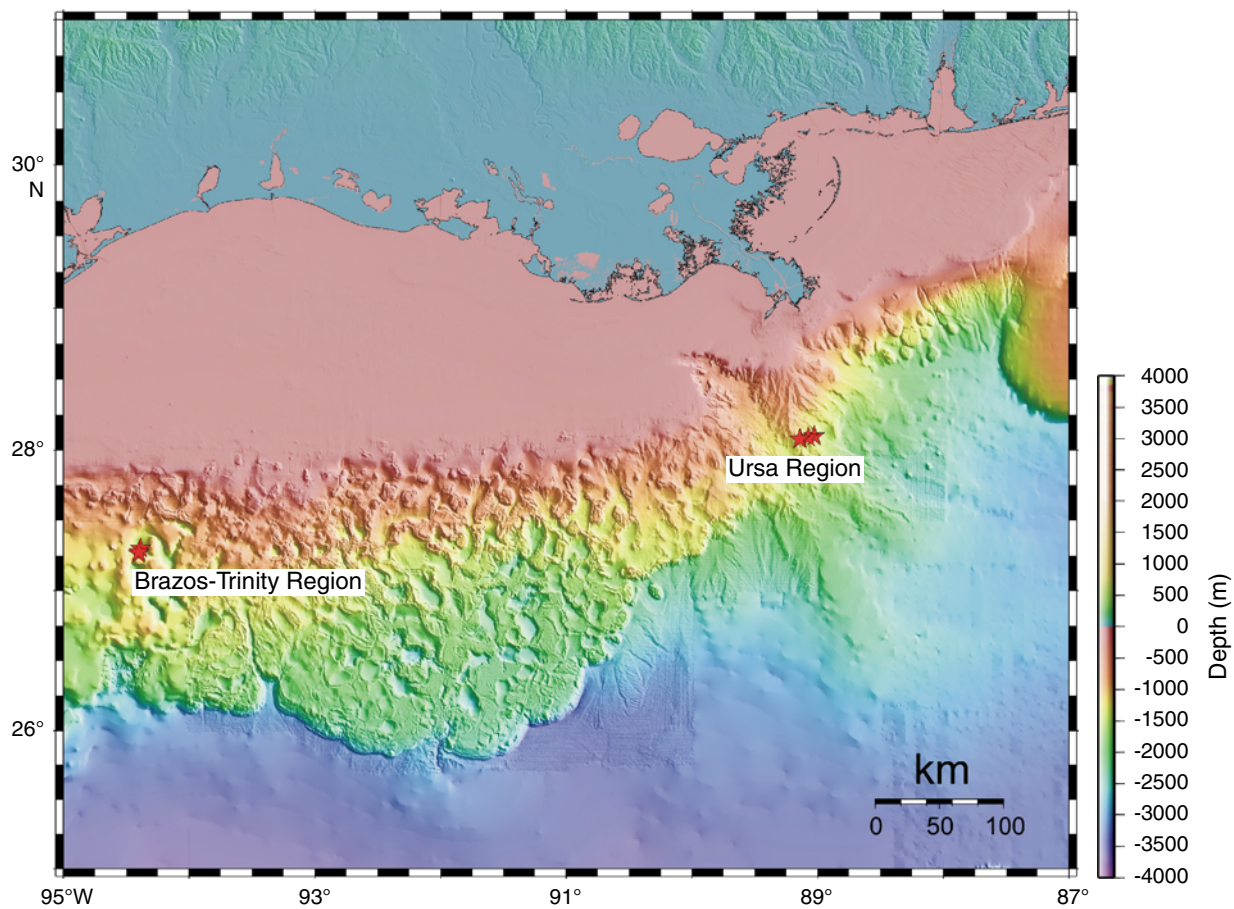


Figure F5. Bathymetric chart of Brazos-Trinity Basin #4 showing locations for dip seismic Line 3020 and the three sites drilled during Expedition 308. Depth contours are at 10 m intervals. Artificial sun illumination from the northwest. Bathymetric information adapted from report Number 3060-TAMU-GOM.

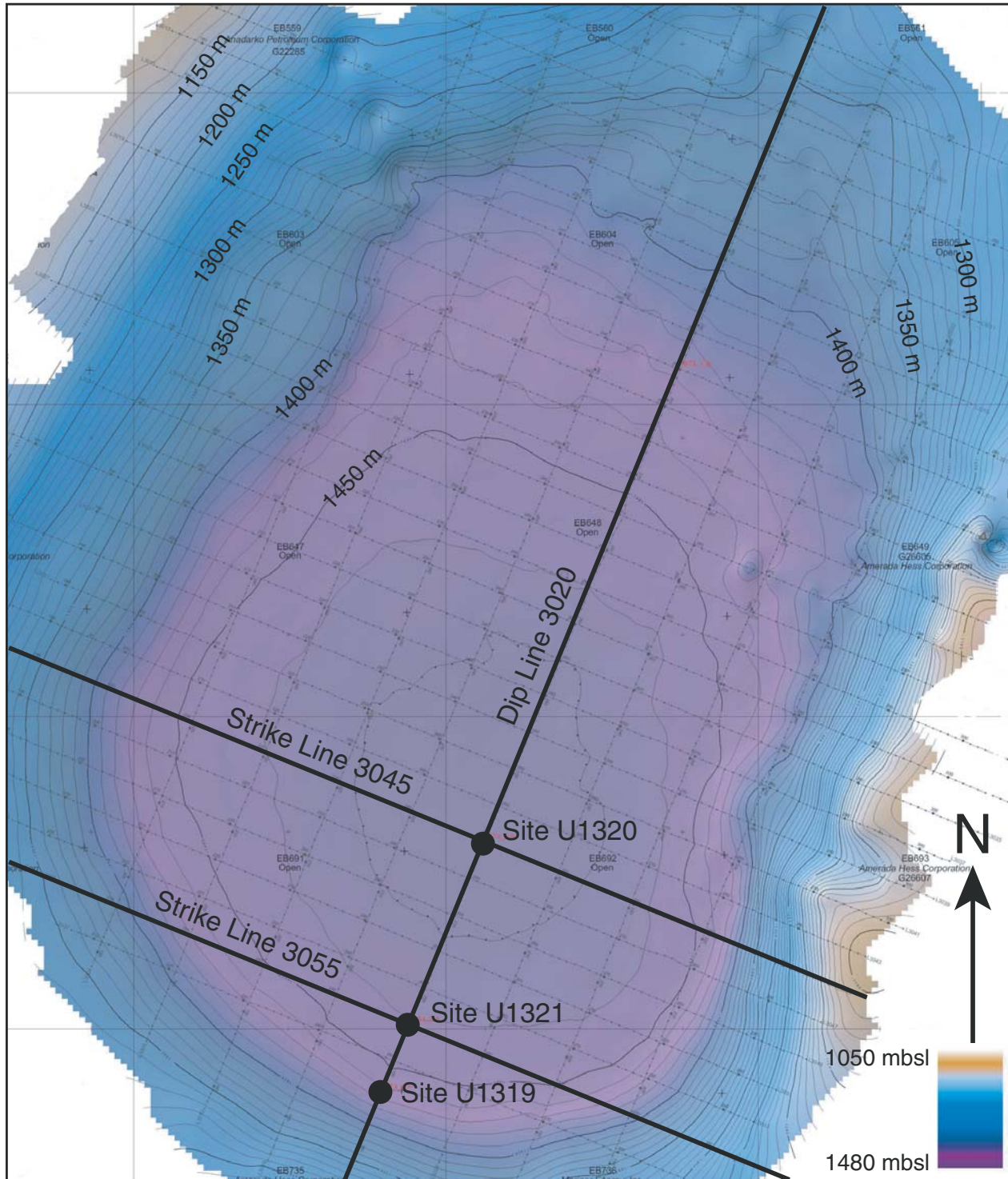


Figure F6. Dip seismic Section 3020 (shown in Fig. F5). Specific sites are located at the cross-tie with strike Line 3045 (Site U1320), strike Line 3055 (Site U1321), and at the southern limit of this line (Site U1319). Primary sites for Brazos-Trinity include Site U1320 and U1319. Site U1321 was a secondary site. SF = sea-floor.

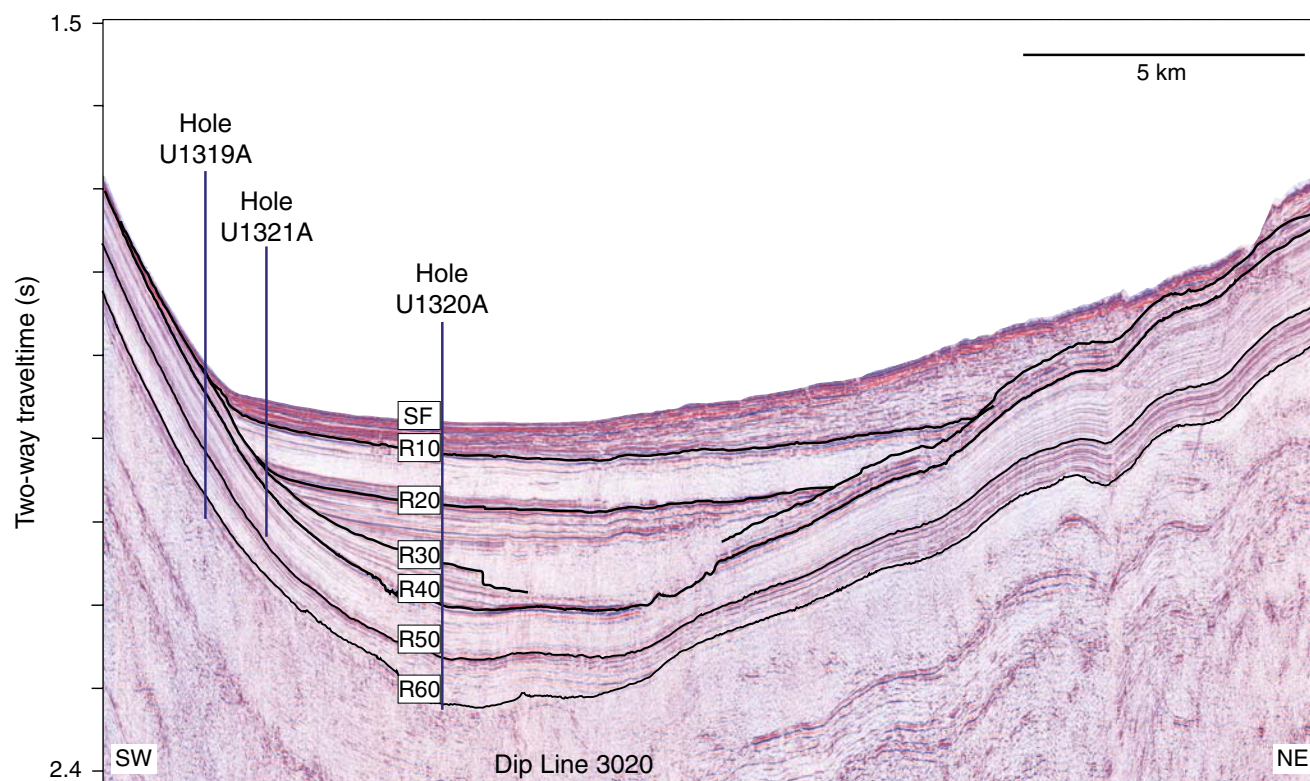


Figure F7. Strike seismic Line 3045. Primary Site U1320 is located at the intersection of Lines 3020 and 3045.

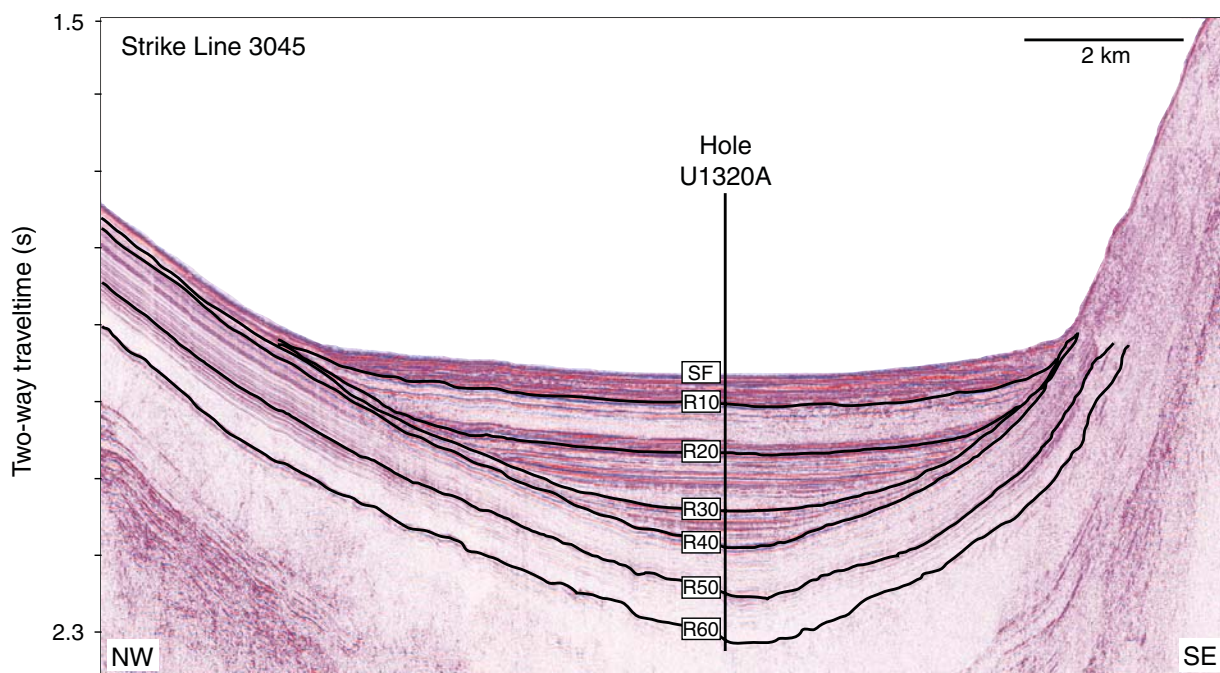


Figure F8. Bathymetric image of the Ursa region illustrating the location of Sites U1322, U1423, and U1324.

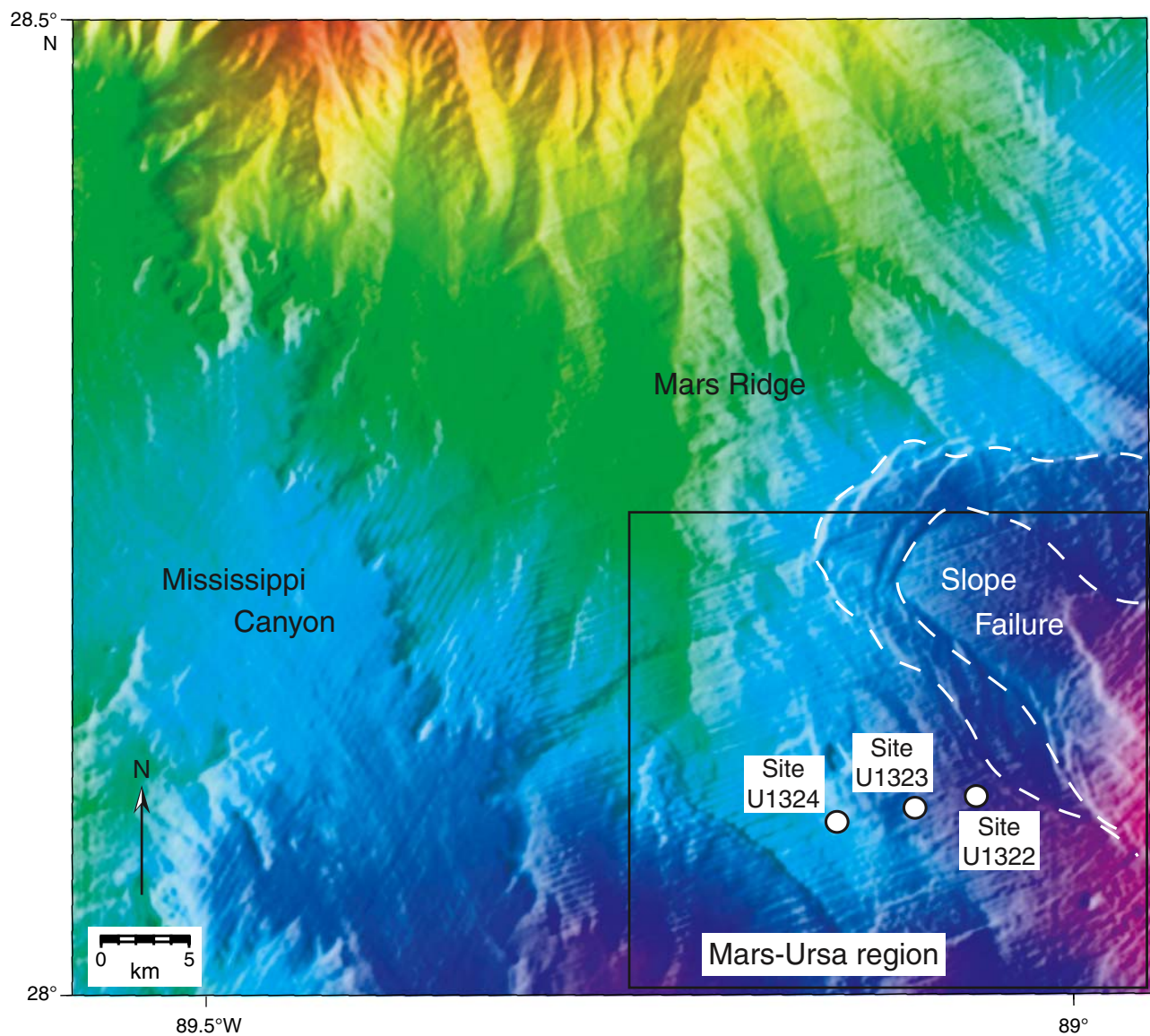


Figure F9. Basemap of seismic cross-section A-A'.

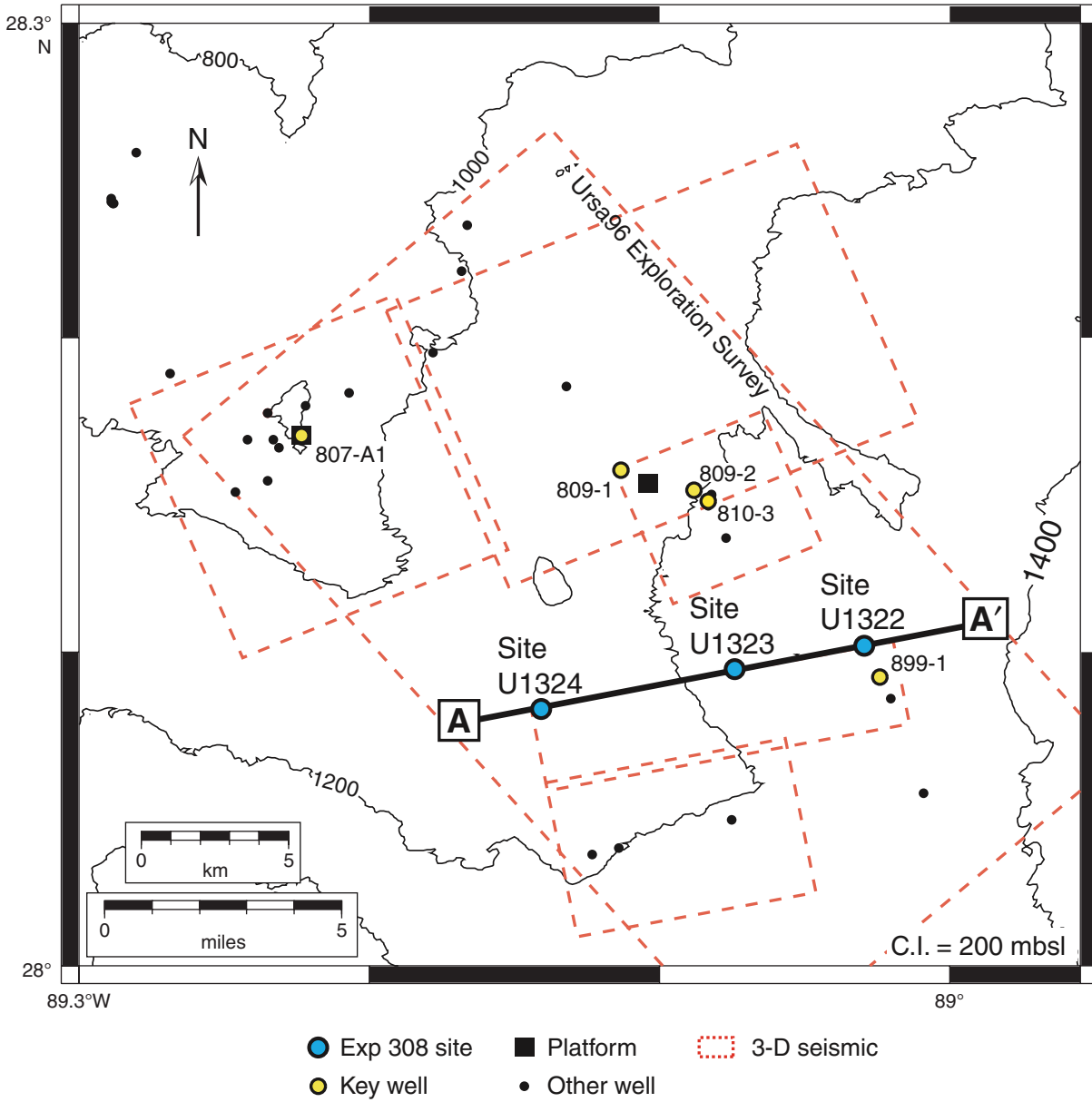


Figure F10. Gamma ray (NGR) and resistivity logs, core and log porosities, and in situ pressures at M.C. 810 Ursa geotechnical well #1. The Blue Unit (light gray) lies between 300 and 550 mbsf and is composed of interbedded sandstone and mudstone layers. Core porosity (ϕ_{core}) declines rapidly with depth to 200 mbsf and thereafter is constant. Overpressure ($P^* = P - P_h$) is plotted; thus the vertical axis is hydrostatic pressure (P_h) and the right boundary of the plot is the reduced lithostatic pressure ($\sigma_v^* = \sigma_v - P_h$). Circles = piezoprobe pressures, triangles = preconsolidation pressures from uniaxial consolidation tests of core, stars = pressure measurements inferred from pressure while drilling (PWD) in the Blue Unit. Ostermeier et al. (2000) and Eaton (1999) further describe these data.

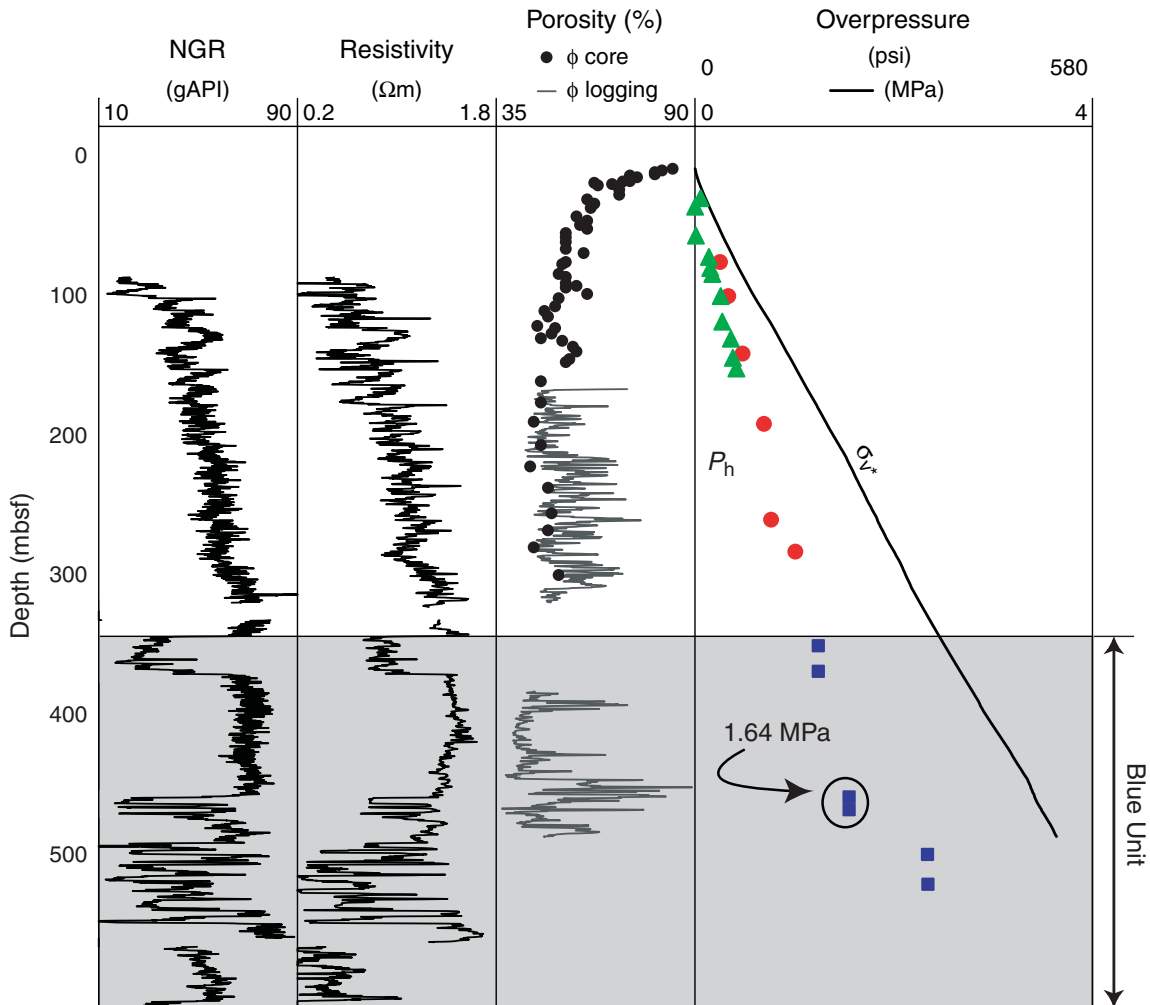


Figure F11. A. Seismic cross-section A–A'. **B.** Interpreted cross-section A–A'. The sand-prone Blue Unit has been incised by a channel-levee complex and then overlain by a thick and heavily slumped hemipelagic mudstone wedge that thickens to the west (left). The Blue Unit sands are correlated to a distinct seismic facies. The thickness of the hemipelagic mudstone above the Blue Unit does not change significantly in the north-south direction. Seismic reproduced with permission of Shell Exploration and Production Company.

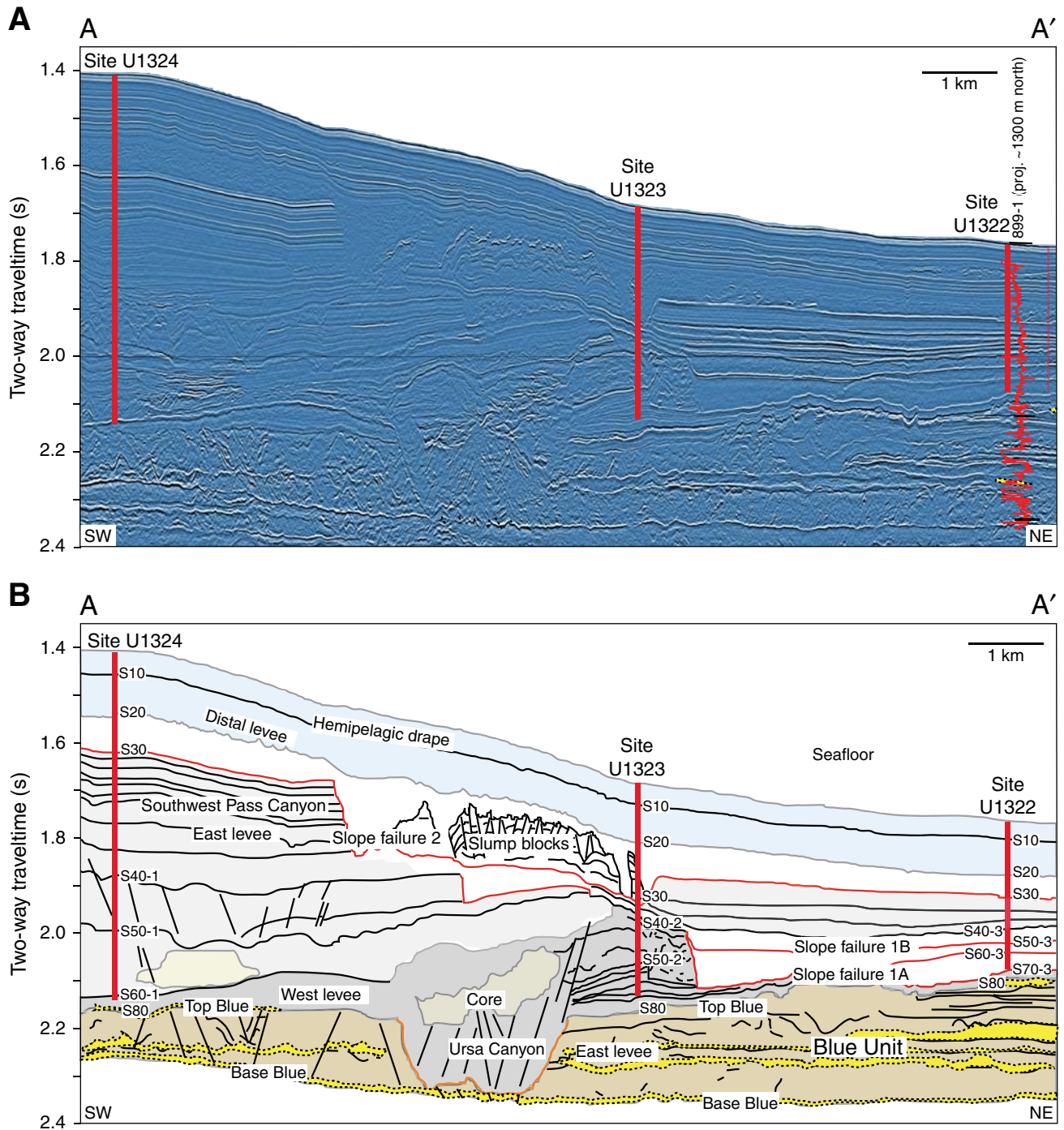


Figure F12. The T2P penetrometer is being co-developed at MIT, Pennsylvania State University, and IODP-TAMU. It is designed to measure pore pressure and hydraulic conductivity in mudstones. The plot illustrates the dissipation at both the tip and the shaft after penetration in a December 2004 land deployment in Boston Blue Clay in Newburyport, Massachusetts (USA). Excess pore pressure ratio = $(u - u_h)/(u_i - u_h)$. u = pore pressure, u_h = hydrostatic pressure, u_i = peak insertion pressure.

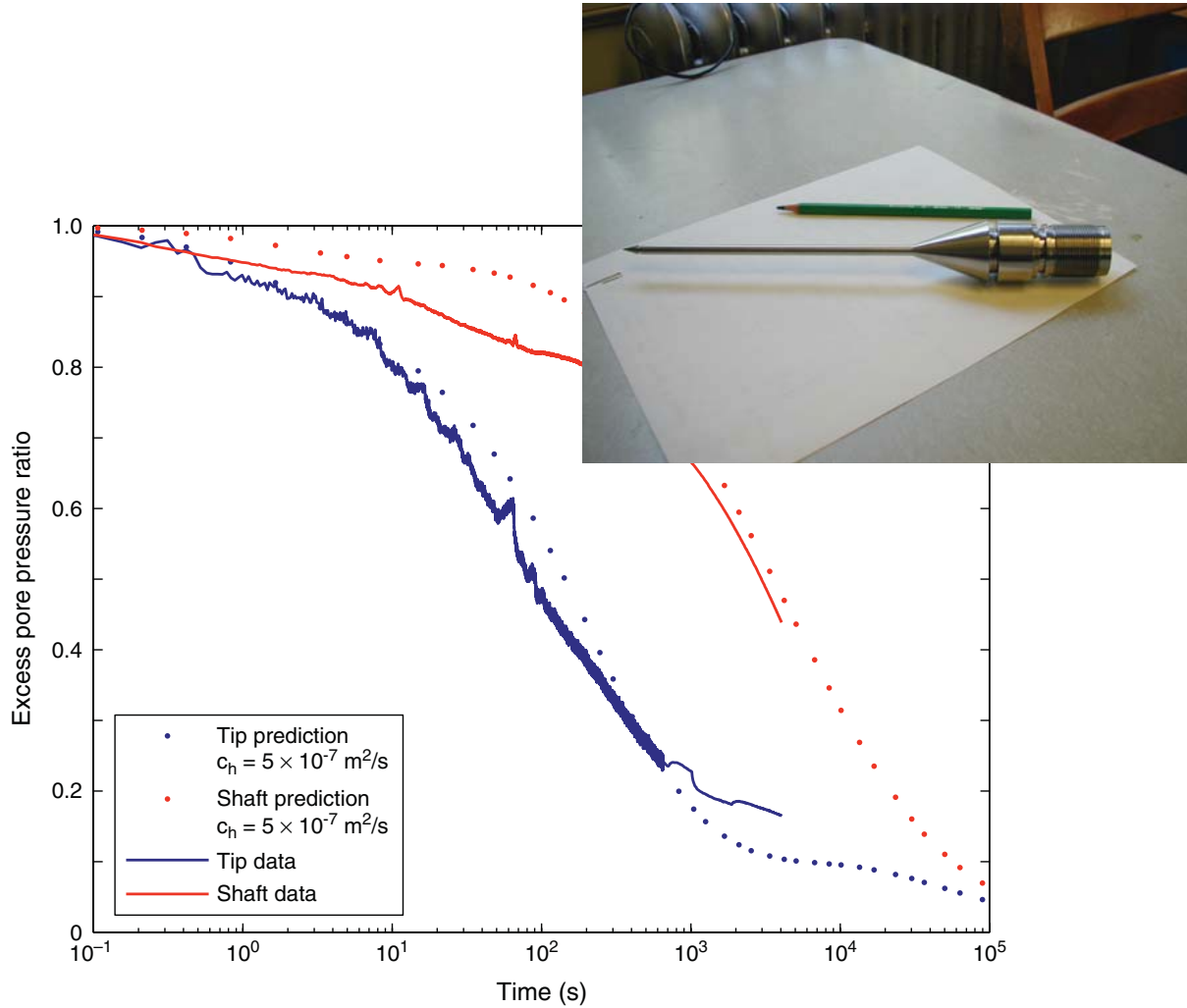


Figure F13. Combination diagram showing seismic strip chart, the lithologic column with lithostratigraphic units deduced from core description, downhole variations of gamma ray intensity and resistivity, porosity, experimentally determined peak shear strength, and headspace methane contents at Site U1319. The time-depth correlation was achieved by converting wireline logs in time using the check shots obtained in Hole U1320A.

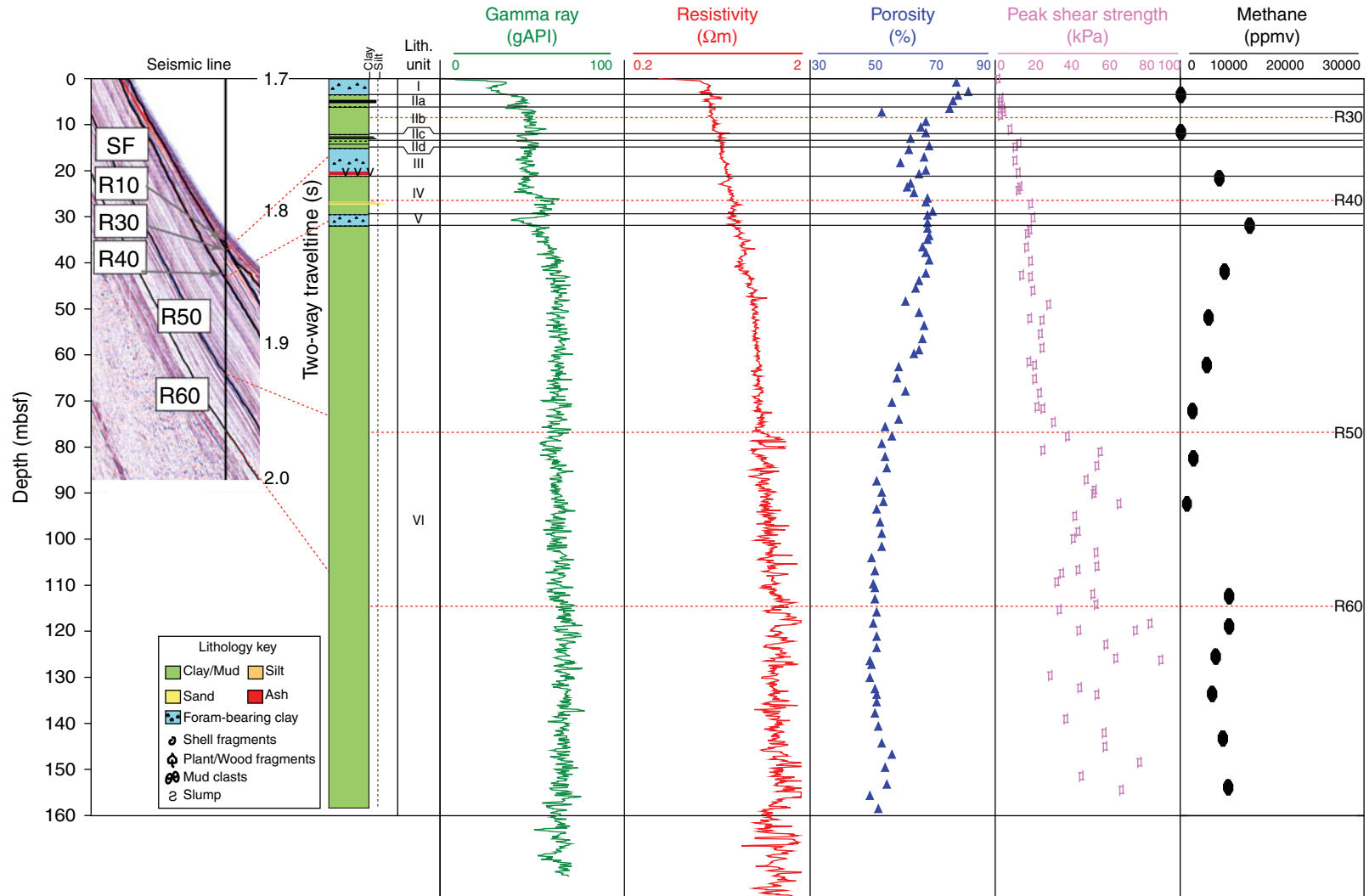


Figure F14. Combination diagram showing seismic strip chart, the lithologic column with lithostratigraphic units deduced from core description, downhole variations of gamma ray intensity and resistivity, porosity, experimentally determined peak shear strength, and headspace methane contents at Site U1320. The time-depth correlation was achieved by converting wireline logs in time using the check shots obtained in Hole U1320A.

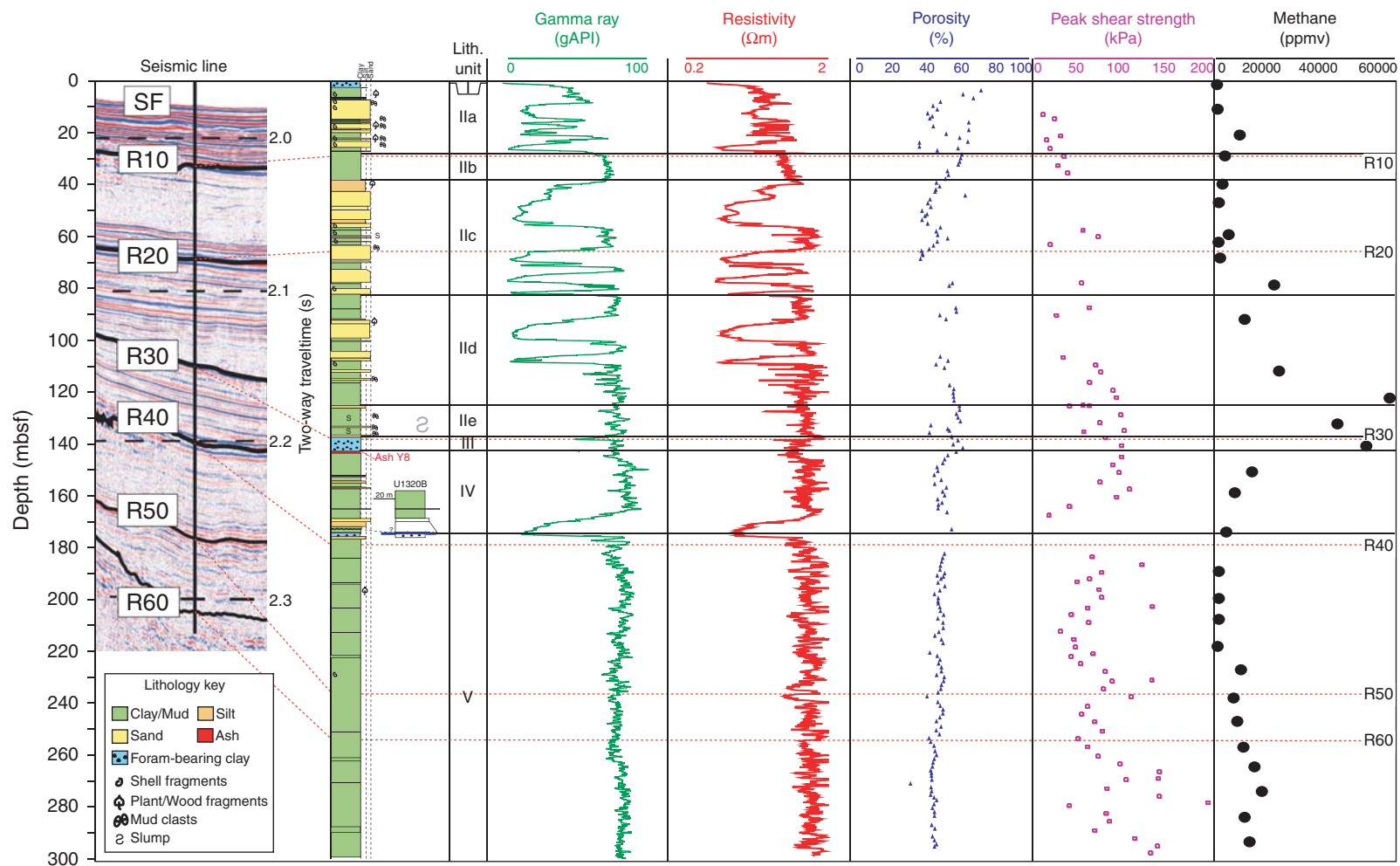
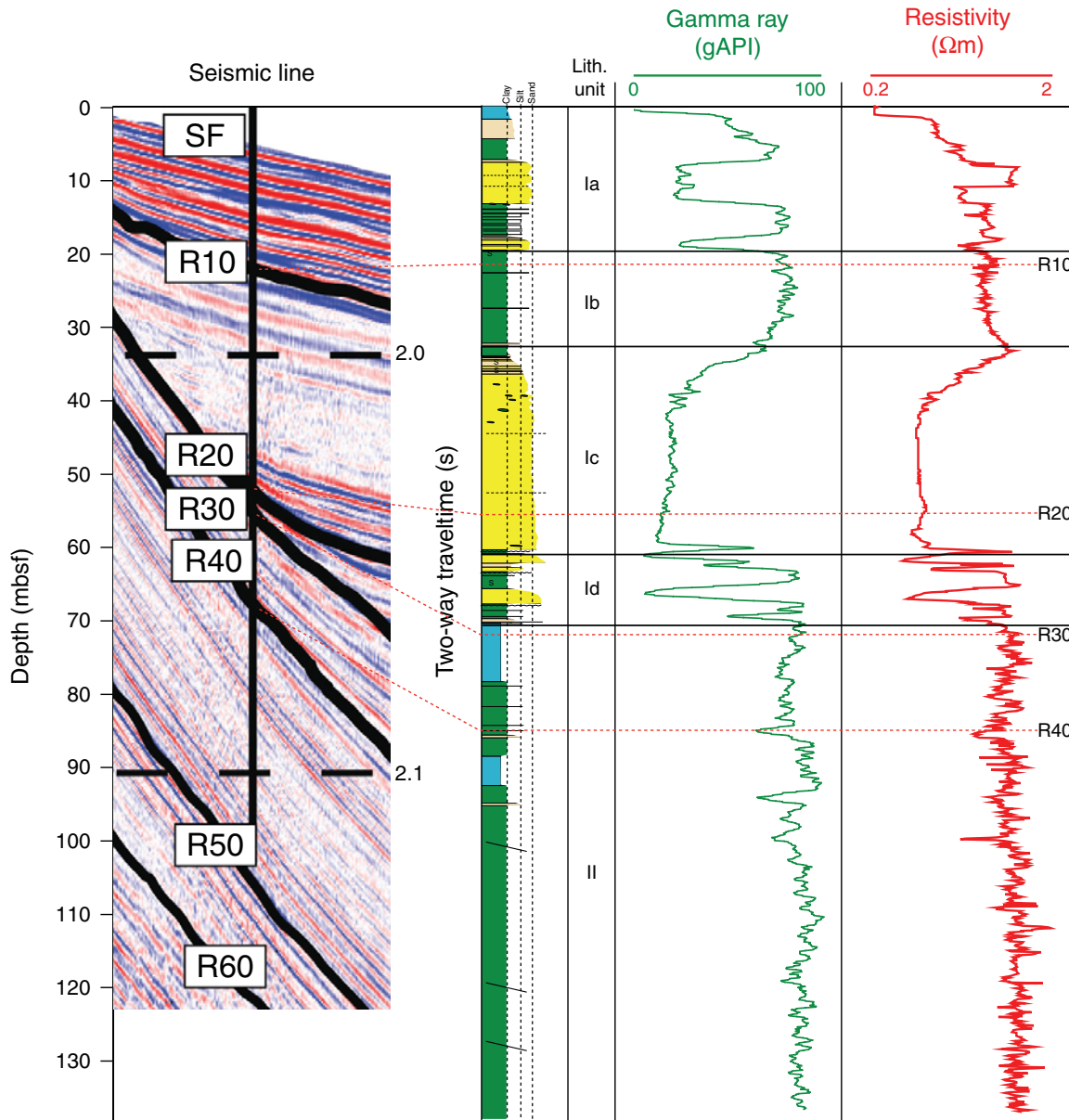


Figure F15. Combination diagram showing seismic strip chart, the lithologic column interpreted from the logging data, downhole variations of gamma ray intensity and resistivity, and log porosity at Site U1321. The time-depth correlation was achieved by converting wireline logs in time using the check shots obtained in Hole U1320A.



Lithology key

- Sand
- Mud/Clay
- Hemipelagic clay
- Silt
- Mud clast
- Deformation

Figure F16. Combination diagram showing seismic strip chart, the lithologic column with lithostratigraphic units deduced from core description, downhole variations of gamma ray intensity and resistivity, porosity, experimentally determined peak shear strength, and headspace methane contents at Site U1322.

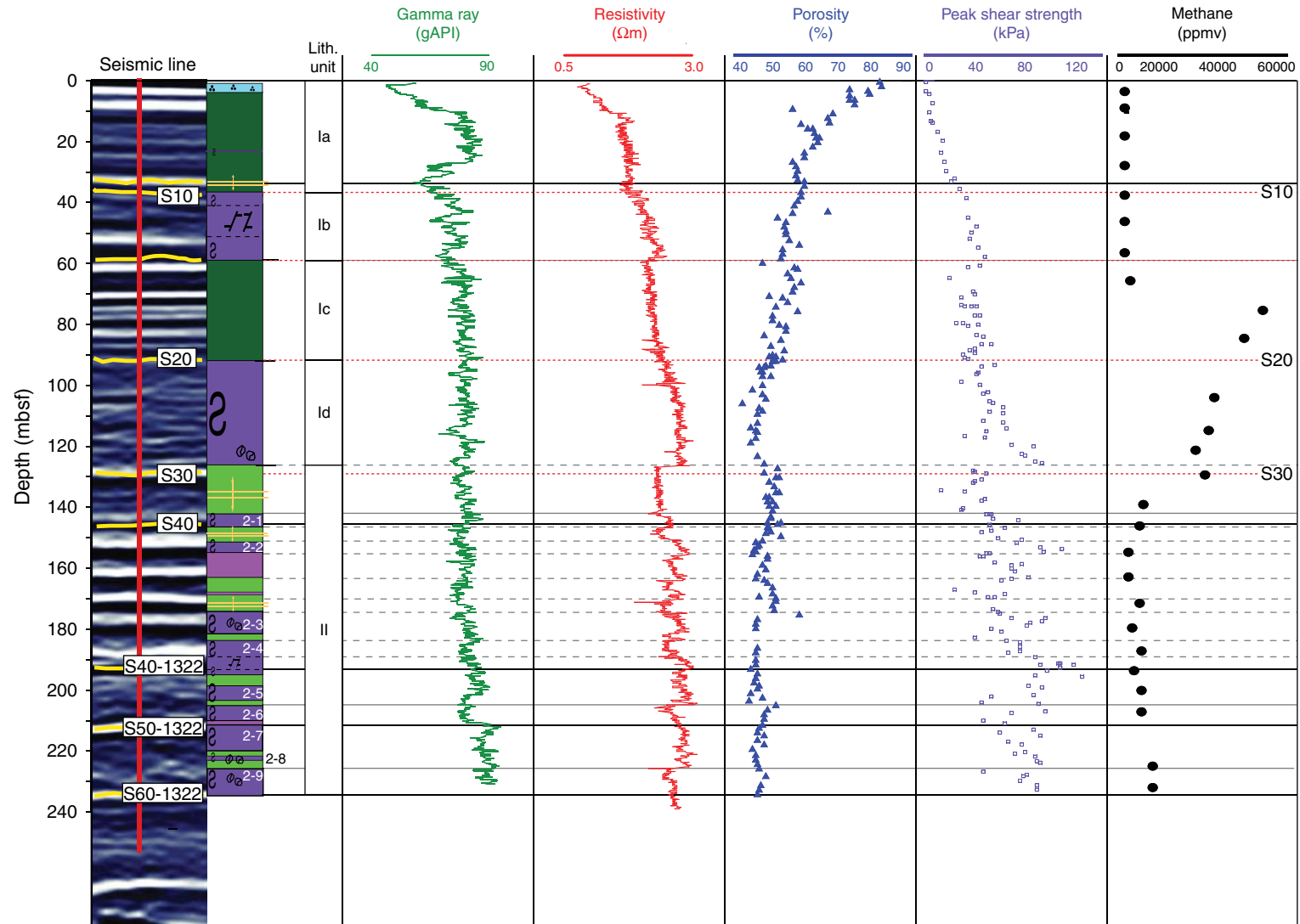


Figure F17. Combination diagram showing seismic strip chart, the lithological column interpreted from the logging data, down-hole variations of gamma ray intensity and resistivity, and log porosity at Site U1323.

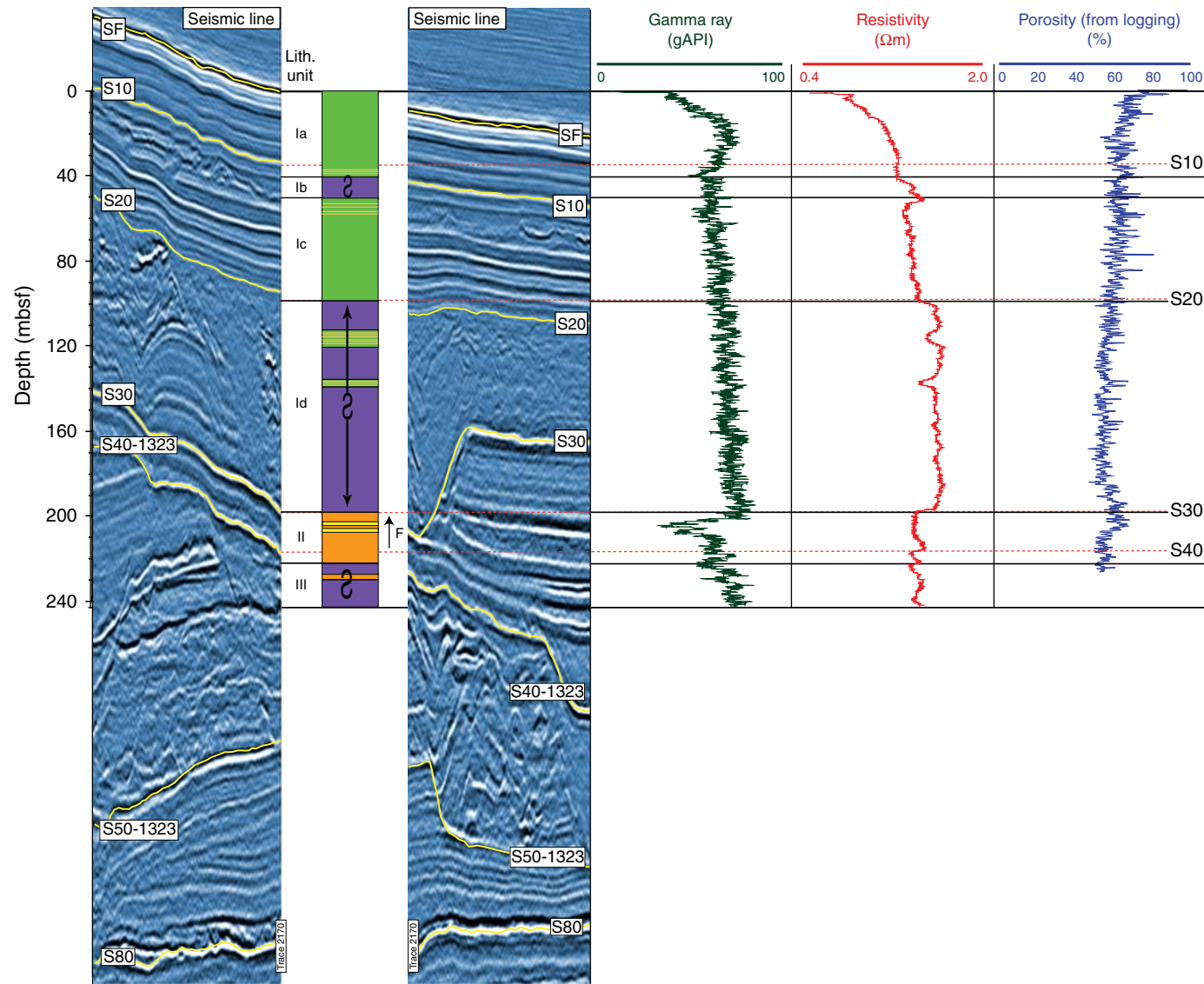


Figure F18. Combination diagram showing seismic strip chart, the lithologic column with lithostratigraphic units deduced from core description, downhole variations of gamma ray intensity and resistivity, porosity, experimentally determined peak shear strength, and headspace methane contents at Site U1324.

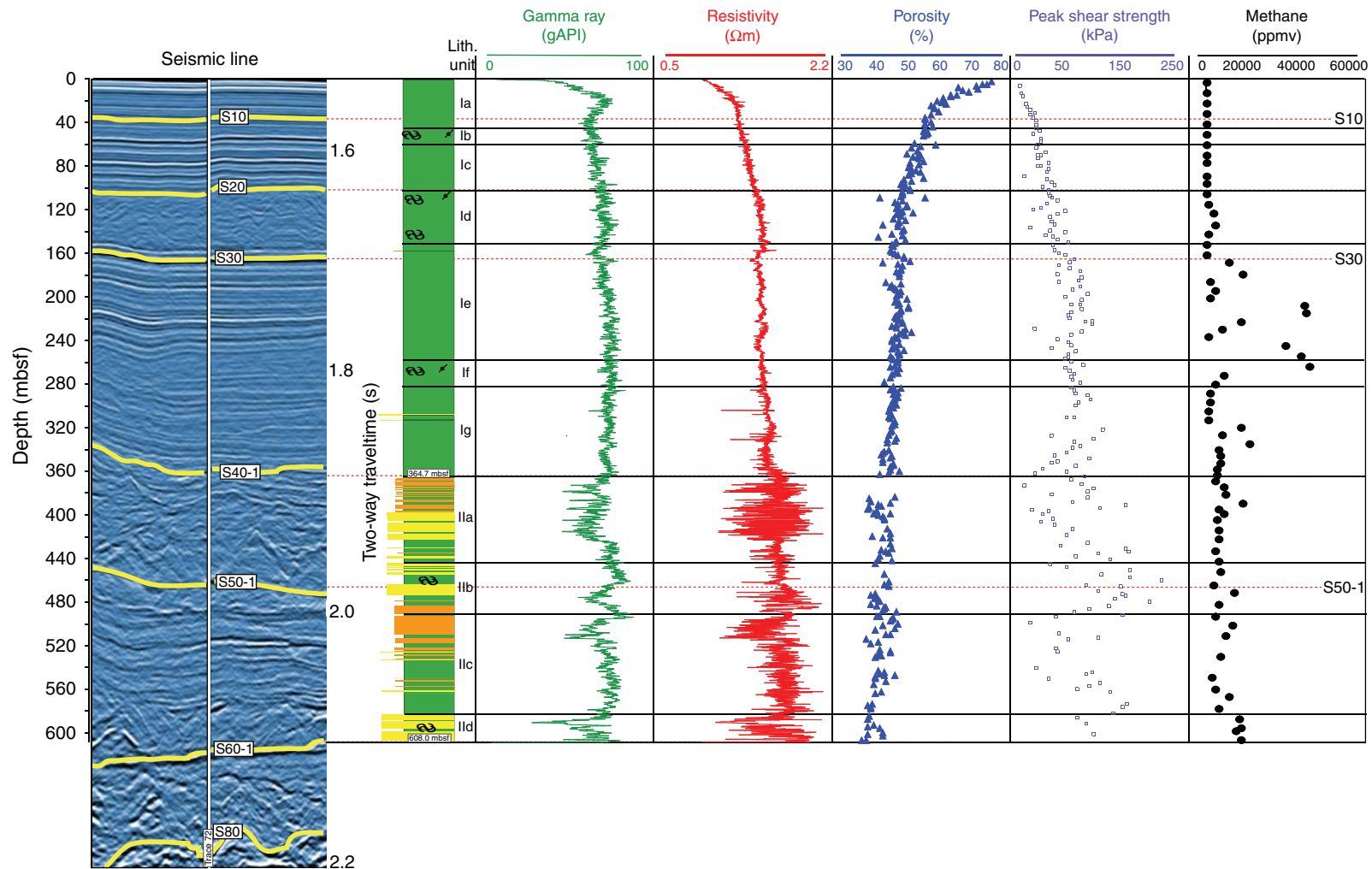


Figure F19. Mud trucks loading barite in Mobile, AL. 880 short tons (2000 lb/ton) of barite and 120 short tons of sepiolite were loaded on the *JOIDES Resolution* during port call. Up to 90% of these supplies were used during the expedition.



Figure F20. Pressure versus depth plot illustrating the effect of drilling with weighted mud. Normally the *JOIDES Resolution* drills with seawater. Thus, the borehole pressure will follow the hydrostatic pressure. If the formation is overpressured (the pore pressure is greater than the hydrostatic pressure at any depth), permeable, and unconsolidated, there is danger that there will be flow of water and sand into the borehole. To counter this effect, weighted mud was used during drilling. A 10.5 ppg mud weight raised the formation pressure to approximately one-third of the way between hydrostatic and lithostatic, whereas a 12.5 ppg mud would raise the borehole pressure to more than half of the distance from hydrostatic to lithostatic pressure.

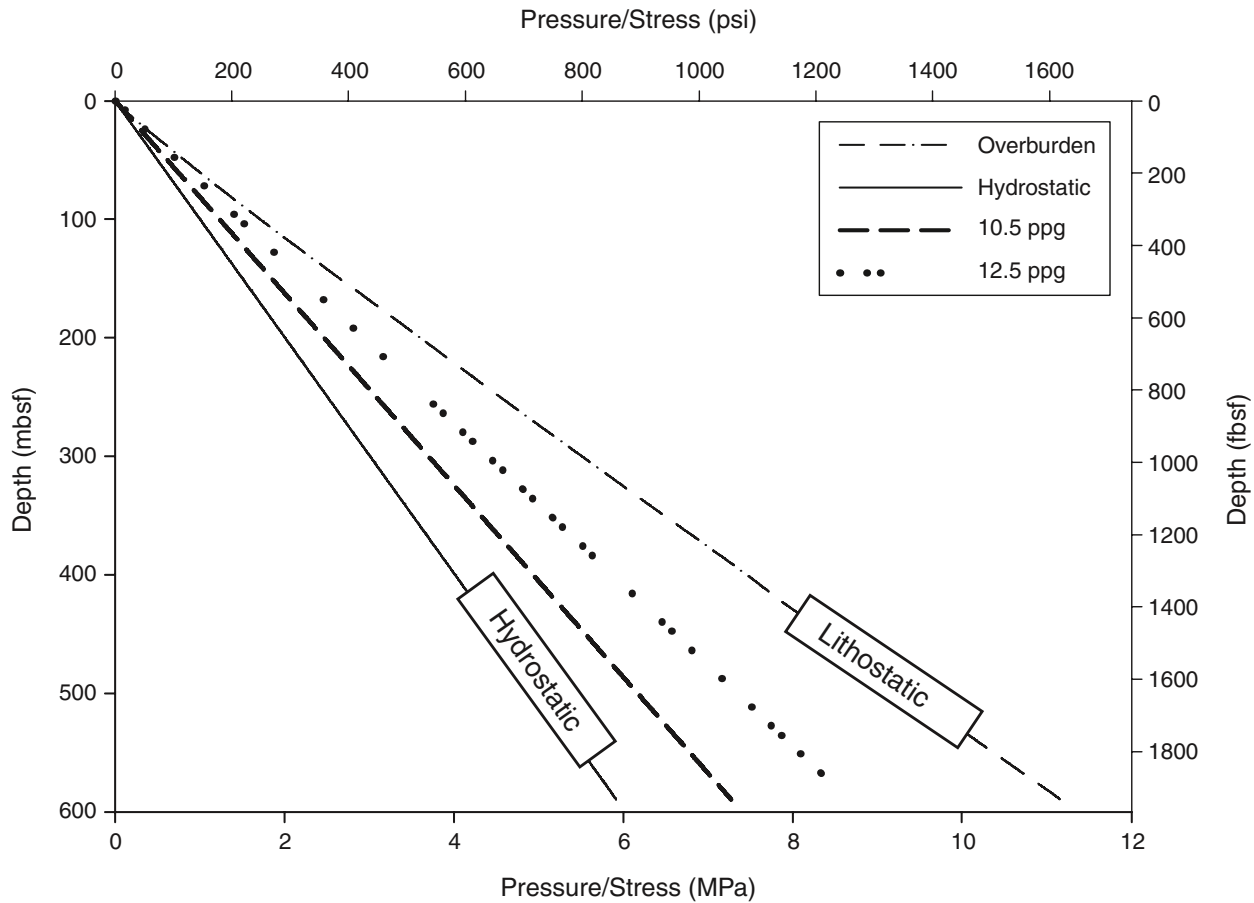


Figure F21. Measurement-while-drilling results at Site U1323. Annular pressure while drilling (APWD), annular pressure in excess of hydrostatic (APWD*), and equivalent circulating density referenced to the seafloor (ECD_{rsf}) at Hole U1323A. The ECD_{rsf} and APWD* curves show characteristic decreasing and increasing trends, respectively, over the upper 150 mbsf. At 198 mbsf, a 3 m thick sand layer recorded an increase in APWD of ~150 psi over the background drilling pressure. This was interpreted to record flow of sand into the borehole. Mud weight was raised and the well was ultimately cemented and abandoned at 238 mbsf. TWT = two-way travel time, GR = gamma radiation.

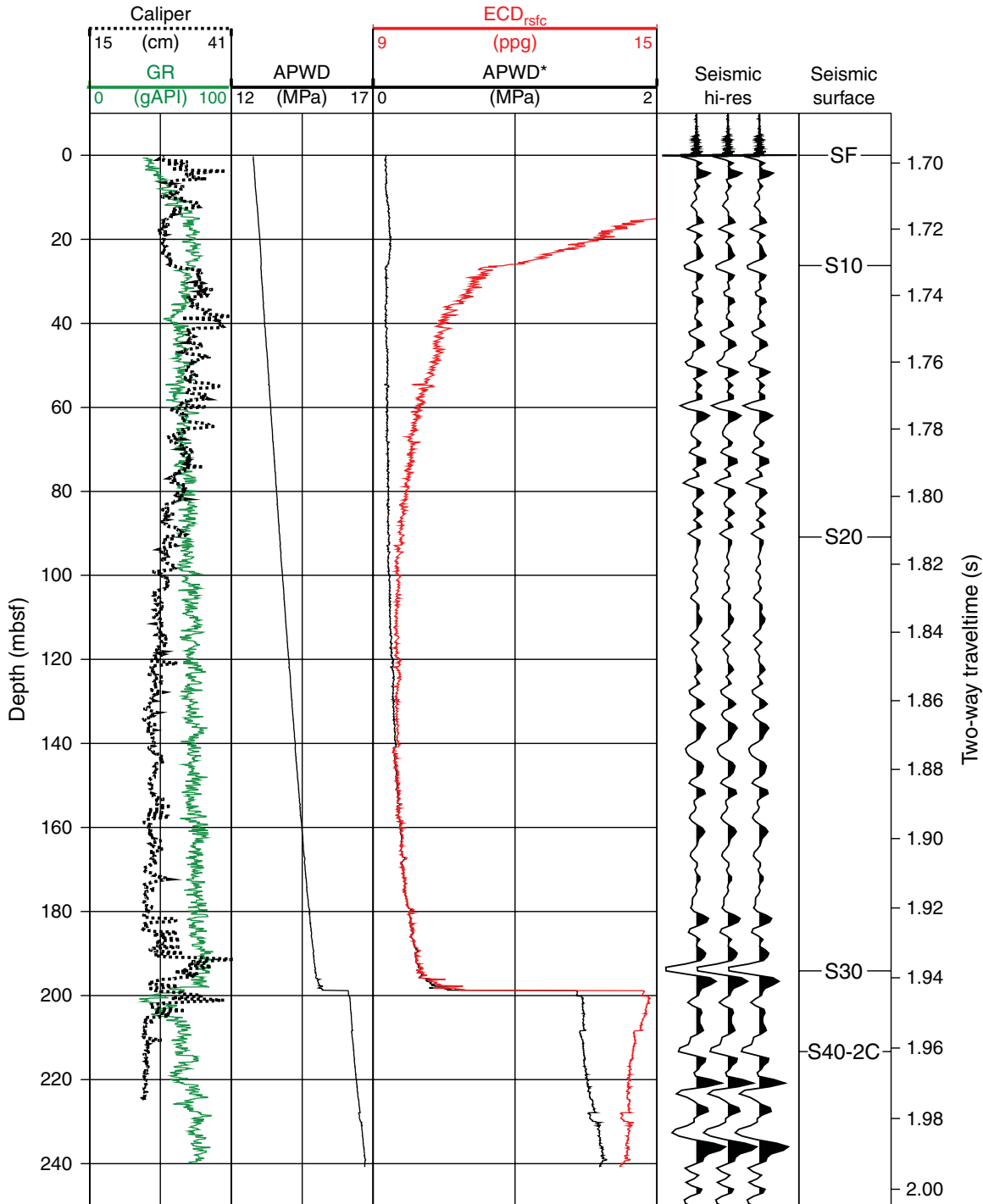


Figure F22. The T2P (foreground) and DVTTP (background). Both tools measure formation pressure by being forced into the formation by the drill string. The T2P is significantly narrower both at the tip and along the shaft than the DVTTP.

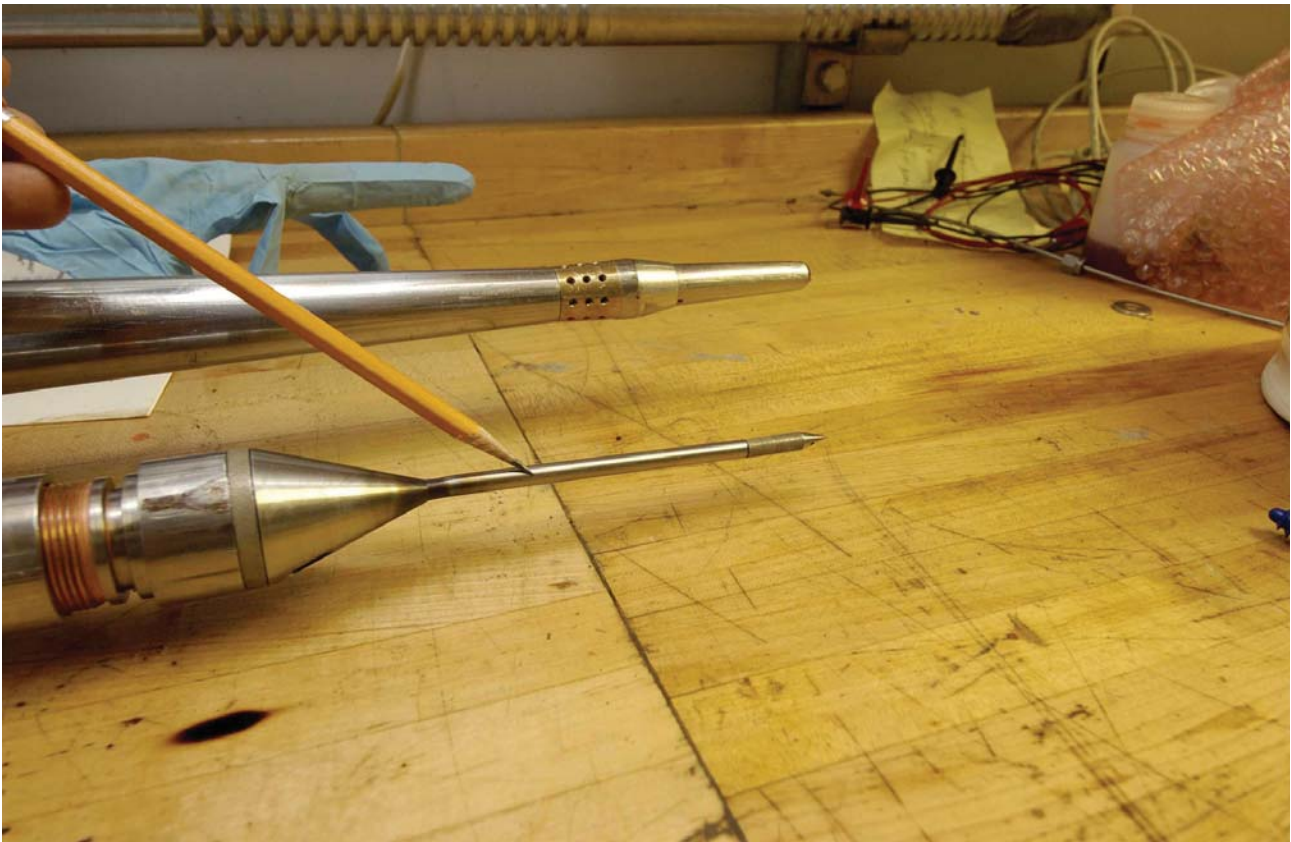


Figure F23. Characteristic deployments of the DVTPP and T2P. **A.** Good deployments are characterized by an abrupt rise during penetration and a subsequent dissipation. **B.** Fair deployment. Many deployments recorded a subhydrostatic pressure when the drill string was raised in order to decouple the probe from the ship's motion. With time, the pressure equilibrated upward toward what is inferred to be the in situ pressure. **C.** "Leak" deployments had abrupt drops in pressure during the dissipation phase. This is interpreted to result from leakage within the tool into the air-filled chambers within the tools.

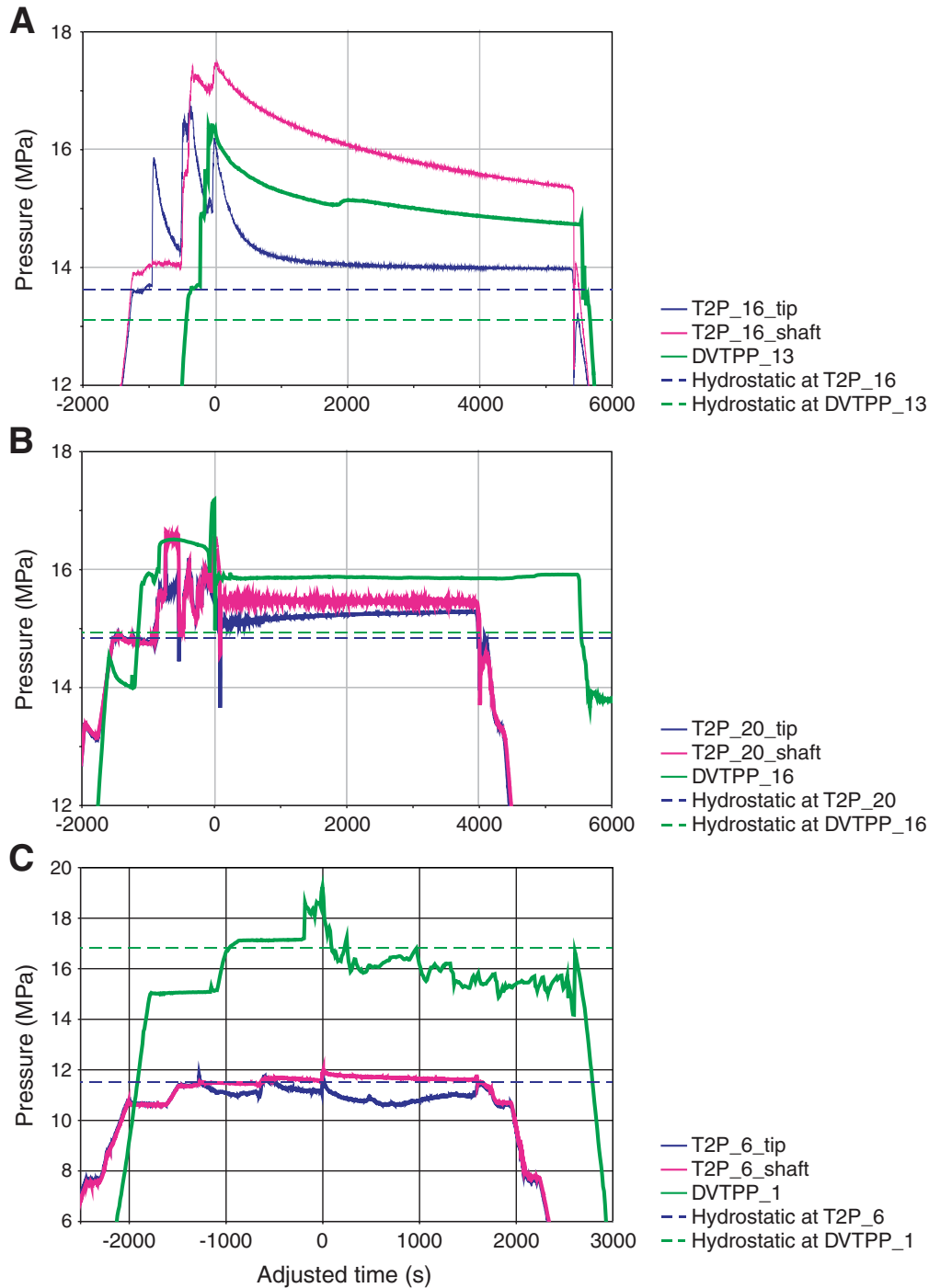


Figure F24. There were 25 T2P deployments and 20 DVTPP deployments. Good deployments are illustrated in Figure F23A. Fair deployments contain some data that will give insight into in situ pressures (Fig. F23B). Poor deployments will most likely not yield information about in situ properties. During failed deployments, no meaningful data were retrieved.

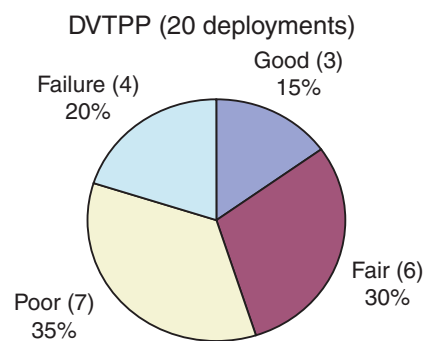
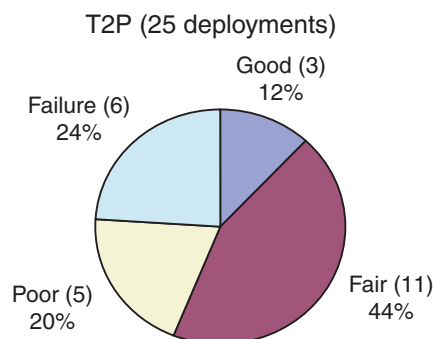


Figure F25. Illustration of the procedure for deployment of the penetration probes. **A, B.** The drill string pushes the probe into the formation. After penetration, the drill string is raised. **C.** The probe should stay in the ground and the bottom-hole assembly should slide upward as the drill string is raised a few meters. **D.** In many penetrometer deployments, when the drill string was raised it appears there was partial coupling between the drill string and tool. As a result, the tool was partially pulled out of its hole. **E.** During a successful penetration, there is an abrupt increase in pressure during penetration and then there is a slow dissipation of pressure after the tool is left in the ground. **F.** During unsuccessful deployments, the pore pressure record sharply drops during pullout. The result is a subhydrostatic pressure that gradually builds back to the formation pressure.

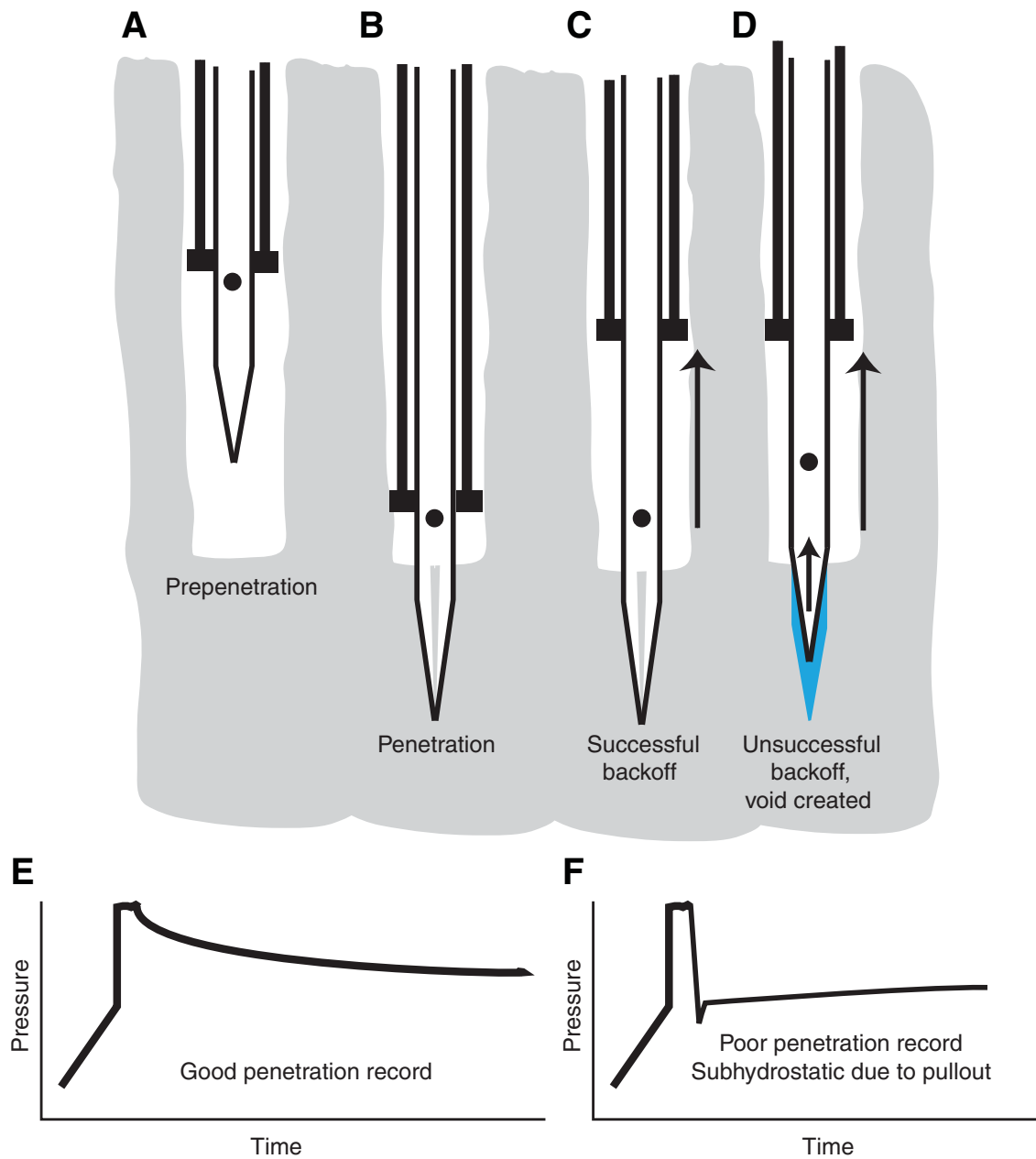


Figure F26. Dip-oriented seismic line across Brazos-Trinity Basin #4 with LWD resistivity (RING) logs. Depth scale in the well logs were converted to time using the check shot survey in Hole U1320A. This time-depth curve was also used for Sites U1319 and U1321. SF = seafloor.

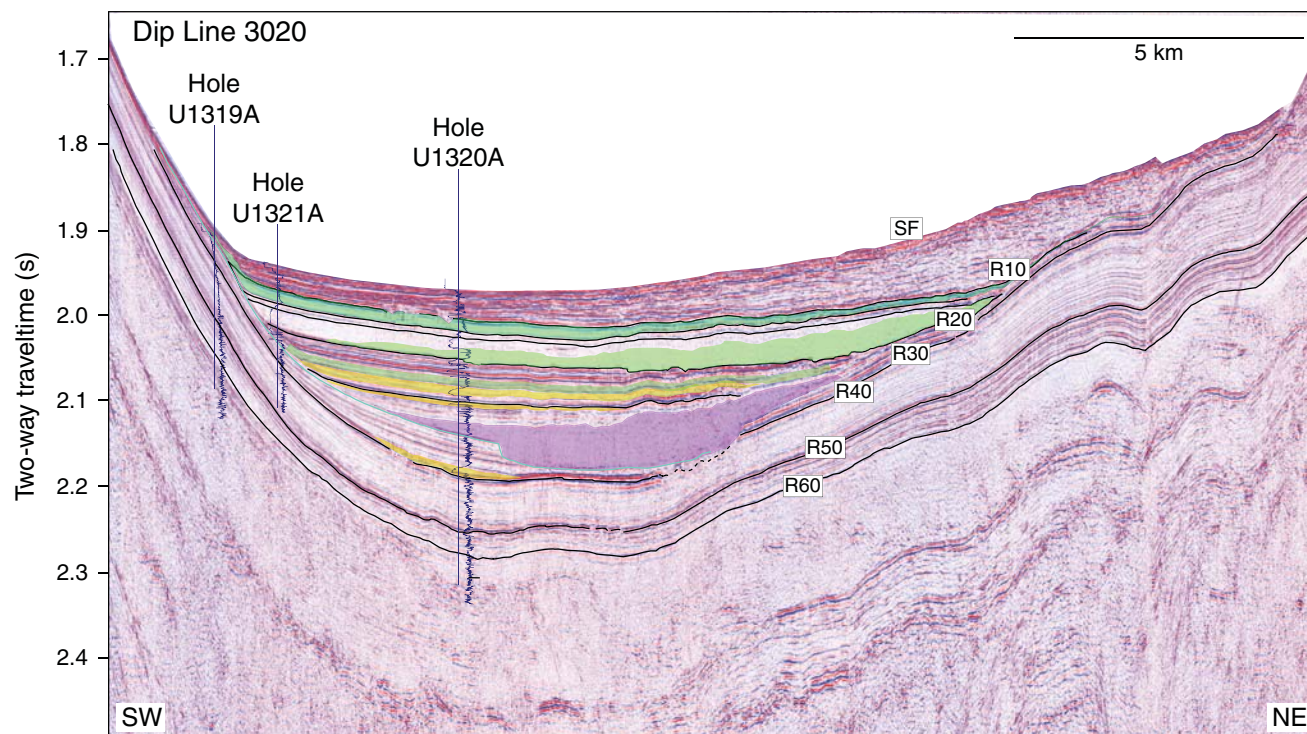


Figure F27. Strike-oriented seismic line across Site U1320 with LWD resistivity (RING) log. The logs were converted to depth using results from the check shot survey at this site. SF = seafloor.

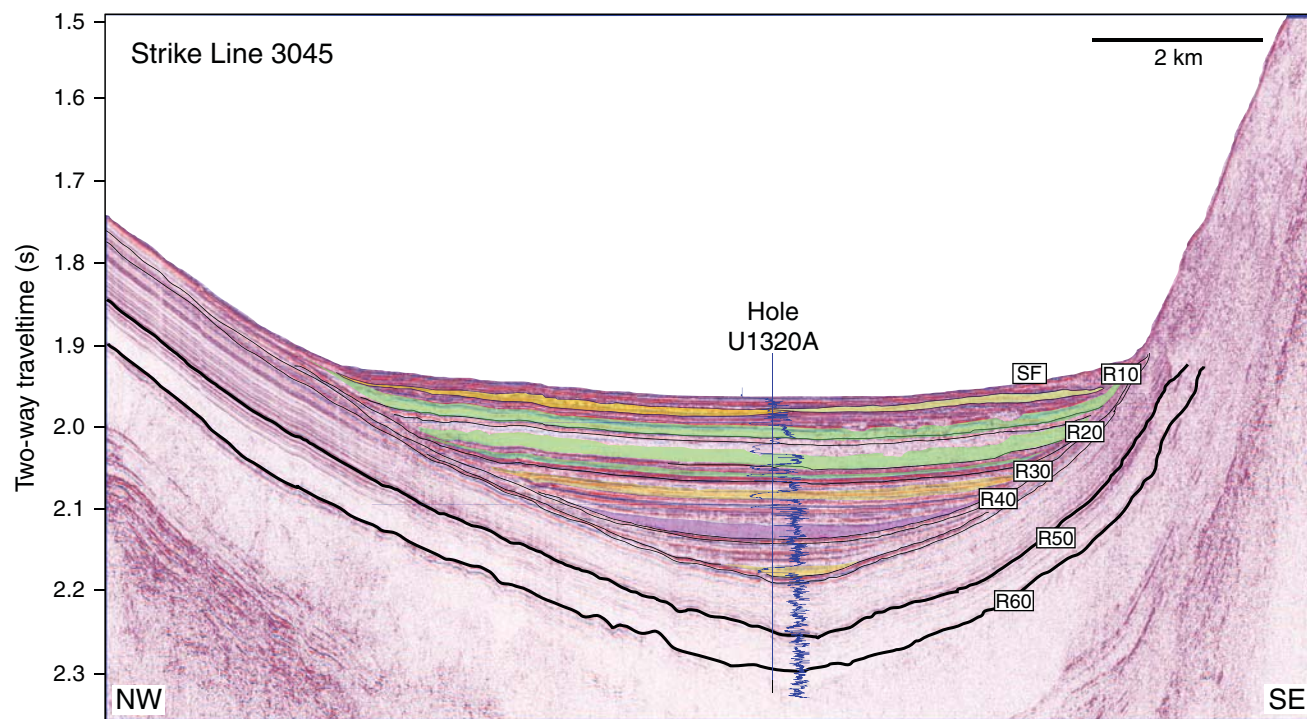


Figure F28. Preliminary age model of the basin, integrating results from planktonic foraminifers, nannofossils, and magnetostratigraphy. Lower part of the diagram shows the sea level curve of Lambeck and Chappel (2001). MIS = marine isotope stage.

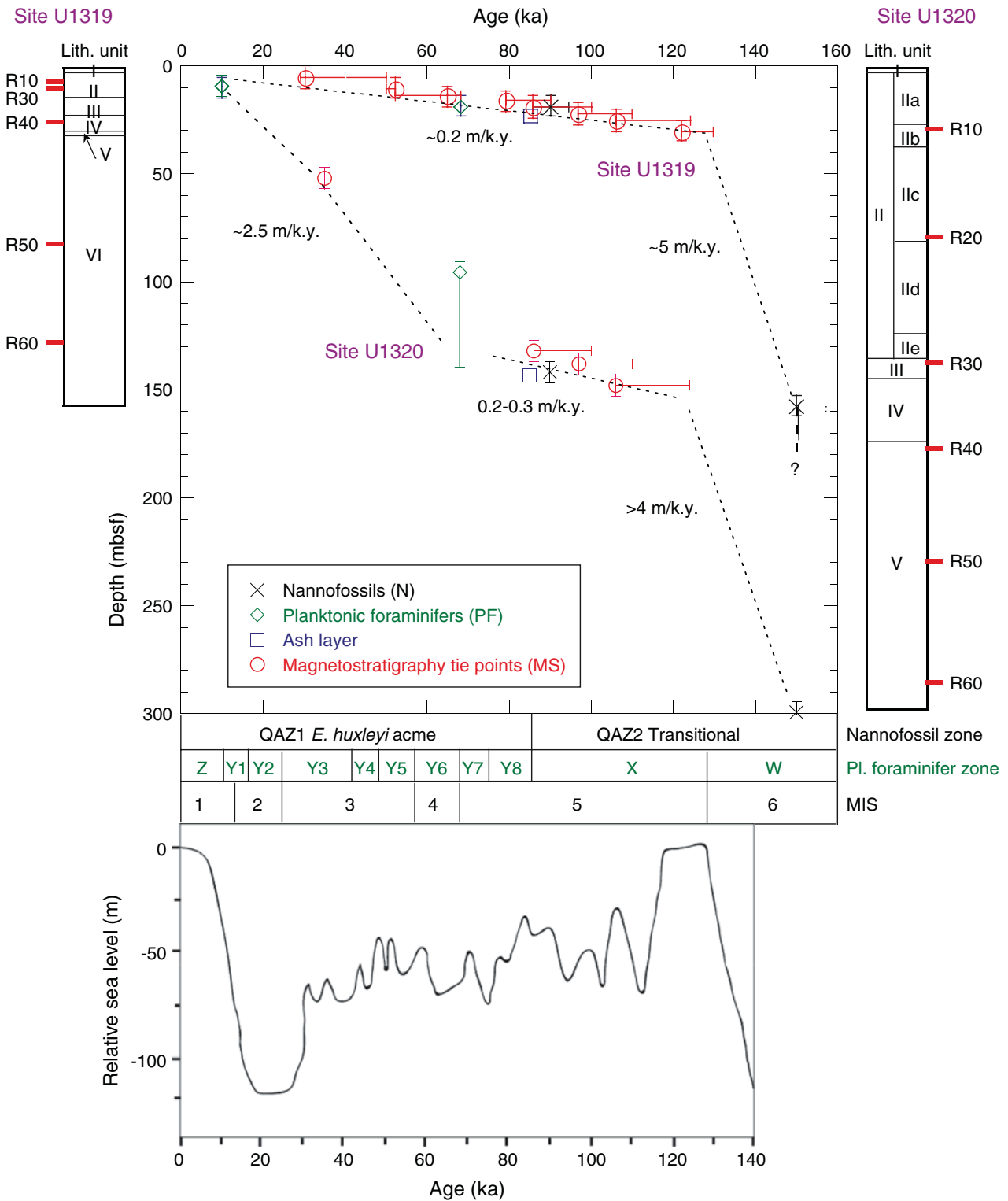


Figure F29. Stratigraphic cross-section of Brazos-Trinity Basin #4. The core and well logs are datumed at sea level. Stratigraphic ties between sites are based on seismic, lithology, log signature, and biostratigraphy. Each column contains a depth scale, a schematic lithology, gamma ray (GR) and resistivity logs (from LWD), and the depth of key seismic surfaces. In the core recovery diagram, black = cored, red = overlap due to core expansion, and white = no recovery.

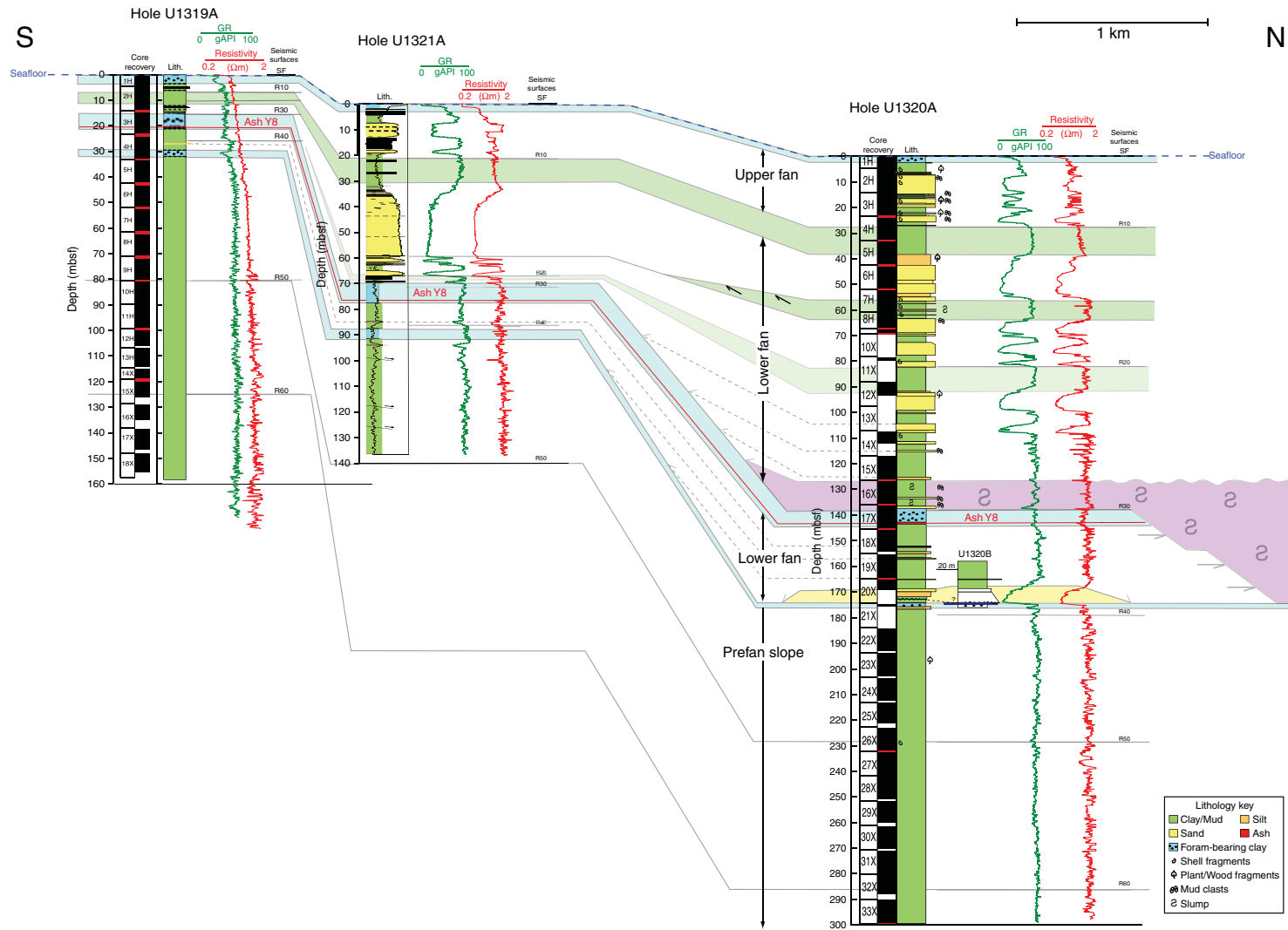


Figure F30. Selected core photographs illustrating facies encountered in each of the units. **A.** Turbidites in the upper fan sequence. **B.** Upper hemipelagic interval containing ash layer Y8 (Drexler et al., 1980; Mallarino et al., in press). Inset shows a microphotograph of the volcanic glass silt and sand. **C.** Thin-bedded turbidites in the lower fan sequence. **D.** Lower hemipelagic interval at the base of Brazos-Trinity Basin #4. **E.** Laminated and bioturbated mud in the prefan sequence.

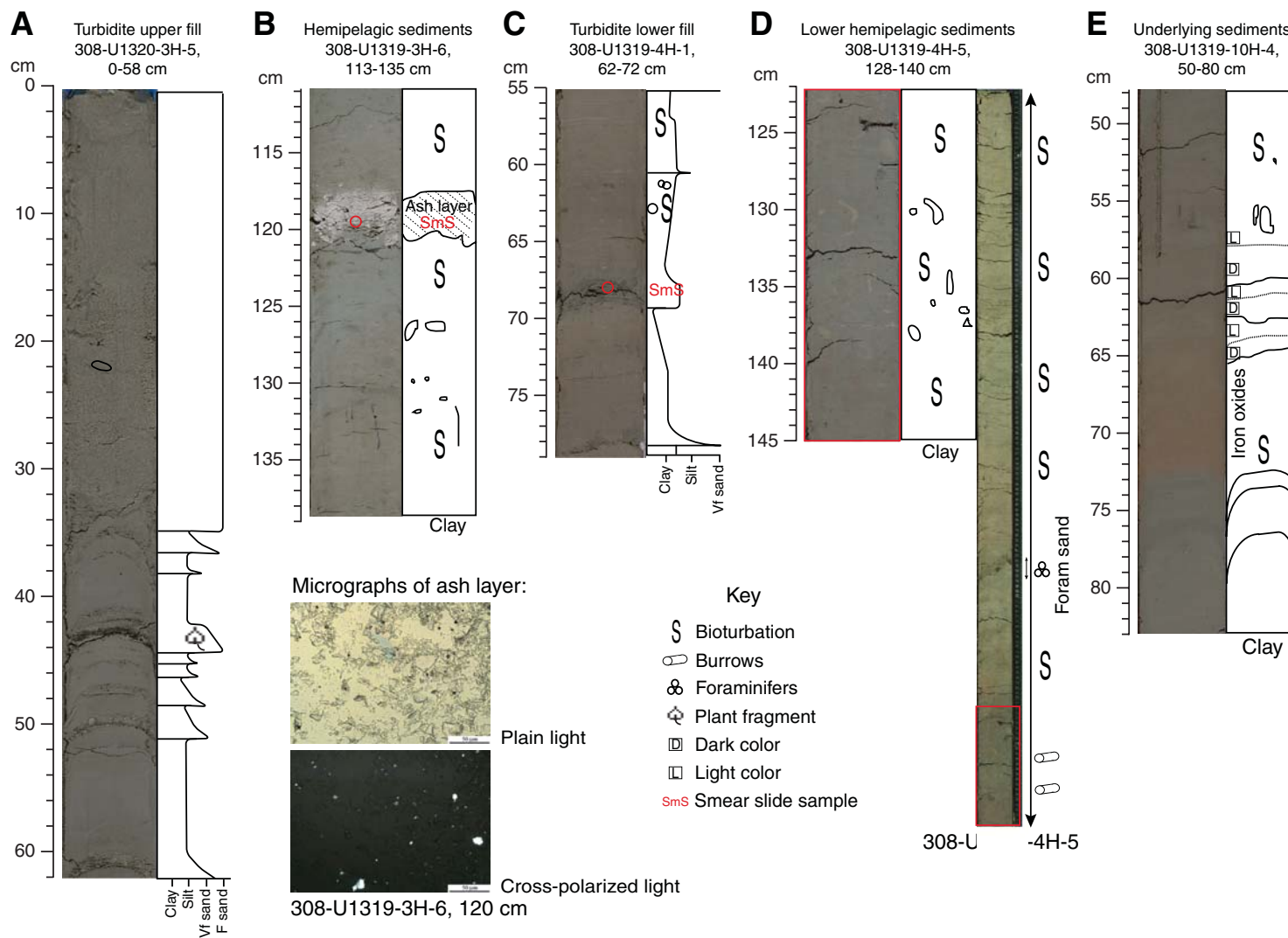


Figure F31. Lithostratigraphic, LWD resistivity, and seismic reflector correlation between Sites U1322, U1323, and U1324. Seismic Reflectors S10–S30 can be traced through all sites and encompass a consistent sedimentary environment of mud and clay deposition interspersed with two mass transport events. Below S30, sediments at Site U1324 are characterized by the onset of conspicuous turbidite deposition in lithostratigraphic Unit II, whereas Site U1322 shows a concentration of mass transport deposits in lithostratigraphic Unit II. Because the bases of Sites U1322 and U1324 (see Fig. F32) are approximately the same age, the contrasting deposits represent approximate time-equivalent facies.

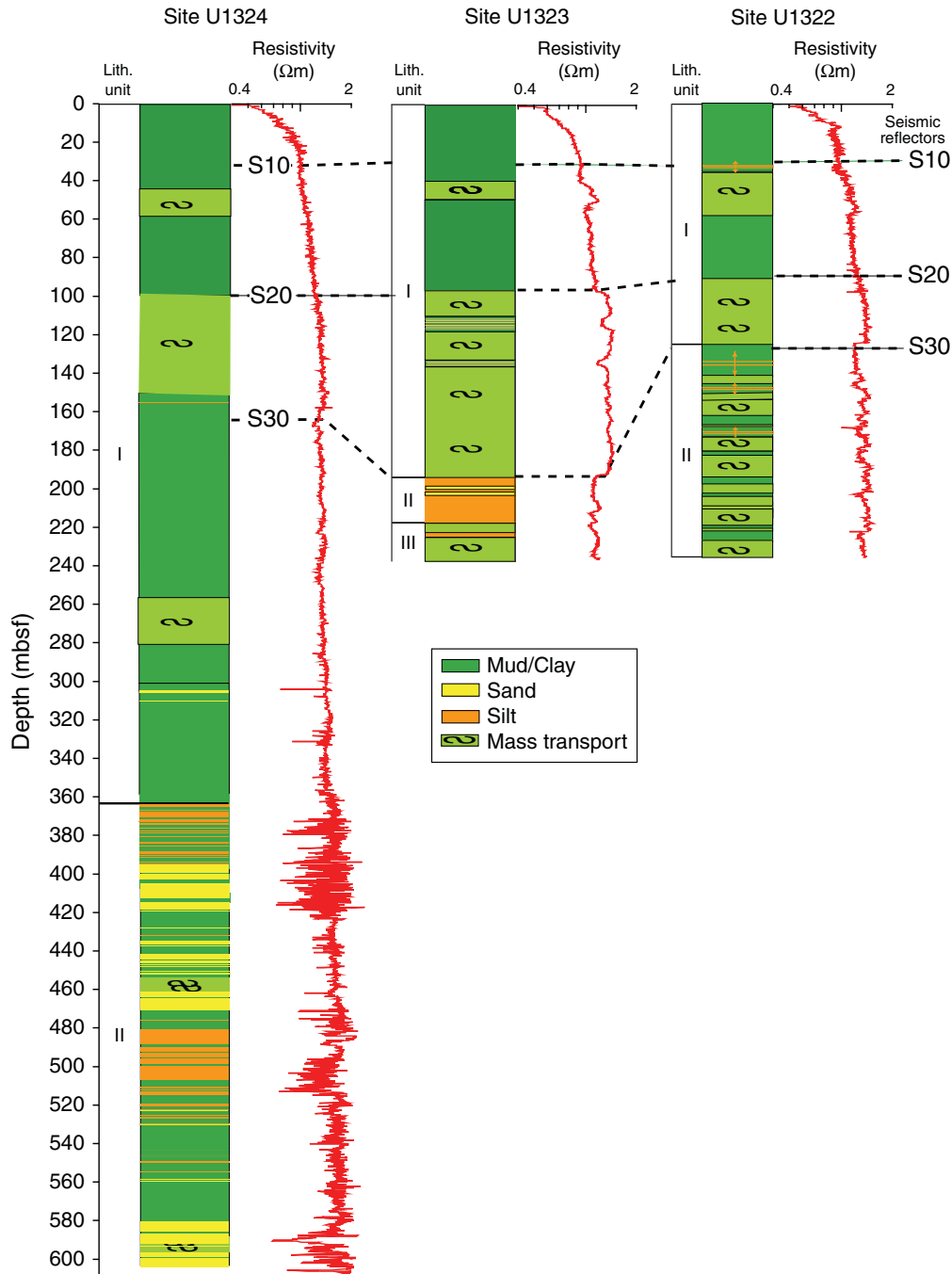


Figure F32. Summary of age constraints from microfossils and magnetostratigraphy from Sites U1322 and U1324. Black dashed line shows best-estimate age curve from cores that is additionally projected to the base of the Blue Unit. The Blue Unit was not penetrated during Expedition 308, but its age is estimated from industry penetration in the area (Winker and Booth, 2000). Sediment accumulation rates are similar at both sites from present to about 24 ka, then diverge below. The turbidite deposition at the base of Site U1324 accounts for a much higher rate of sedimentation than that observed over a similar time interval at Site U1322. MIS = marine isotope stage, LAD = last-appearance datum.

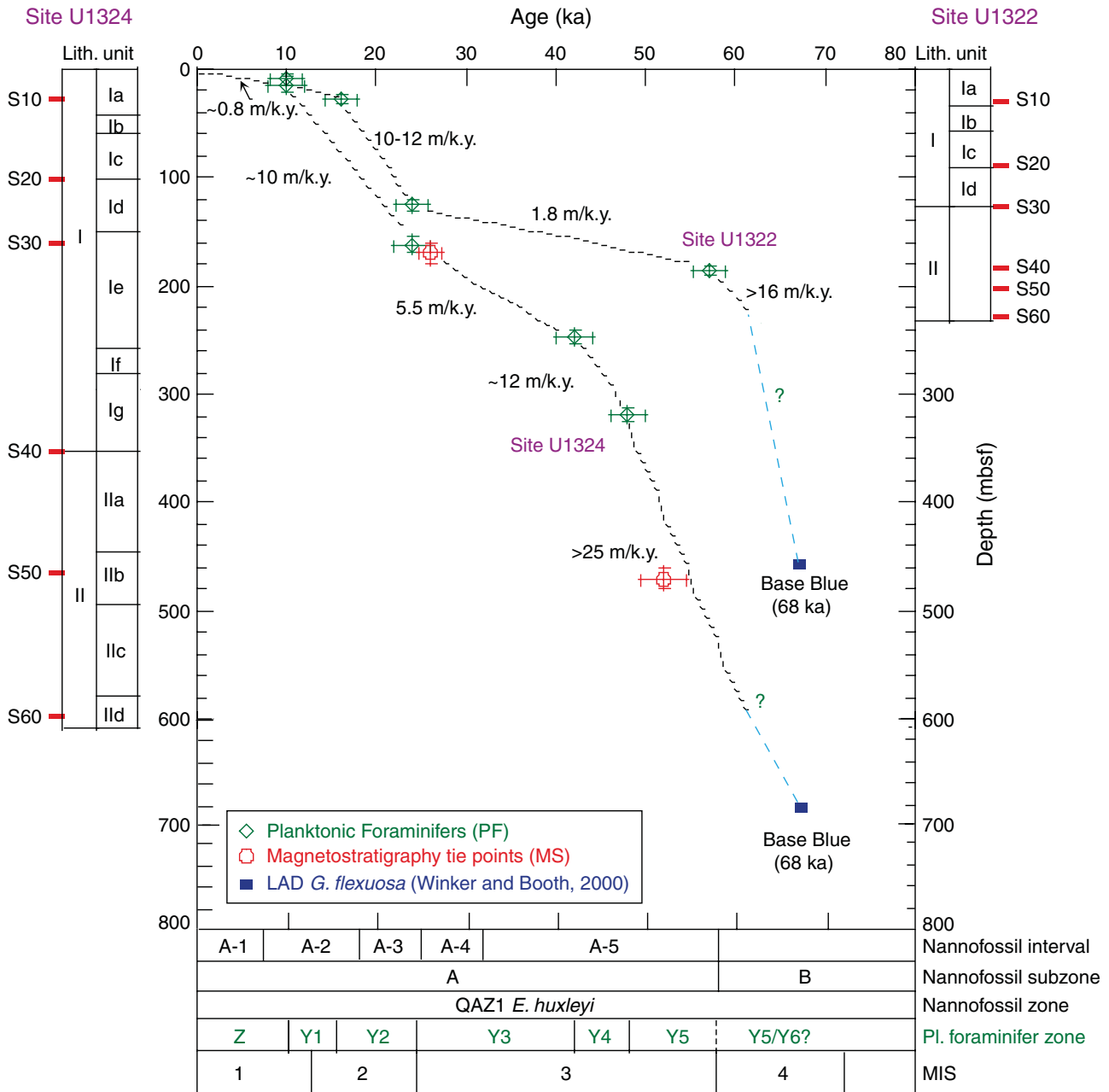


Figure F33. Seismic data and line-drawing interpretation of Sites U1322, U1323, and U1324. Ages in ka are estimated from biostratigraphy. Note the continuity of layers above Reflector S30 and below S80. Between these reflectors, the depositional system shows contrasts across the Ursa Canyon east levee deposits. The latter may have formed a high that partitioned deposition. LAD = last-appearance datum.

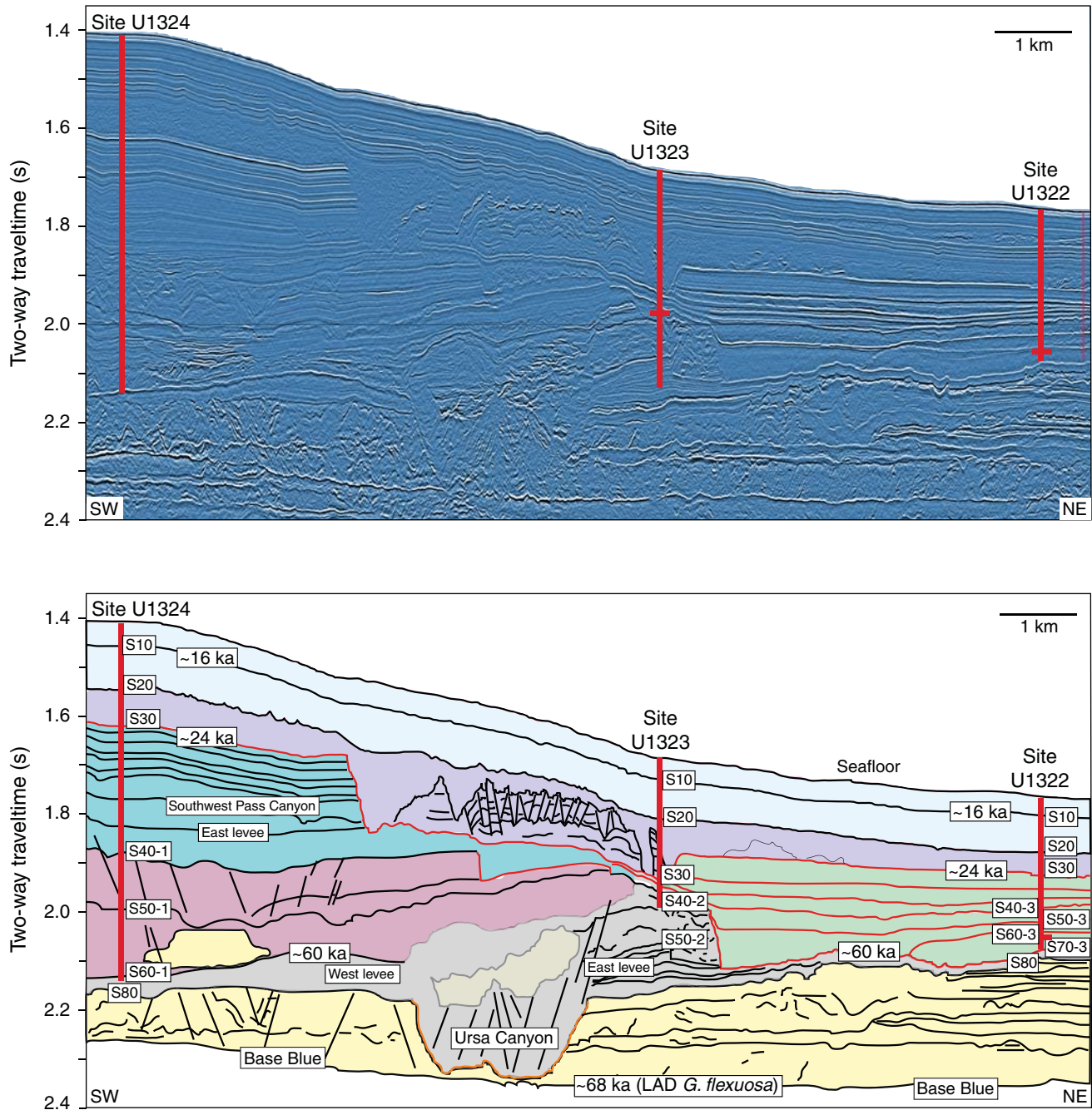


Figure F34. Summary of diagnostic features of mass transport deposits in the Ursa Basin. At seismic scale, mass transport deposits are characterized by discontinuous reflections and of transparent to low amplitude. At logging scale, mass transport deposits typically show increased resistivity and increased density, presumably due to transport-induced compaction. In resistivity-at-bit imaging, folds are apparent. Finally, at core scale, folding is common in mass transport deposits, some with half-wavelengths of a meter or more.

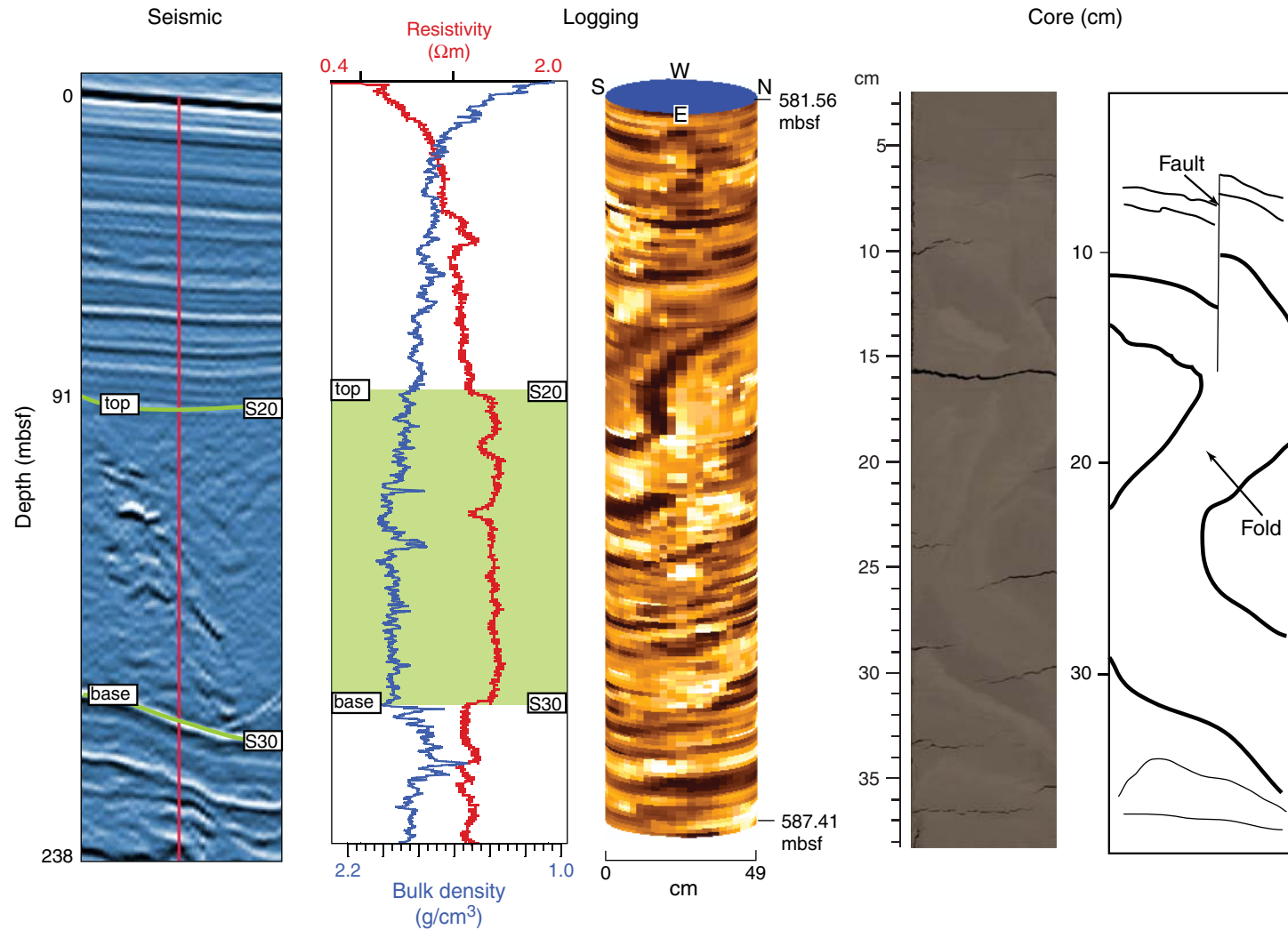


Figure F35. Porosity versus depth below Reflector R40 at Sites U1319, U1320, and U1321 from moisture and density (MAD) and logging-while-drilling (LWD) measurements. Main seismic reflectors are shown on the right.

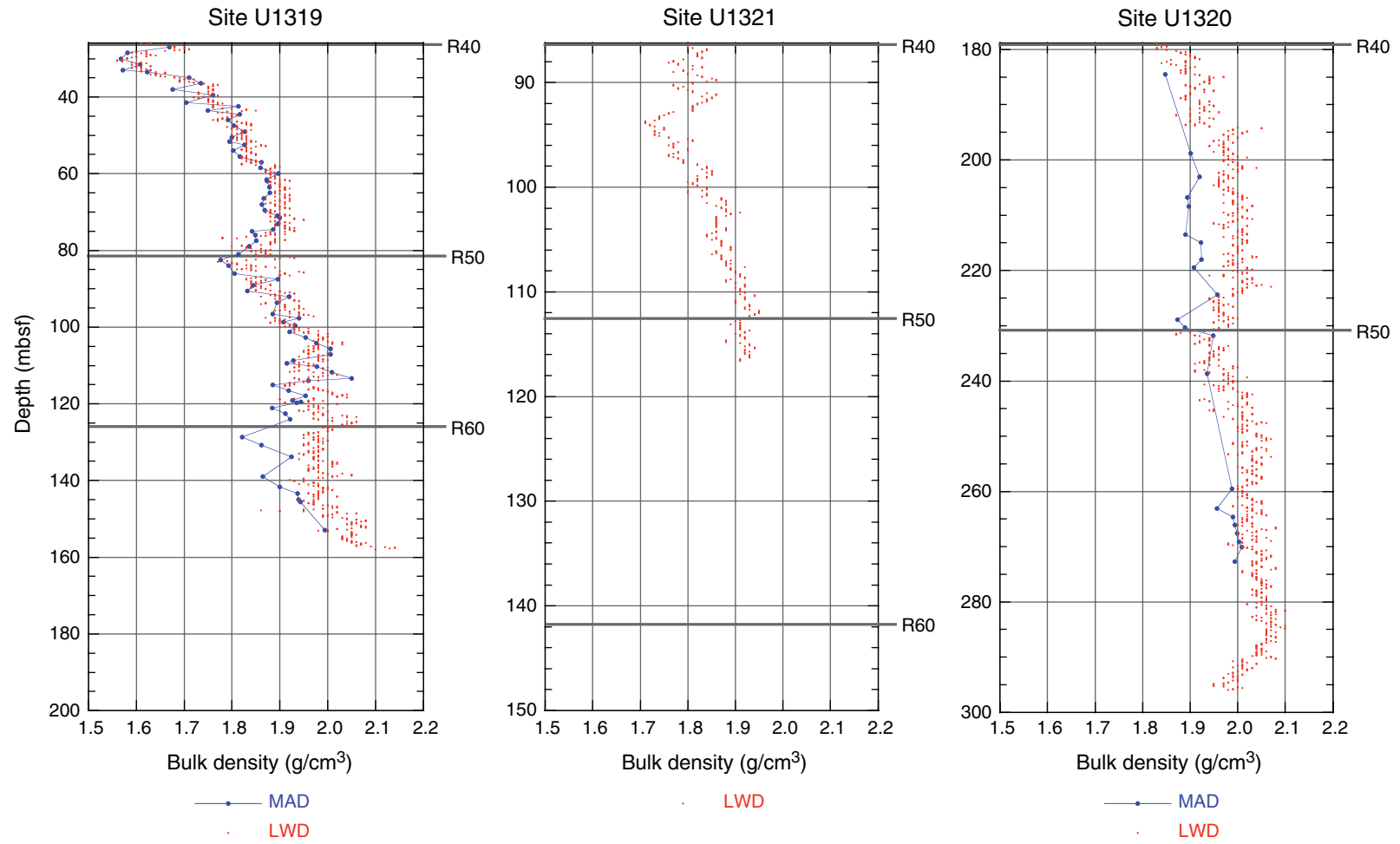


Figure F36. A. Void ratio (e) versus hydrostatic vertical effective stress (σ'_{vh}) for all sediments below Reflector R40 at Sites U1319 and U1320. The reference void ratio (e_0) and compression index (C_c) are derived from a fit of the type $e = e_0 - C_c \ln(\sigma'_{vh})$. B. Pore pressures for Site U1322 and U1324 are derived from parameters derived in A. assuming that trend at Site U1319 is hydrostatically pressured. Pore pressures recorded at the end of temperature and dual pressure probe (T2P) deployment are also shown. BSF = below seafloor.

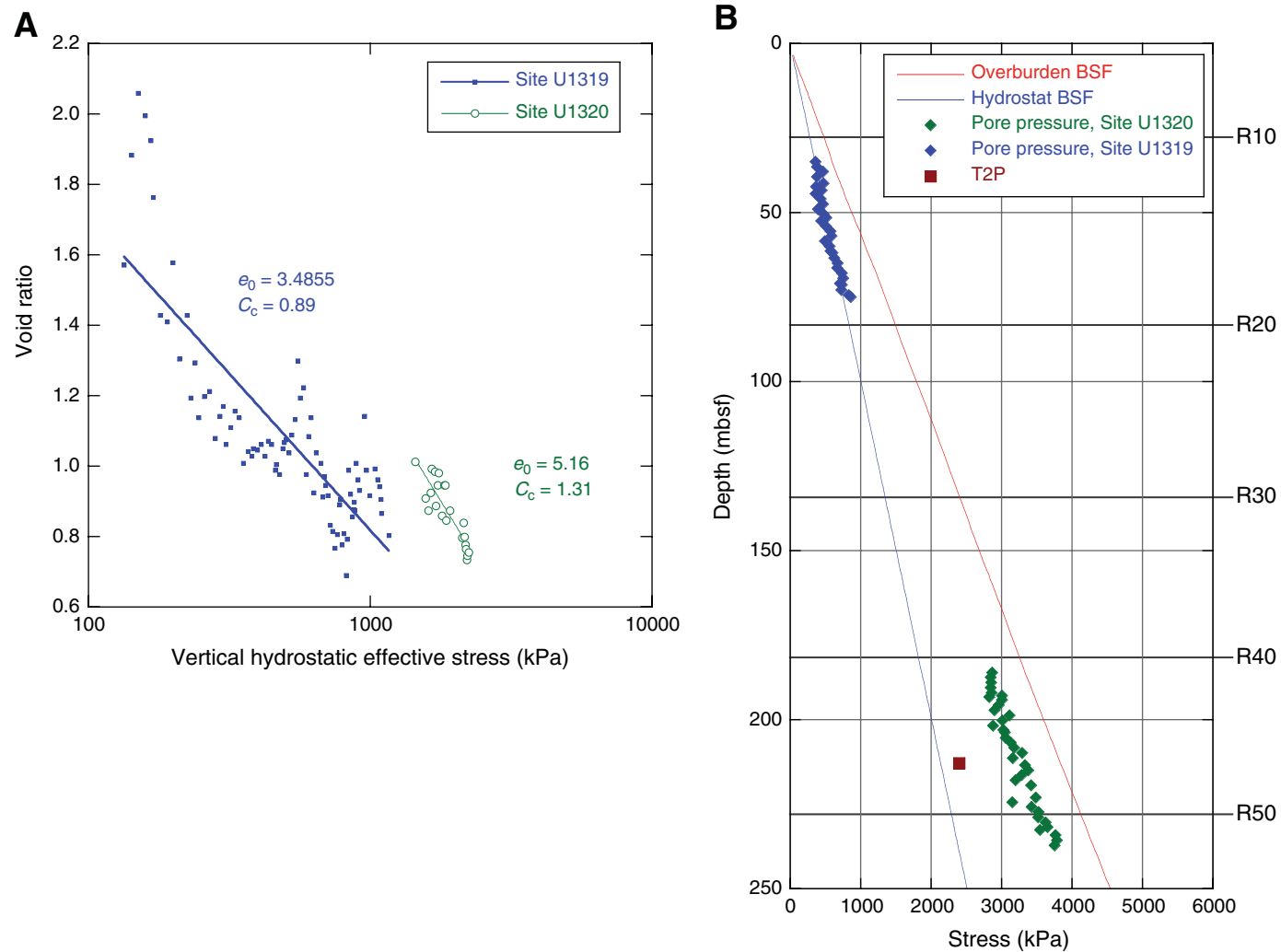
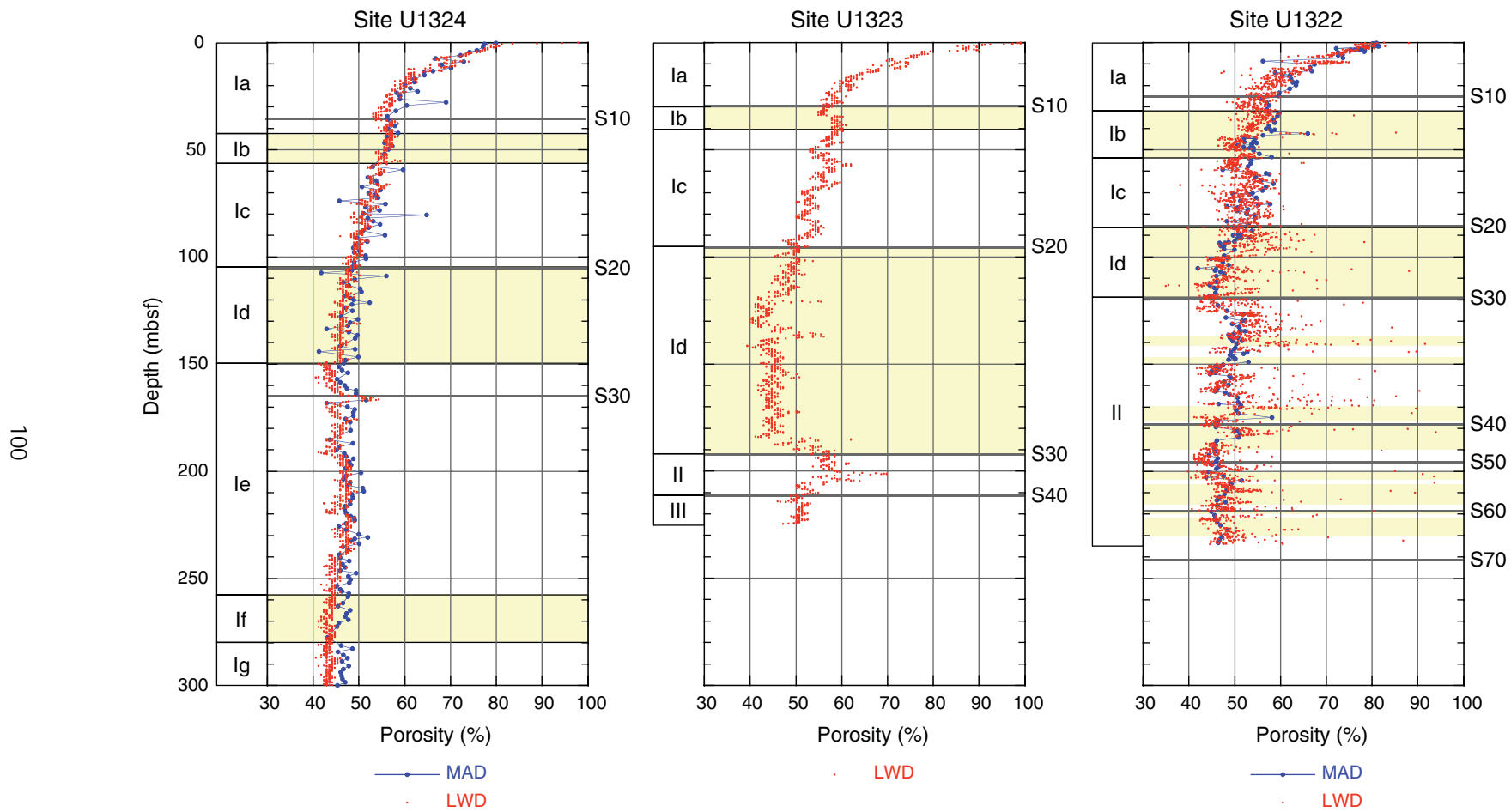


Figure F37. Porosity versus depth at Sites U1322, U1323, and U1324 from moisture and density (MAD) and logging-while-drilling (LWD) measurements. The boxes on the left are the lithostratigraphic units; seismic reflectors are plotted on the right. Slump intervals are shaded.



100

Figure F38. A. Void ratio (e) versus hydrostatic vertical effective stress (σ'_{vh}) for lithostratigraphic Subunit Ic at Site U1324. The reference void ratio (e_0) and compression index (C_c) are derived from a fit of the type $e = e_0 - C_c \ln(\sigma'_{vh})$. **B.** Pore pressures for Site U1322 and U1324 are derived from parameters derived in A. assuming that lithostratigraphic Subunit Ic (blue dots) at Site U1324 is hydrostatically pressured. Pore pressures recorded at the end of temperature and dual pressure probe (T2P) (red triangles) and Davis-Villinger Temperature-Pressure Probe (DVTPP) (red squares) deployments are also shown. BSF = below seafloor, RM = running mean, PP = pore pressure.

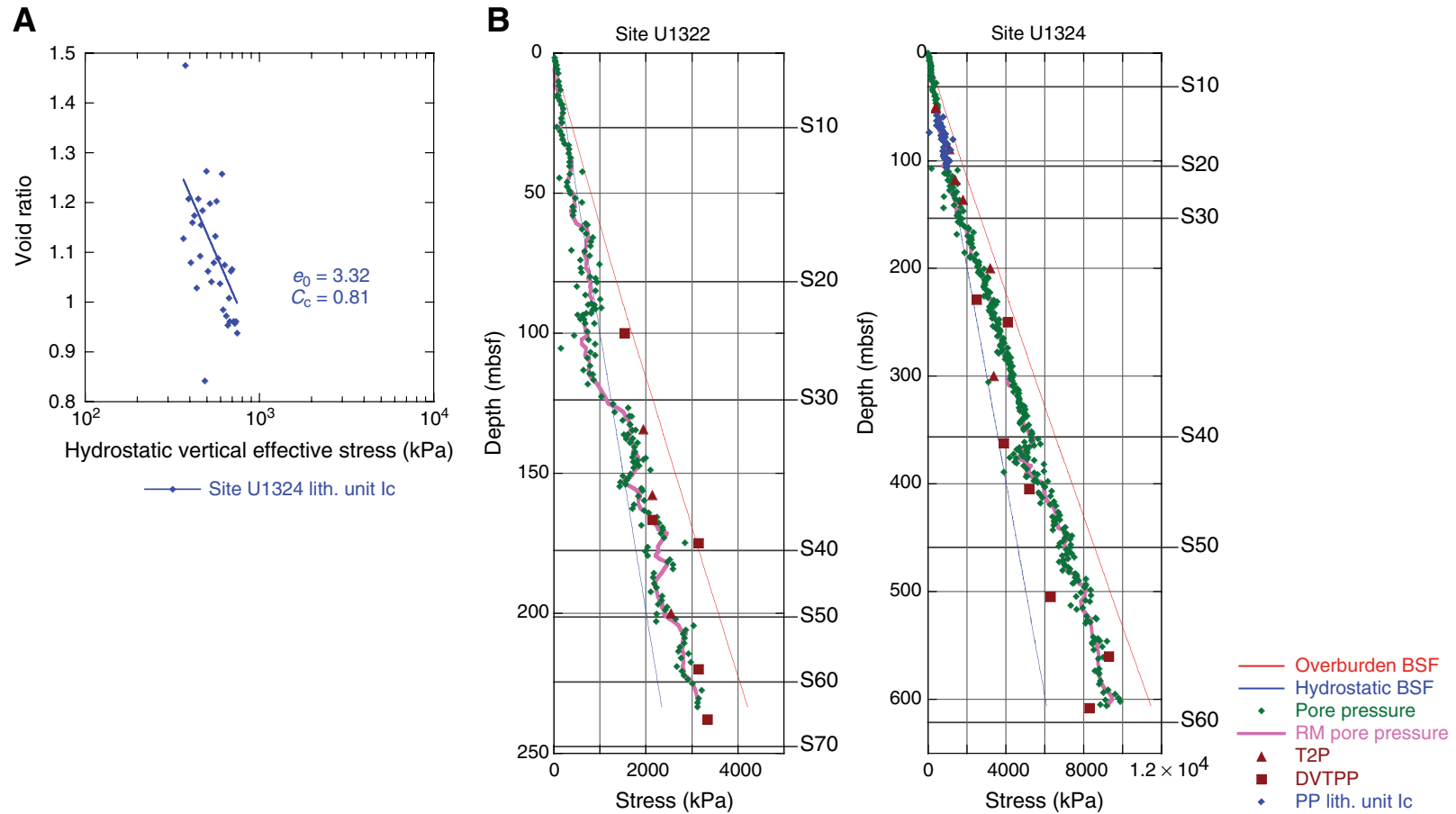


Figure F39. Porosity versus depth at all Ursa Basin and Brazos-Trinity Basin #4 sites from LWD data. The values associated with washout zones as indicated from the caliper log are not shown. Sites U1319 and U1320 are located in Brazos-Trinity Basin #4 and the sites in the Ursa Basin are represented by the data from Site U1324.

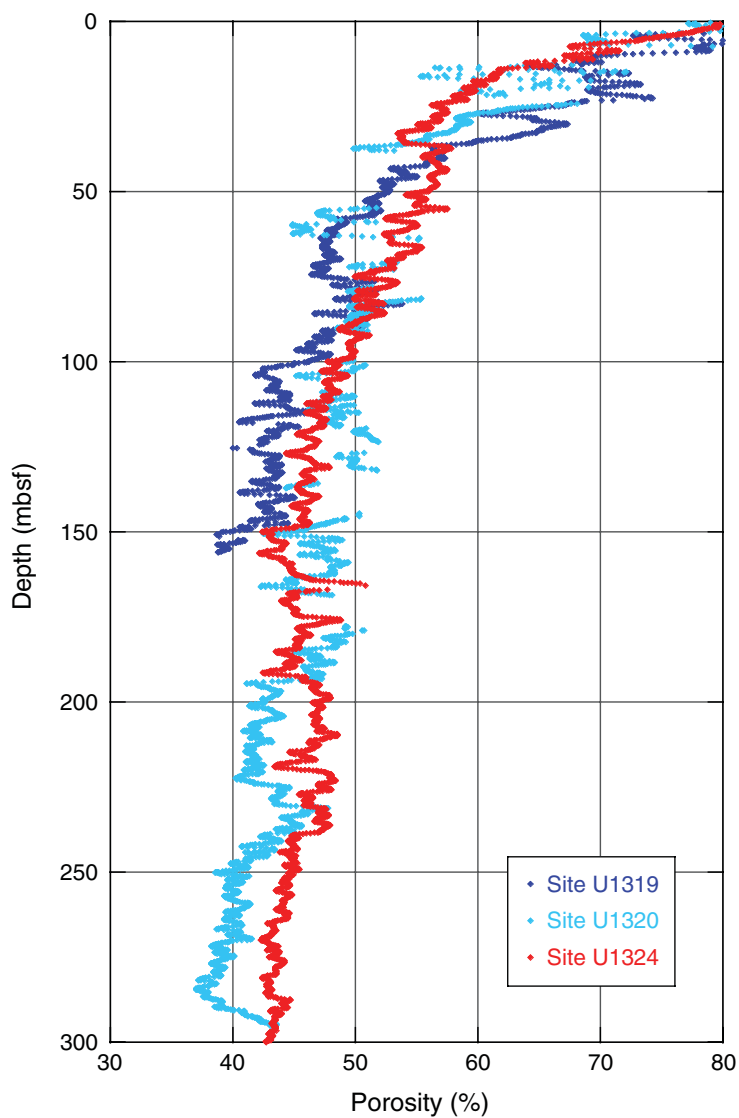


Figure F40. Pore water geochemical profiles at Sites U1319 and U1320 in Brazos-Trinity Basin #4.

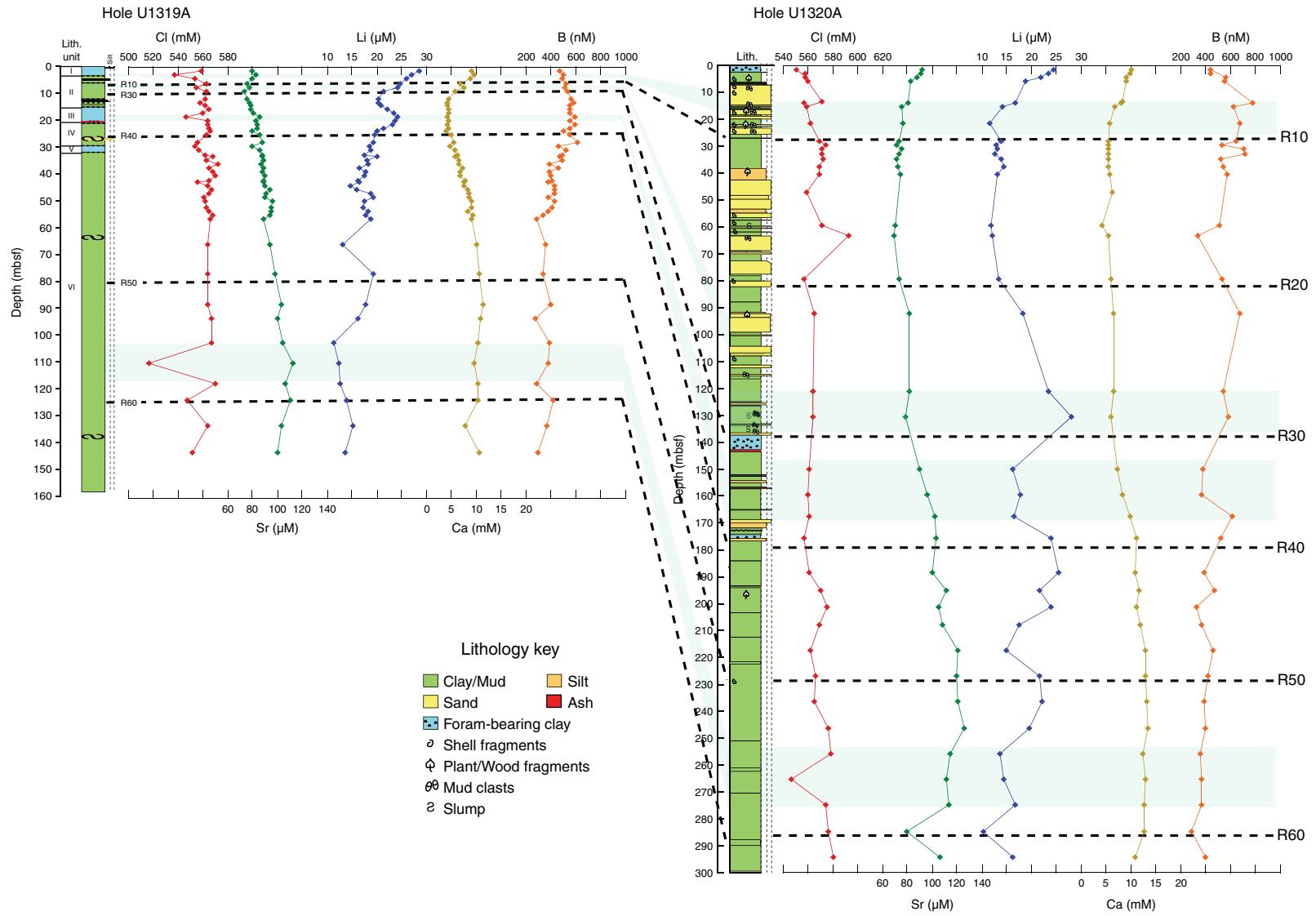


Figure F41. Pore water geochemical profiles at Sites U1322 and U1324 in Ursa Basin.

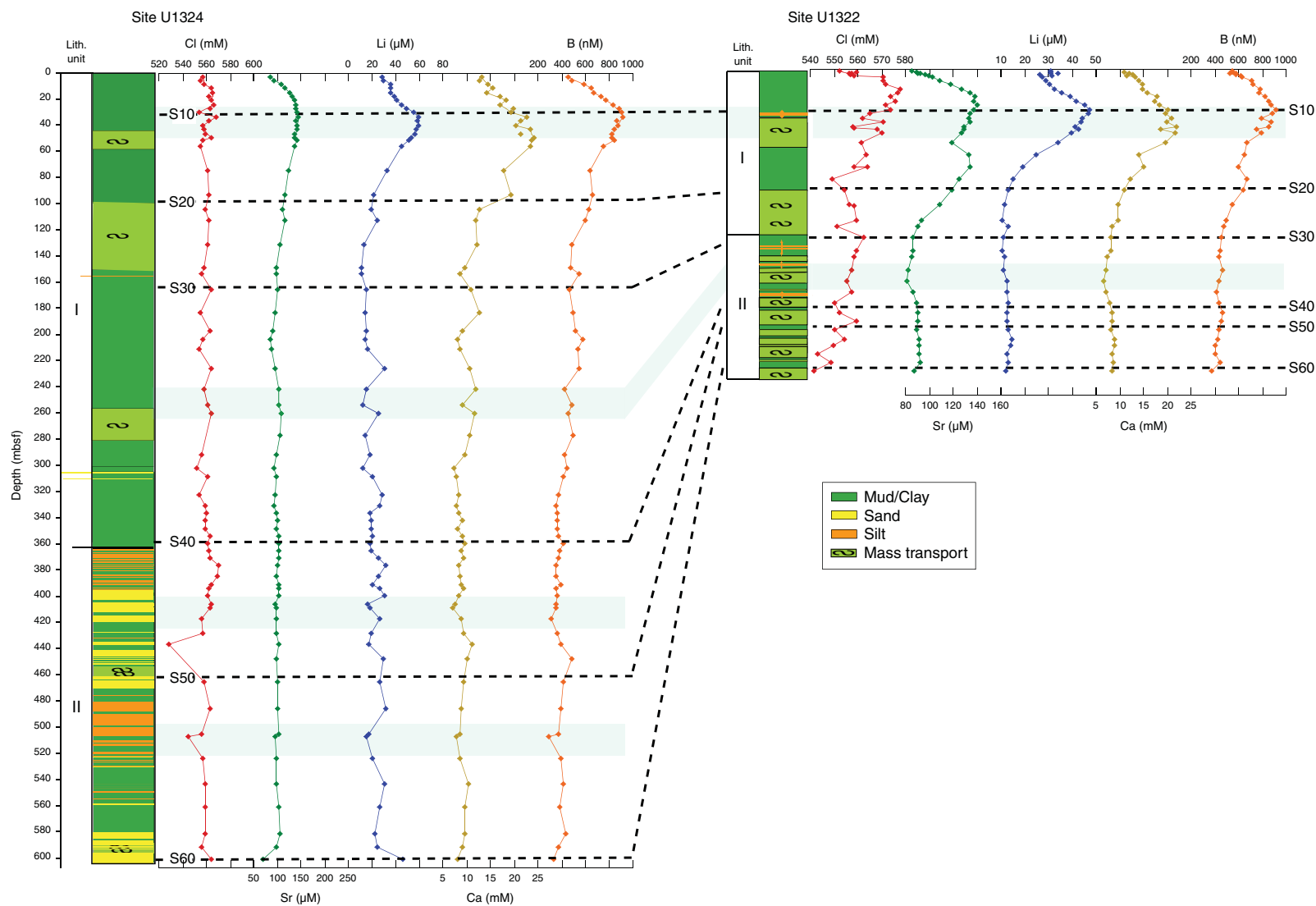


Figure F42. A. Site U1324 porosity versus depth. B. Site U1322 porosity versus depth. The change in porosity relative to depth is extremely similar at these two locations. MAD = moisture and density, LWD = logging-while-drilling.

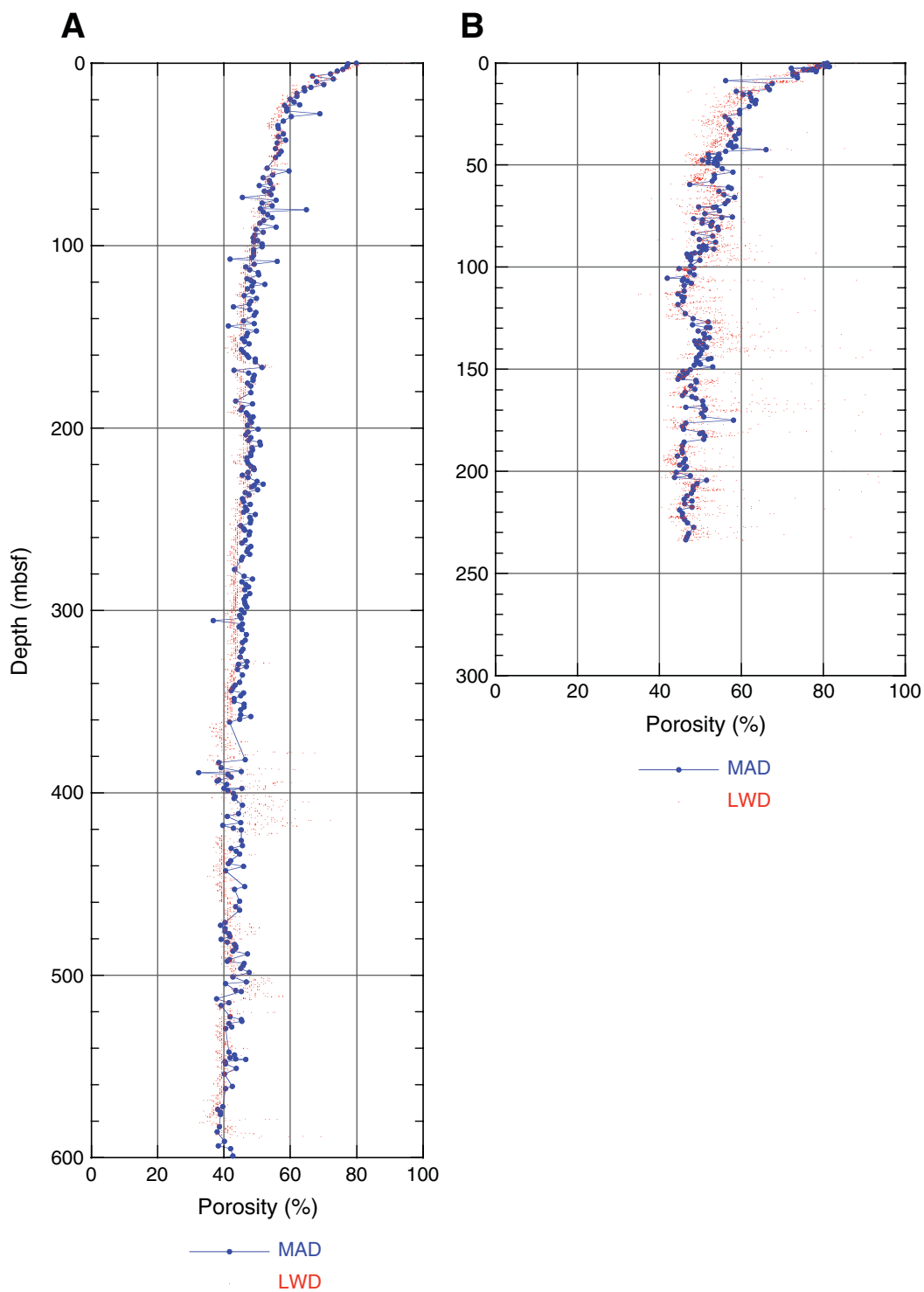


Figure F43. Porosity-based pressure prediction for (A) Site U1324 and (B) Site U1322. Both locations have fundamentally similar results. Conditions are predicted to be more or less hydrostatic to 150 mbsf and at deeper levels pressure rises to more than half of the distance to the lithostatic pressure. BSF = below sea-floor, DVTTP = Davis-Villinger Temperature-Pressure Probe, T2P = temperature and dual pressure probe.

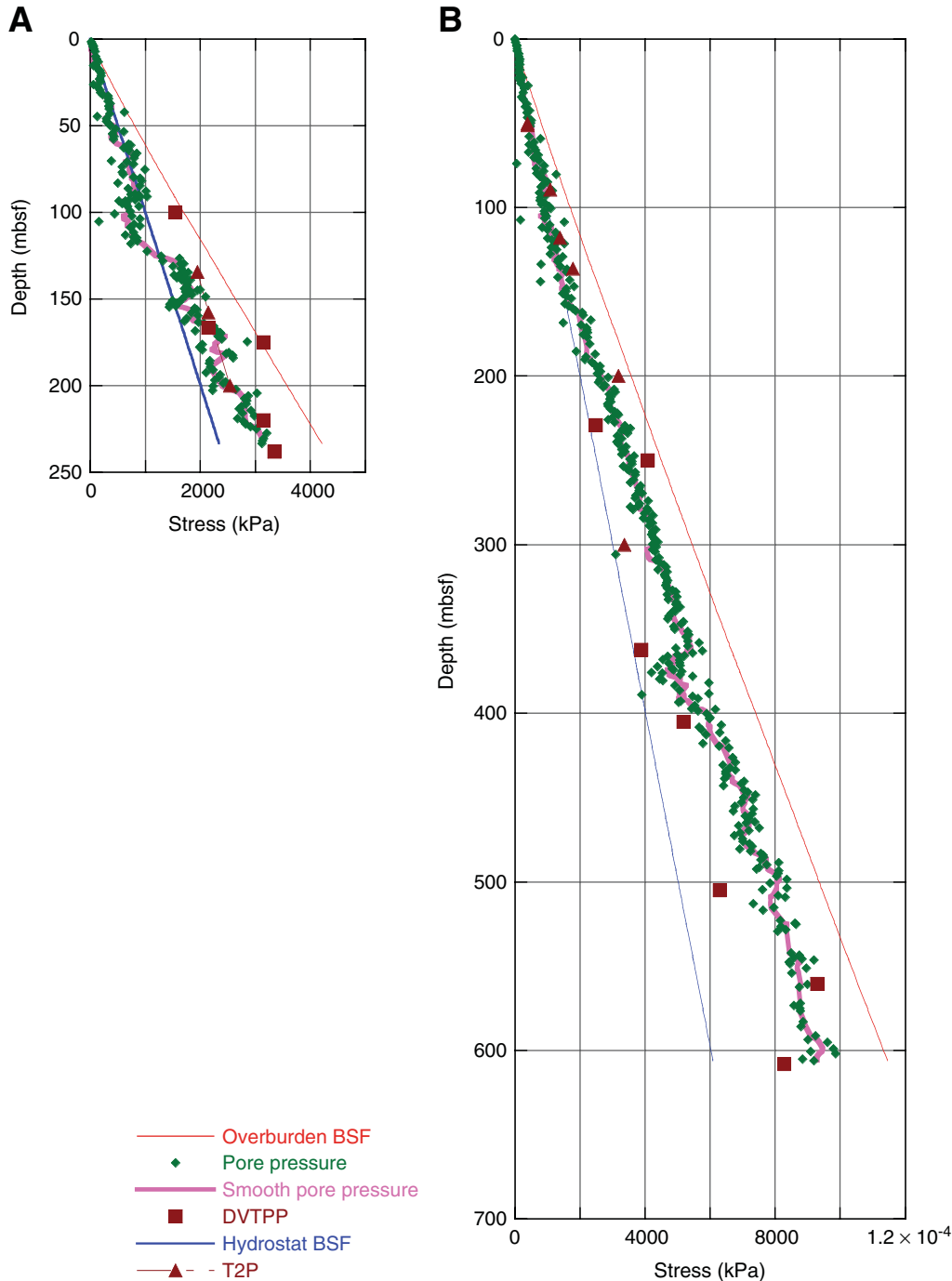


Figure F44. Pressure versus depth for penetrometer tools (Davis-Villinger Temperature-Pressure Probe [DVTPP] and temperature and dual pressure probe [T2P]). **A.** Site U1324. **B.** Site U1322. Pressure data suggest that to a depth of 250 mbsf pore pressures are greater at Site U1322 than at Site U1324. Solid symbols represent penetrations where there was a clear penetration and dissipation, whereas open symbols represent penetrations that were initially subhydrostatic and subsequently recovered to an elevated pressure.

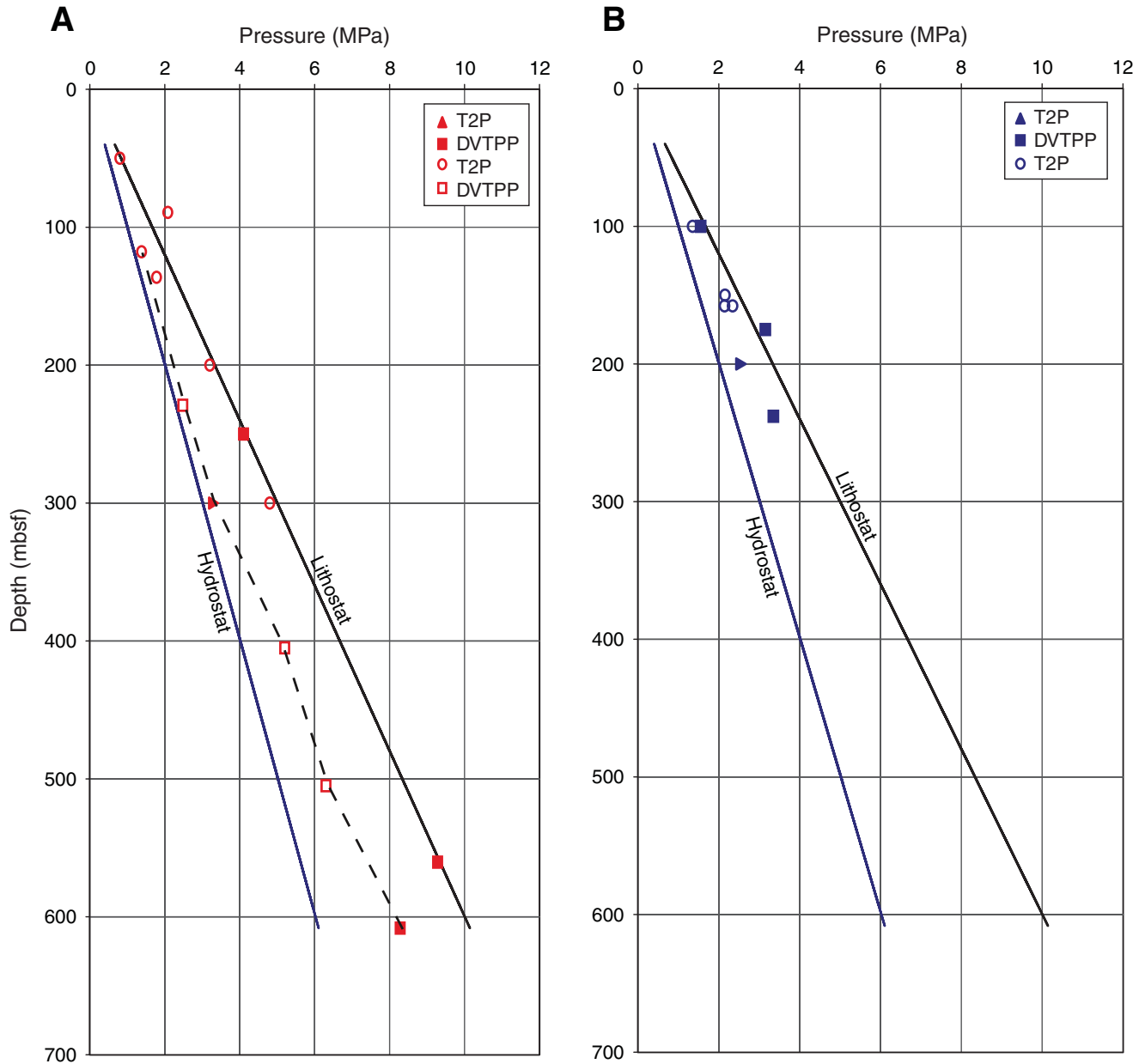


Figure F45. Temperature data for Site U1322 and Site U1324. Advanced piston corer temperature (APCT) tool data are corrected to predict the in situ temperature whereas Davis-Villinger Temperature-Pressure Probe (DVTTP) and temperature/dual pressure probe (T2P) data are not corrected. The average gradient at Site U1324 is 18.4°C/km whereas at Site U1322 the average gradient is 26.2°C/km.

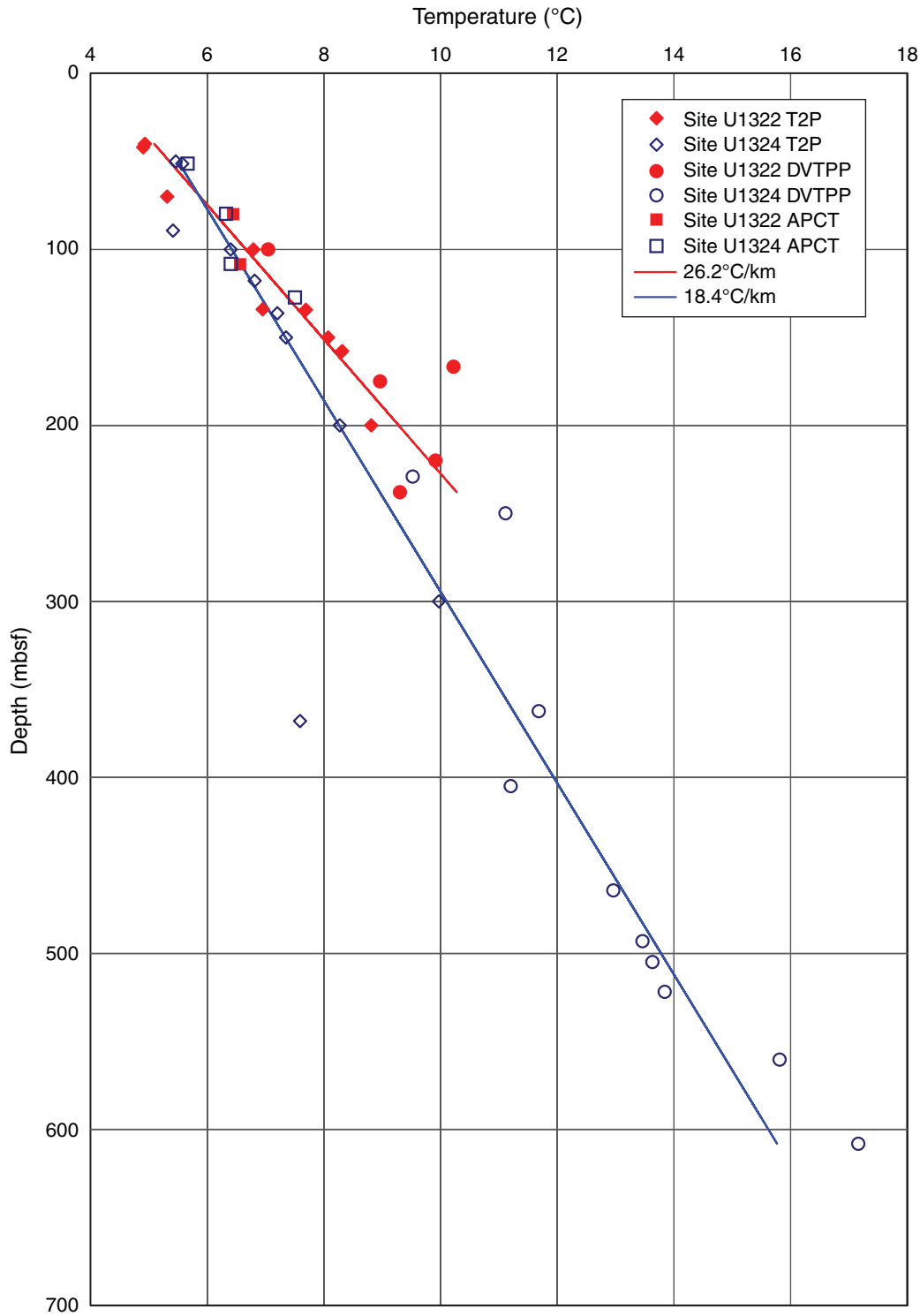


Figure F46. A. Site U1324. Temperature gradient = $\sim 18^\circ\text{C}/\text{km}$ (red), overpressure ratio (λ^*) = ~ 0.6 , overpressure = blue. B. Site U1322. Temperature gradient = $\sim 26^\circ\text{C}/\text{km}$ (red), overpressure ratio (λ^*) = ~ 0.6 , overpressure = blue. C. Conceptual model of flow in Ursa Basin. The constant overpressure gradient at both sites implies that flow is driven upward at approximately the same rate in both locations within the mudrock above the Blue Unit. However, because Site U1324 is considerably deeper than Site U1322, the pressures at the top of the Blue Unit must be greater at Site U1324 (~ 3.1 MPa) than at Site U1322 (~ 1.3 MPa). We infer that the Blue Unit is composed of multiple hydraulically isolated sand bodies. Flow is transported laterally from Site U1324 to U1322 only within the deepest sand body because the overlying sand bodies have been truncated by the Ursa channel-levee system. To the right of the levee, flow is upward through both sands and shales. The elevated temperature gradient at Site U1322 may record the lateral flow within the Blue Unit.

